

ECCE 2017

IEEE ENERGY CONVERSION CONGRESS & EXPO

Cincinnati, OHIO October 1-5

SPONSORED BY THE IEEE POWER ELECTRONICS
AND INDUSTRY APPLICATIONS SOCIETIES



PROCEEDINGS

IEEE ENERGY CONVERSION CONGRESS & EXPOSITION®

Welcome

Meeting Supporters

Schedule at a Glance

Leadership

Table of Contents

Author Index

Tutorials

2018 Call for Papers

Copyright

Search

Help

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Welcome from General Chair: Andy Knight



It is my pleasure to welcome you to Cincinnati for the 9th Annual IEEE Energy Conversion Congress & Exposition ECCE 2017, sponsored by the IEEE Power Electronics Society (PELS) and the IEEE Industry Applications Society (IAS).

As the world's leading technical conference and exposition for energy conversion solutions, ECCE provides a unique opportunity to engineers, researchers, students, and other professionals from the broad spectrum of energy conversion for the exchange of technical knowledge, networking, and exposure to the latest technology trends. ECCE is unique in our emphasis on integrated systems, presenting the best in contemporary energy conversion research alongside innovations from more traditional component topics.

As we are in Ohio, close to the home of the Wright brothers' pioneering efforts in aviation, ECCE 2017 features an emphasis on the challenges in aerospace electrification. This is highlighted in our plenary keynote speeches from Robert Bayles of UTC Aerospace Systems, Dr. Nateri K. Madavan of NASA and Dr. Huang Hao from GE Aviation Systems. We are extremely fortunate to have these distinguished leaders from industry to share their visions and wisdom with us.

At ECCE 2017, as we build on previous successes in our technical program, we have also made efforts to expand our professional program. This year, the technical program features 864 technical presentations which are selected from over 1500 digests submitted from across the globe. Technical papers are organized in 141 oral sessions across 10 time-slots and 29 poster sessions across 3 poster dialog sessions.

The professional program at ECCE 2017 begins on Sunday, with 11 tutorial sessions that offer an in-depth discussion of important and complex technical topics that combine practical application with theory. After the Monday plenary session, we have expanded our special sessions to offer applied and practical topics throughout the first three days of the conference. Special session topics include: Workforce Development and Careers in Power Electronics from the US Power Electronics Industry Collaborative; a joint session between IAS and KIPE on developments in Energy Conversion in Korea; Advances in Magnetic Materials. Recognizing and taking advantage of our location in Cincinnati, Wednesday features a series of four special sessions on challenges facing aerospace electrification. Wednesday also sees a session on power electronics in low inertia electrical systems, and two joint sessions on the interface between Power Electronics and Power Systems. Smart Grid initiatives are also emphasized by technical tours to the Duke Energy Envision Center. A new focus of the professional program this year is our support of Women in Engineering. There is a WIE function on Monday evening, the traditional PELS WIE breakfast on Wednesday and a family space reserved for any attendees who may be traveling with small children.

We are very pleased to acknowledge the support of Wolong Electric Group Co. and GE Aviation Systems as Platinum Partners for ECCE 2017. Both our Platinum Partners will join our other exhibitors and partners in the Exhibition Hall on Monday and Tuesday. The exhibitors will showcase their state-of-the-art technologies, products, and solutions, creating a highly interactive networking environment. This year sees the return products and services presentations to the Expo floor, together with the poster sessions and student demonstrations.

For many of our attendees, the ECCE conference is like a homecoming event where you can catch up with old friends and meet new ones. One of the changes that people may see this year is the co-location of the Industry Applications Society Annual Meeting. ECCE and the IAS AM will operate as separate conferences, with their own technical and professional programs. However, IAS AM attendees will join us at our social functions. We look forward to new networking opportunities with our IAS colleagues at the Welcome Reception, Expo Opening Reception, Industry Night Out, and Awards Luncheon. For those new to ECCE, thank you for joining us and we hope you can come to our first timer session just before the Sunday Welcome Reception event.

ECCE 2017 provides two Creative Digressions Lounges, spaces that do not need a reservation and provide a place for colleagues and friends to brainstorm on a few ideas generated during the conference, with paper boards, markers, and of course coffee and refreshments. Additionally, ECCE 2017 has three rooms that may be booked by industry organizations, exhibitors or alumni groups for private meetings.

I would like to express my utmost gratitude to the members of the organizing committee, the technical program committee, the steering committee, and Courtesy Associates / SmithBucklin, who with hard work and selfless dedication have made possible this event. I would like to thank PELS and IAS for their sponsorship and stewardship, and the generous support of all our corporate partners. I would like to thank each and every one of you as a presenter, an attendee, an exhibitor, a volunteer, or any combined role of the above for your contribution and participation.

Once again I welcome you to ECCE 2017,

A handwritten signature in black ink that reads "Andy Knight". The signature is fluid and cursive.

Andy Knight
General Chair IEEE ECCE 2017

Welcome from Technical Program Chairs

Electrical energy conversion is driving forward not only the industry, but also our society. We transform solar, wind, wave, heat, fuel energy into electrical energy. We can then store this in batteries, or transform it into mechanical energy through motors, or into light energy via lighting systems, or supply power converters. The whole process represents industrial connections and collaboration at its best. Since the start of the ECCE conference series in 2009, there has been a continuous growth in the numbers of technical papers submitted, the topics covered and worldwide attendance representation. We are pleased that you have selected ECCE to be one of the top events and conferences in the world and greatly appreciate your support as an author and/or attendee. In 2017, for the 9th edition of ECCE, there have been submitted 1504 digests – this is in line with the average achieved in the last three years of the event. Following the peer review process, a total of 864 papers have been accepted and scheduled into 16 parallel oral sessions and 3 poster sessions. An acceptance ratio of 57.5% shows that all research topics and results that will be presented at ECCE 2017, have earned the right to publication through a good competition. As a tradition started few years back, there are 10 presentation-only special sessions that are scheduled throughout the week.

Each submitted digest has been peer reviewed by three to five experts in the field. It is here, that we want to express our appreciation and big thanks for all the experts from around the world, who by volunteering to be part of the review process, make this conference a successful event. On average, we had over 4 reviews per digest. The review process was monitored by the Technical Program Committee (TPC), which is formed by Chairs, Vice Chairs, and Topic Chairs. Based on reviewers' comments/observations, the Topic Chairs responsible for that technical sub-track made a proposal for publication to the corresponding Vice Chairs, which proposed a final recommendation to the TPC Chairs. As per the usual procedure, all accepted digests have been discussed in the TPC meeting. As TPC Chairs, we have tried our best to monitor the whole review process, providing guidelines when and if required. Each of the TPC members has his/her responsibilities and as a group we have worked hard to ensure a uniform acceptance standard across all the tracks. The allocation of an accepted digest to a certain topic session and the mode of presentation, i.e. oral or poster, is the result of creating a balanced program. This should allow the audience to attend presentations that are in the same specific field, but spread on several days in oral sessions, or discuss all technical details and meet the authors in poster sessions. All papers presented at ECCE 2017, will be uploaded to IEEE Xplore Digital Library and made available to the world research community. Please reference this official conference policy if your institution requires conference attendance justification. Following ECCE 2017, depending on the topics, all presented papers are eligible for submission to IEEE Transactions on Industry Applications or Power Electronics. Please contact for more details the specific technical committee covering the scope of your paper.

On behalf of the entire Technical Program Committee, we strongly trust that you will consider 2017 to be one of the best ECCE events yet. We look forward to seeing you in Cincinnati. Once again, we want to give our gratitude to all of you who have contributed to ECCE2017 as an author, reviewer, TPC member or attendee.

Sincerely,



Emmanuel Agamloh
Advanced Energy, USA



David Dorrell
University of KwaZulu-Natal, South Africa



Ryan Li
University of Alberta, Canada



Mircea Popescu
Motor Design Ltd, UK



Pat Wheeler
University of Nottingham, UK

ECCE 2016 Technical Program Chairs

Welcome from Society Presidents



On behalf of the IEEE Power Electronics Society and Industry Applications Society, it gives us immense pleasure to welcome you all to Cincinnati to attend the 9th Annual IEEE Energy Conversion Congress and Exposition (ECCE). Considering the growing importance of electrical energy conversion driven by the urgent need to reduce carbon emissions and save energy, the two Societies came together to establish the first ECCE in 2009. The objective was to provide a forum for the exchange of information among students, researchers and practicing professionals in the energy conversion business. ECCE 2017 organizing committee has worked diligently so we can once again bring together both users and researchers of energy conversion systems and sub systems with an emphasis on the content of technical papers and on the quality of the growing exposition.

Whether you are a first time attendee or regular attendee since 2009 or anything in between, we encourage you to enjoy the ECCE experience, create new networks and get involved in the organization of the future ECCE's. The technical committees of the two Societies work hard in consistently delivering an excellent technical program at ECCE. The committees conduct their meetings at various times during ECCE (Please refer to the meeting calendar in the program booklet) and are open to all Society members. If you are not a Society member, please visit the Society booth at the exposition area and become a member. The Society volunteers will be ready to answer any questions you may have.

Many thanks to our ECCE 2017 General Chair Prof. Andy Knight and his dedicated organizing committee who have developed an excellent program that is rich in its technical content with plenty of socializing opportunities. Please make use of this opportunity to network with other professionals in the energy conversion area. It is our hope that all the interactions and technical programs will give you and your organization the tools to advance the field and address the challenges of the industry.

Again, on behalf of both Societies, we welcome you to Cincinnati and wish you a pleasant and productive conference!

Alan Mantooth
President
IEEE Power Electronics Society

Tomy Sebastian
President
IEEE Industry Applications Society

Schedule-at-a-Glance

Saturday, September 30th

5:00PM – 7:00PM **Registration** 2nd Floor “V”

Sunday, October 1st

7:00AM – 7:00PM **Registration** 2nd Floor “V”

AM Tutorials • 8:00AM – 12:00PM

262	260/261	236	263	264	237/238
T1-1: High Power Medium Frequency Transformer Design Optimization	T1-2: Model Predictive Control of High Power Converters and Industrial Drives	T1-3: Modeling and Energy Management of Modern Shipboard Power Systems	T1-4: DC Arc Fault Detection and Protection in DC Electric Power Systems	T1-5: Practical Considerations for the Application of High Power Si and SiC Modules	T1-6: Isolated Bi-directional DC/DC Converter Topologies and Control

12:00PM – 1:00PM **Lunch on Your Own**

PM Tutorials • 1:00PM – 5:00PM

263	236	260/261	264	237/238
T2-1: Using Soft-Switching Technology to Design High-Power, High-Current, Isolated, DC/DC Converters that Achieve Low-Cost, High Reliability, and Electromagnetic Compliance	T2-2: SiC Power Device Design and Fabrication, And Insertion In Novel MV Power Conversion Systems	T2-4: Electrical Machine Analysis Using Free Software	T2-5: EMI Issues and Solutions in PWM Converters	T2-6: Wireless Power Transfer for Electric Vehicle and Mobile Applications

5:00PM – 5:45PM **ECCE Newcomers** Room: 252

5:30PM – 7:30PM **Welcome Reception** Grand Ballroom Pre-function Lobby

Monday, October 2nd

7:00AM – 7:00PM **Registration** 2nd Floor “V”

8:30AM – 10:20AM **Plenary Session** Grand Ballroom AB

10:20AM – 10:50AM **AM Break** Greenhouse Pre-function Lobby & South Concourse Alcove

Oral Sessions • 10:50AM – 12:30PM

200	201	203	204	205	206	207/208	230/31	232	233	236	237/38	260/61	262	263	264
S9: Modeling and Control of Resonant Converters	S8: DC/DC Converters I	S4: Applications of MMC	S7: Multi-Phase DC/AC Converters I	S10: Modeling and Control of Power Factor Correction Converters	S16: Magnetics I	S15: GaN Switching Performance	S6: Single-Phase DC/AC Converters I	S5: Inductive Power Transfer for EV Charging	S3: Dynamic Performance of Power Converters for Renewable Energy	S1: Power Conversion for Solar Photovoltaic Systems I	S2: Hybrid AC/DC Microgrids	S14: Diagnostics and Fault Tolerant Systems in Drives	S13: Control of Electric Drives I	S12: Axial Flux Machines	S11: Induction Machines I

12:30PM – 2:00PM **Lunch on Your Own**

Oral Sessions • 2:00PM – 4:05PM

200	201	203	204	205	206	207/208	230/31	232	233	236	237/38	260/61	262	263	264
S24: Modeling and Control of Multilevel Converters	SS1: Workforce Development and Careers in Power Electronics	S31: Wireless Power Transfer I	S21: Multi-Phase DC/AC Converters II	S23: Power Quality Control	S29: Magnetics II	S30: SiC Converter Applications	S22: Single-Phase DC/AC Converters II	S20: Control Aspects of Electrified Vehicles	S18: Power Converter Topologies for Renewable Energy	S17: Power Conversion for Solar Photovoltaic Systems II	S19: Renewable Impacts in Industrial Microgrids	S27: Medium Voltage Drives and High Power Drives	S28: Sensorless Drives I	S25: Switched Reluctance Machines	S26: Induction Machines II

4:15PM – 7:30PM **Expo Hall Reception** Exhibit Hall B

Poster Session 1 • 5:00PM – 7:30PM

Exhibit Hall B

Energy Storage Systems	AC/AC Converters	Reliability, Diagnostics and Fault Analysis of Power Electronics	AC Electrical Machines: Innovative Design Studies	Axial and Transversal Flux Machines	Utility Converters and Power Electronics Transformers	Motor Drives I	Switching Devices I	Electric Vehicle Energy Management	Sensing and Control for Power Converters	Modelling and Control of MMC	Control in Microgrids
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Tuesday, October 3rd

7:00AM– 5:30PM **Registration** 2nd Floor "V"

Oral Sessions • 8:30AM – 10:10AM

200	201	203	204	205	206	207/208	230/31	232	233	236	237/38	260/61	262	263	264
S40: Modeling and Control of Modular Multilevel Converter	S37: DC/DC Converters II	S33: Power Converters for HVDC Grids	S36: Multi-Phase AC/DC Converters	S39: Sensorless Methods and State and Parameter Estimation	S46: Wide Band Gap Device Reliability	S45: GaN Device and Gate Drive	S38: Single-Phase Grid Connected Converters	SS2: Industry Activities in Korea, Organized in Collaboration with KIPE	S32: Harmonic Compensation Techniques for Microgrids	S35: Power Conversion for Solar Photovoltaic Systems III	S34: Solid State Transformers	S43: Sensorless Drives II	S44: PM and IPM Motor Drives I	S41: Large Synchronous Machines	S42: Synchronous Reluctance Machines I

10:10AM– 10:30AM **AM Break** Greenhouse Pre-function Lobby & South Concourse Alcove

Poster Session 2 • 10:30AM – 1:00PM

Exhibit Hall B

Datacenters and Telecommunication Applications	Applications of Electric Traction and Propulsion	Multilevel Converters	DC/AC Converters	DC/DC Converters	PV Applications	EMI in Power Converters	Advances in Special Electrical Machines	Induction and Permanent Magnet AC Machines	Motor Drives II	Switching Devices II	Wireless Power Transfer	DC and Hybrid AC/DC Systems
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10:30AM– 5:30PM **Exhibit Hall Open** Exhibit Hall B

12:15PM – 2:30PM **Lunch** Exhibit Hall B

Poster Session 3 • 2:30PM – 5:00PM

Exhibit Hall B

Applications of MMC	Batteries and Wireless EV Charging	AC/DC Converters	Modeling and Control of Multilevel Converters	Modeling and Control of Grid Connected Converters	Power Quality	Stability of Converter Systems	Other Topics in Control, Modeling and Optimization of Power Converters	Analysis Techniques in Electrical Machines	AC Electrical Machines: Performance Estimation	Component Technologies	Renewable Energy and Grid Integration
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Wednesday, October 4th

7:00AM – 5:30PM **Registration** 2nd Floor "V"

7:30AM – 8:30AM **IEEE PELS Women In Engineering Breakfast (WIPELS)** Room: 211

Oral Sessions • 8:30AM – 10:10AM

200	201	203	204	205	206	207/208	230/31	232	233	236	237/38	260/61	262	263	264
S54: Design Optimization of Power Converters	S51: DC/DC Converter Topologies	S60: LED Drivers	S50: Control and Modulation of Multi-Phase AC/DC Converters	S53: Reliability, Diagnostic, and Faults Analysis in Power Converters I	SS7: Power Electronic Meets Power Utilities & Systems	S59: Packaging I	S52: AC-AC Converters I	SS3: Electrical Power for Aviation Applications	S48: Droop Control in Microgrids	S47: Wind Energy Systems	S49: Grid Connected Converter Stability	S57: Energy Efficient Motor Drives	S58: Induction Motor Drives	S55: Thermal and Faults of Electric Machines	S56: PM Machines and Windings

10:10AM– 10:30AM **AM Break** Greenhouse Pre-function Lobby & South Concourse Alcove

Oral Sessions • 10:30AM – 12:10PM

200	201	204	205	206	207/208	230/31	232	233	236	237/38	260/61	262	263	264
S73: Wireless Power Transfer II	S67: Modulation Techniques I	S64: LLC Converters	S66: Reliability, Diagnostic, and Faults Analysis in Power Converters II	SS8: Power Electronic Meets Power Utilities & Systems	S72: Packaging II	S65: AC-AC Converters II	SS4: IOT and Twin for Aviation	S62: Power Sharing Techniques in Microgrids	S61: Wind Energy Applications	S63: DC Circuit Breaker Design	S68: Modeling and Control of Grid Connected Converters I	S71: PM and IPM Motor Drives II	S69: Synchronous Reluctance Machines II	S70: Variable Flux PM Machines

12:10PM– 2:00PM **Lunch on Your Own**

Oral Sessions • 2:00PM – 3:40PM

200	201	204	205	206	207/208	230/31	232	233	236	237/38	260/61	262	263	264
S86: Wireless Power Transfer III	S80: Modulation Techniques II	S77: Resonant DC/DC Converters	S79: Reliability, Diagnostic, and Faults Analysis for Power Devices	SS9: Power Electronics and Control for Low-Inertia Electrical Systems	S85: High Voltage Devices	S78: Modular Multilevel Converters (MMC)	SS5: Advanced Aircraft Electrification beyond MEAs	S75: Droop Techniques for Microgrid Operation	S74: PV Plants and PV Farms	S76: Control in DC Microgrids	S81: Modeling and Control of Grid Connected Converters II	S84: Drive Applications	S82: Linear Machines	S83: PM Motor Design, Control and Testing

Schedule-at-a-Glance (continued)

Wednesday, October 4th (continued)

3:40PM– 4:00PM **PM Break** Greenhouse Pre-function Lobby & South Concourse Alcove

Oral Sessions • 4:00PM – 5:40PM

200	201	204	205	206	207/08	230/31	232	233	236	237/38	260/61	262	263	264
S99: Emerging Applications	S95: Model Predictive Control of Power Converters I	S91: DAB DC/DC Converters	S94: Modeling and Control of AC-DC Converters	SS10: Magnetic Materials Standards in the Research Environment	S89: Datacenters and Telecommunication Applications	S92: MMC Modulation and Control	SS6: Wide Band Gap Devices for the Aviation Applications	S90: Power Electronics in Electrified Vehicles	S87: Solar Photovoltaic Technologies	S88: Control and Design Techniques for Microgrids I	S93: Control of Grid Connected Converter	S98: Control of Electric Drives II	S96: Thermal Model of Electric Machines	S97: PM Machines, Demagnetization, Eccentricity and Losses

6:30PM– 8:30PM **Industry Night Out** Grand Ballroom AB

Thursday, October 5th

7:00AM – 12:00PM **Registration** 2nd Floor "V"

Oral Sessions • 8:30AM – 10:10AM

200	201	204	205	207/208	230/31	232	233	236	237/38	260/61	262	263	264
S113: New Device, Circuit and Control Strategies	S107: Model Predictive Control of Power Converters II	S104: Multilevel Converters Applications	S106: Modeling and Control of DC-DC Converters I	S112: SiC Switching I	S105: MMC New Topologies	S103: Wireless Charging for EV	S101: Power Quality of Grid Connected Converters I	S100: Other Topics in Renewable Energy Applications	S102: Control and Design Techniques for Microgrids II	S108: Stability in Power Converters	S111: Electric Drives for Wind and Other Renewable Integration	S109: High Torque Machines	S110: Small PM Motors

10:10AM – 10:30AM **AM Break** Greenhouse Pre-function Lobby & South Concourse Alcove

Oral Sessions • 10:30AM – 12:10PM

200	201	204	205	207/208	230/31	232	233	236	237/38	260/61	262	263	264
S127: Wireless Power Transfer IV	S121: Modeling and Control of DC-AC Converters I	S118: Multilevel Converters I	S120: Modeling and Control of DC-DC Converters II	S126: SiC Switching II	S119: PFC Converters	S117: Modeling and Monitoring of Batteries I	S116: Power Quality of Grid Connected Converters II	S114: Energy Storage Systems	S115: Power Conversion Systems for AC and DC Grids	S122: EMI in Power Converters	S125: Electric Drives for Aerospace and Traction Applications	S123: High Speed Machines	S124: Noise, Vibration, Short Circuit of Electric Machines

12:10PM – 2:00PM **Awards Luncheon** Grand Ballroom AB

Oral Sessions • 2:00PM – 3:40PM

200	201	204	205	207/208	230/31	232	233	236	237/38	260/61	262	263	264
S134: Isolated DC/DC Converters	S136: Modeling and Control of DC-AC Converters II	S133: Multilevel Converters II	S135: Grid Synchronization Techniques	S141: Device Self Sensing Techniques	S132: Single-Phase AC/DC Converters	S131: Modeling and Monitoring of Batteries II	S130: Grid Connected Inverters and LCL Filter Design	S129: Wave Energy System	S128: Hybrid Energy Systems	S137: Testing, Measurement, and Validation of Power Converters	S140: PM and IPM Motor Drives III	S139: General Topics in Electrical Machines	S138: Motors for Transportation

Organizing Committee

Technical Program

Technical Program Co-Chairs

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Dave Dorrell
Ryan Li
Mircea Popescu
Pat Wheeler

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Xu She

Professional Program

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Uday Deshpanday

Industry PR

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Special, Panel and Plenary Sessions

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Vanessa Broccoli
Rudy Wang

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Yilmaz Sozer
Mark Scott

Student Awards

Helen Li
Po Tai Cheng

Renewable and Sustainable Energy Applications

Rathore, Akshay (Vice Chair), Concordia University, Canada
 Mazumder, Sudip (Vice Chair), University of Illinois, Chicago, USA
 Kumar, Dinesh, Danfoss Drives A/S, Denmark
 Weise, Nathan, Marquette, University, USA
 Mahanty, Ranjit, Indian Institute of Technology (BHU), India
 Ma, Ke, Shanghai Jiao Tong University, China
 Liu, Liming, ABB Inc, USA
 Akin, Bilal, UT Dallas, USA
 Doolla, Suryanarayana, Indian Institute of Technology, Bombay, India
 Choi, Jaeho, Chungbuk National University, Korea
 Pan, Xuewei, Harbin Institute of Technology, China
 Sarkar, Tirthajyoti, ON Semiconductor, USA
 Mishra, Santanu, Indian Institute of Technology, Kanpur, India
 Khanna, Raghav, University of Toledo, USA
 Gao, Fei, University of Technology of Belfort-Montbéliard (UTBM), France

Smart Grid & Utility Applications

Grainger, Brandon (Vice Chair), University of Pittsburgh, USA
 Mirafzal, Behrooz (Vice Chair), Kansas State University, USA
 Barater, Davide, University of Parma, Italy
 Kish, Gregory, University of Alberta, Canada
 Suul, Jon Are, SINTEF Energy Research, Norway
 Izadian, Afshin, Purdue School of Engineering and Technology, USA
 Bifaretti, Stefano, University of Rome Tor Vergata, Italy
 Skorek, Adam, University of Quebec at Trois-Rivières, Canada
 Chen, Nan, ABB Corporate Research, Sweden
 Lu, Xiaonan, Argonne National Laboratory, USA
 Du, Yu, ABB Inc, USA
 Wang, Xiongfei, Aalborg University, Denmark
 Vasquez, Juan, Aalborg University, Denmark
 Zhao, Tiefu, UNC Charlotte, USA
 Garcia, Pablo, University of Oviedo, Spain
 Liang, Hao, University of Alberta, Canada
 Lee, Tzung-Lin, National Sun Yat-sen University, Taiwan
 Garcia, Jorge, University of Oviedo, Spain
 Chowdhury, Asif, Halla Mechatronics, USA
 She, Xu, GE Global Research, USA

Datacenters and Telecommunication Applications

Ordonez, Martin (Vice Chair), University of British Columbia, Canada
 Garcia, Pablo, University of Oviedo, Spain
 Siwakoti, Yam, University of Technology Sydney, Australia
 Alzola, Rafael Pena, University of Strathclyde, Scotland
 Tan, Nadia, Universiti Tenaga Nasional, Malaysia

Transportation Electrification Applications

Sarlioglu, Bulent (Vice Chair), University of Wisconsin-Madison
 Debnath, Suman, Oak Ridge National Lab, USA
 Galigekere, Veda Prakash, Oak Ridge National Lab, USA
 Kollmeyer, Phillip, MacMaster University, Canada
 Gao, Fei, University of Technology of Belfort-Montbéliard (UTBM), France
 Krishnamurthy, Mahesh, Illinois Institute of Technology, USA
 Ye, Jin, San Francisco State University, USA
 Wang, Mengqi, University of Michigan-Dearborn, USA

Power Converter Topologies

Zanchetta, Pericle (Vice Chair), University of Nottingham, UK
 Sun, Kai (Vice Chair), Tsinghua University, China
 Mishra, Santanu, Indian Institute of Technology, Kanpur, India
 Lei, Qin, Arizona State University, USA
 G. Lamar, Diego, University of Oviedo, Spain
 Lee, Tzung-Lin, National Sun Yat-sen University, Taiwan
 Solero, Luca, University of Roma Tre, Italy
 Grbovic, Petar, Huawei Technologies, Germany
 Petrella, Roberto, University of Udine, Italy
 Cao, Dong, North Dakota State University
 Pucci, Marcello, ISSIA-CNR, Italy
 Formentini, Andrea, University of Nottingham, UK
 Lidozzi, Alessandro, University of Roma Tre, Italy
 Manjrekar, Madhav, UNC Charlotte, USA
 Kshirsagar, Parag, UTRC, USA
 Itoh, Junichi, Nagaoka University of Technology, Japan
 Zarri, Luca, University of Bologna, Italy
 Tang, Yi, Nanyang Technological University, Singapore

Control, Modelling and Optimization of Power Converters

Pitel, Grant (Vice Chair), Magna Power Electronics, USA
 Muetze, Annette (Vice Chair), Graz University of Technology, Austria
 Preindl, Matthias, Columbia University, USA
 Lu, Xiaonan, Argonne National Laboratory, USA
 Essakiappan, Somasundaram, UNC Charlotte, USA
 Oriti, Giovanna, Naval Postgraduate School, USA
 Guerrero, Juan, University of Oviedo
 Anglani, Norma, University of Pavia, Italy
 Skorek, Adam, University of Quebec at Trois-Rivières, Canada
 Suul, Jon Are, SINTEF Energy Research, Norway
 Wang, Ruxi, GE Global Research, USA
 Bifaretti, Stefano, University of Rome Tor Vergata, Italy
 Wang, Xiongfei, Aalborg University, Denmark
 Wei, Lixiang, Rockwell Automation, USA
 Monopoli, Vito Giuseppe, Politecnico di Bari, Italy
 Chen, Minjie, Princeton University, USA

Electrical Machines

Chiba, Akira (Vice Chair), Tokyo Institute of Technology, Japan
Wung, Peter (Vice Chair), GE Aviation, USA
Bianchi, Nicola, University of Padova, Italy
Cavagnino, Andrea, Politecnico di Torino, Italy
Gebregergis, Abraham, Halla Mechatronics, USA
Inoue, Yukinori, Osaka Prefecture University, Japan
Islam, Mohammad, Halla Mechatronics, USA
Jia, Shaofeng, Xi'an Jiaotong University, China
De Donato, Giulio, Sapienza-University of Rome
Reigosa, David Diaz, University of Oviedo, Spain
Gyftakis, Konstantinos, Coventry University, UK
Barater, Davide, University of Parma, Italy
Paul, Subhra, Nexteer Automotive, USA
Bird, Jonathan, Portland State University, USA
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Pucci, Marcello, ISSIA-CNR, Italy
Antonino-Daviu, Jose, Polytechnic University of Valencia, Spain
Lyra, Renato, Aerotech Inc, USA
Heins, Greg, Regal Beloit, Australia
Dutta, Rukmi, UNSW, Australia
Pakdelian, Siavash, University of Massachusetts Lowell, USA
Lee, Sang Bin, Korea University, Korea
Prasad, Rashmi, General Motors, USA
Vaschetto, Silvio, Politecnico di Torino, Italy
Qu, Ronghai, Huazhong University of Science and Technology, China

Electric Drives

Marques Cardoso, Antonio J. (Vice Chair), CISE/
University of Beira Interior, Portugal
Swamy, Mahesh (Vice Chair), Yaskawa America Inc, USA
Bazzi, Ali, University of Connecticut, USA
Scelba, Giacono, University of Catania, Italy
Dutta, Rukmi, UNSW, Australia
Jiang, Dong, Huazhong University of Science and Technology, China
Dazhong, Gu, UTRC, USA
Gebregergis, Abraham, Halla Mechatronics, USA
Paul, Subhra, Nexteer Automotive, USA
Chowdhury, Mazharul, Halla Mechatronics, USA
Bojoi, Radu, Politecnico di Torino, Italy
Yang, Shih-Chin, National Taiwan University, Taiwan
Fatemi, Alireza, General Motors, USA
Neely, John, Eaton Aerospace, USA
He, Jiangbiao, GE Global Research, USA
Su, Gui-Jia, Oak Ridge National Lab, USA
Barater, Davide, University of Parma, Italy
Liu, Jingbo, Rockwell Automation, USA

Pramod, Prerit, Nexteer Automotive, USA
Hinkkanen, Marko, Aalto University, Finland
Reigosa, David Diaz, University of Oviedo, Spain
Zhang, Pinjia, Tsinghua University, China
Mir, Sayeed, Eaton Aerospace, USA
Tallam, Rangarajan, Rockwell Automation, USA
Schroeder, Stefan, GE Global Research, Germany
Guerrero, Juan, University of Oviedo
Wu, Long, John Deere, USA
Zhao, Yue, University of Arkansas, USA
Pucci, Marcello, ISSIA-CNR, Italy
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Petrella, Roberto, University of Udine, Italy

Power Semiconductor Devices, Passive Components, Packaging, Integration, and Materials

Xu, Dehong Mark (Vice Chair), Zhejiang University, China
Krishnamurthy, Shashank (Vice Chair), UTRC, USA
Nawaz, Muhammad, ABB Corporate Research, Sweden
Guo, Ben, UTRC, USA
Costinett, Daniel, University of Tennessee, USA
Dong, Dong, GE Global Research, USA
Wada, Keiji, Tokyo Metropolitan University, Japan
Wang, Ruxi, GE Global Research, USA
Popovic, Jelena, TU Delft, Netherlands

Energy Efficient Systems Applications and Lighting Technologies

Dalla Costa, Marco (Vice Chair), Federal University of Santa Maria, Brazil
Afridi, Khurram (Vice Chair), University of Colorado Boulder, USA
Alonso, Marcos, University of Oviedo, Spain
Suzuki, Kayo, Acaterial Ltd., Japan
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Wang, Yijie, Harbin Institute of Technology, China
Lin, Ray-Lee, National Cheng Kung University, Taiwan
Perreault, David, MIT, USA
Zissis, Georges, University of Toulouse, France

Emerging Technologies and Applications

Wang, Jin (Vice Chair), Ohio State University, USA
Chen, Yaow-Ming (Vice Chair), National Taiwan University, Taiwan
Luo, Fang, Ohio State University, USA
Chiu, Huang-jen, National Taiwan University of Science and Technology, Taiwan
Chen, Ching-Jan, National Taiwan University, Taiwan
Wang, Huai, Aalborg University, Denmark
Lucia, Oscar, University of Zaragoza, Spain
Chen, Nan, ABB Corporate Research, Sweden

Conflict of Interest

Burgos, Rolando (Vice Chair), Virginia Tech, USA

TABLE OF CONTENTS

Scroll to the title and select a [Blue](#) link to open a paper. After viewing the paper, use the bookmarks to the left to return to the beginning of the Table of Contents.

Monday, October 2

Session 1: Power Conversion for Solar Photovoltaic Systems I

Chair(s): Ranjit Mahanty, Yongheng Yang

[Single-Stage Three-Phase Grid-Connected Photovoltaic System with Maximum Power Tracking and Active and Reactive Power Control based on Nonlinear Control](#) 1
Pablo R. Rivera, Michael L. McIntyre, Mohammad Mohebbi and Joseph Latham
University of Louisville, United States

[A Single Phase Doubly Grounded, PV Inverter using Coupled Inductor with Integrated Magnetics and Active Power Decoupling Technique](#) 8
Yinglai Xia, Jinia Roy and Raja Ayyanar
Texas Instruments, United States; Arizona State University, United States

[A ZVT Cell for High-Frequency Quasi-Resonant Converters in ON-OFF Mode for Solar Applications](#) 15
Hossein Mousavian, Alireza Bakhshai and Praveen Jain
Queen's University, Canada

[Sliding Mode Control of a Single Phase Transformer-less PV Inverter with Active Power Decoupling](#) 23
Jinia Roy, Yinglai Xia and Raja Ayyanar
Arizona State University, United States; Texas Instruments, United States

Session 2: Hybrid AC/DC Microgrids

Chair(s): Jinjun Liu, Meiqin Mao

[Adaptive Active Power Sharing Techniques for DC and AC Voltage Control in a Hybrid DC/AC Microgrid](#) 30
Ángel Navarro-Rodríguez, Pablo García, Ramy Georgious and Jorge García
University of Oviedo, Spain

[Modulation and Control Method for Bidirectional Isolated AC/DC Matrix based Converter in Hybrid AC/DC Microgrid](#) 37
Fanxiu Fang and Yun Wei Li
University of Alberta, Canada

[Fault Ride-Through Capability of Hybrid AC/DC Microgrids during AC and DC Network Faults](#) 44
Lasantha Meegahapola, Inam Ullah Nutkani, Brendan McGrath and Donald Grahame Holmes
RMIT University, Australia

[An Effective DC Microgrid Operation Using a Line Impedance Regulator](#) 52
Fatih Cingoz, Awab Ali, Ali Elrayyah, Yilmaz Sozer and J. Alexis De Abreu-Garcia
University of Akron, United States; Qatar Environment Research Institute, Qatar

Session 3: Dynamic Performance of Power Converters for Renewable Energy

Chair(s): Hui Li, Adel Nasiri

Robust H_{∞} DC Link Control Design for High-Power Density Converters with High-Order Filter in PV Systems	58
Nima Amouzegar Ashtiani, S. Mohsen Azizi and S. Ali Khajehoddin <i>University of Alberta, Canada; Michigan Technological University, United States; Concordia University, Canada</i>	
Grid Voltage Harmonic Damping Method for SPC based Power Converters with Multiple Virtual Admittance Control	64
Andres Tarrasó, Jose Ignacio Candela, Joan Rocabert and Pedro Rodriguez <i>Technical University of Catalonia, Spain; Universidad de Loyola, Spain</i>	
Adaptive Control of Grid-Connected Inverters based on Real-Time Measurements of Grid Impedance: DQ-Domain Approach	69
R. Luhtala, T. Messo, T. Reinikka, J. Sihvo, T. Roinila and M. Vilkkö <i>Tampere University of Technology, Finland</i>	
Improve the Robustness of Digitally-Controlled LCL-Filtered Inverters against Grid Impedance Variation with a Lag Compensator	76
Yuying He, Xuehua Wang and Xinbo Ruan <i>Huazhong University of Science and Technology, China</i>	

Session 4: Applications of MMC

Chair(s): Maryam Saedifard, Vito Giuseppe Monopoli

An MMC-based Topology using DHB Power Channels for Load Balancing in 50 Hz Railway Applications	83
Andreas Zafeiropoulos, Antonios Antonopoulos and Jan R. Svensson <i>ABB Corporate Research, Sweden</i>	
Communication Network Latency Compensation in Modular Multilevel Converters	91
Tomás P. Corrêa, Emilio J. Bueno and Francisco J. Rodriguez <i>University of Alcalá, Spain</i>	
Analysis and Mitigation of AC Coupling Effects on Overhead Line of Modular Multilevel Converter (MMC) based HVDC Transmission System	97
Joon-Hee Lee, Jae-Jung Jung and Seung-Ki Sul <i>Seoul National University, Korea</i>	
A Novel Pilot Protection Scheme for MMC-HVDC Transmission Lines	105
Lianying Ning, Xiaodong Zheng, Nengling Tai, Wentao Huang, Jinyi Chen and Zhongyu Wu <i>Shanghai Jiao Tong University, China; Shanghai Pudong Electric Power Corporation, China; MISO, United States</i>	

Session 5: Inductive Power Transfer for EV Charging

Chair(s): Suman Debnath, Daniel Ludois

An Analytical Method to Calculate Winding Resistance for Planar Coil with Ferrite Plate and Litz Wire in Inductive Power Transfer	111
Ming Lu and Khai D.T. Ngo <i>Virginia Polytechnic Institute and State University, United States</i>	

Comparative Evaluation of Front and Back End PFC IPT Systems for a Contactless Battery Charger	118
Ander Avila, Asier Garcia-Bediaga, Ugaitz Iruretagoyena, Irma Villar and Alejandro Rujas <i>IK4-Ikerlan Technology Research Centre, Spain</i>	
Field Attenuation around Inductive-Power-Transfer Coils with Dual-Side-Controlled Converter	126
Ming Lu and Khai D.T. Ngo <i>Virginia Polytechnic Institute and State University, United States</i>	
Power Factor Correction Focusing on Magnetic Coupling of Parallel-connected Wires for Inductive Power Transfer System	133
Keita Furukawa, Keisuke Kusaka and Jun-ichi Itoh <i>Nagaoka University of Technology, Japan</i>	
Session 6: Single-Phase DC/AC Converters I	
Chair(s): Adam Skorek, Feng Gao	
Mode Selection Strategy for Multi-Mode Power Converters to Minimize its Differential Power	141
R. Ramos, I. Zubitur, D. Serrano, J.A. Oliver, P. Alou and J.A. Cobos <i>Universidad Politécnica de Madrid, Spain</i>	
Investigation of Single-Phase Multilevel Inverter based on Series/Parallel-Connected H-Bridges ...	148
Antonio de P.D. Queiroz, Cursino B. Jacobina, Ayslan C.N. Maia, Victor F.M.B. Melo and Ivan da Silva <i>Federal University of Campina Grande, Brazil; Federal Institute of Paraíba, Brazil; Federal Institute of Alagoas, Brazil; Federal Institute of Pernambuco, Brazil</i>	
Design and Implementation of a DC-AC Inverter with Zero-Voltage-Switching	156
Hsin-Ju Liu, Tsorng-Juu Liang, Kuan-Ho Liu and Kai-Hui Chen <i>National Cheng Kung University, Taiwan</i>	
A Hybrid Two-Four Leg H-Bridge Inverter	161
Abinadabe S. Andrade and Edison R.C. da Silva <i>Federal Institute of Paraíba, Brazil</i>	
Session 7: Multi-Phase DC/AC Converters I	
Chair(s): David Diaz Reigosa, Marcello Pucci	
Critical-Mode-based Soft-Switching Modulation for Three-Phase Inverters	167
Zhengrong Huang, Zhengyang Liu, Fred C. Lee, Qiang Li and Furong Xiao <i>Virginia Polytechnic Institute and State University, United States; Beijing Institute of Technology, China</i>	
Implementing Synchronous DC Link Voltage Control with Phase Skipping on a Three-Phase Microinverter using Minimum DC Link Capacitance	175
S. Milad Tayebi, Siddhesh Shinde, Michael Pepper, Haibing Hu and Issa Batarseh <i>University of Central Florida, United States</i>	
Differential-Mode and Zero Sequence Circulating Current Reduction for Paralleled Inverters with Modified Zero-CM PWM Algorithm	183
Zewei Shen, Dong Jiang, Jianan Chen and Ronghai Qu <i>Huazhong University of Science and Technology, China</i>	

MPC-SVM Method with Subdivision Strategy for Current Ripples Reduction and Neutral-Point Voltage Balance in Three-Level Inverter	191
Hyun-Cheol Moon, June-Seok Lee, June-Hee Lee and Kyo-Beum Lee <i>Ajou University, Korea; Korea Railroad Research Institute, Korea</i>	

Session 8: DC/DC Converters I

Chair(s): Philip Krein, Santanu Mishra

Experimental Verification of a Bidirectional Chopper for Battery Energy Storage Systems Capable of Reduction in Size and Weight of an Inductor	197
Haruna Ohnishi and Makoto Hagiwara <i>Tokyo Institute of Technology, Japan</i>	

Magnetic Structure of Close-Coupled Inductors to Improve the Thermal Handling Capability in Interleaved DC-DC Converter	205
Thai Hoang Chuong, Shota Kimura, Daigoro Ebisumoto, Mostafa Noah, Masataka Ishihara, Masayoshi Yamamoto, Jun Imaoka and Wilmar Martinez <i>Shimane University, Japan; Okayama University, Japan; Nagoya University, Japan; Kyushu University, Japan; Toyota Technological Institute, Japan</i>	

Integrated Switched Coupled-Inductor Boost-Flyback Converter	211
Xinping Ding, Dailing Yu, Yingjie Song and Bicui Xue <i>Qingdao University of Technology, China; Jinan University, China</i>	

Energy Efficient Visible Light Communication Transmitter based on the Split of the Power	217
Juan Rodriguez, Daniel G. Aller, Diego G. Lamar and Javier Sebastian <i>University of Oviedo, Spain</i>	

Session 9: Modeling and Control of Resonant Converters

Chair(s): Gerry Moschopoulos, Rivas-davila Juan

Resonant LLC Bus Conversion using Homopolarity Width Control	225
Mehdi Mohammadi and Martin Ordonez <i>University of British Columbia, Canada</i>	

Dual-Loop Controller for LLC Resonant Converters using an Average Equivalent Circuit	230
Franco Degioanni, Ignacio Galiano Zurbriggen and Martin Ordonez <i>University of British Columbia, Canada</i>	

Modeling Resonant Converters in a Rotating Coordinate	237
Yi-Hsun Hsieh and Fred C. Lee <i>Virginia Polytechnic Institute and State University, United States</i>	

Closed-Loop Control of Impedance Control Network Resonant DC-DC Converter	244
Jie Lu, Ashish Kumar and Khurram K. Afridi <i>University of Colorado-Boulder, United States</i>	

Session 10: Modeling and Control of Power Factor Correction Converters

Chair(s): Aleksandar Prodic, Huai Wang

A Discontinuous Boost Power Factor Correction Conduction Loss Model	251
Yanqi Yu, Wilson Eberle and Fariborz Musavi <i>University of British Columbia, Canada; Washington State University, United States</i>	

Digital Control of an Interleaved BCM Boost PFC Converter with Fast Transient Response at Low Input Voltage	257
Robert T. Ryan, John G. Hayes, Richard Morrison and Diarmuid Hogan <i>University College Cork, Ireland; Excelsys Technologies, Ireland</i>	

New Modulated Carrier Control Method for Power Factor Correction Rectifier	265
Jintae Kim, Dong-Wook Yoo and Chung-Yuen Won <i>Sungkyunkwan University, Korea; Korea Electrotechnology Research Institute, Korea</i>	

Efficiency Evaluation of Three-Phase SiC Power Factor Correction Rectifier with Different Controllers	272
Alireza Kouchaki and Morten Nymand <i>University of Southern Denmark, Denmark</i>	

Session 11: Induction Machines I
Chair(s): **Andrea Cavagnino, Renato Lyra**

Induction Machine Design for Dynamic Loss Minimization along Driving Cycles for Traction Applications	278
Yuying Shi and Robert D. Lorenz <i>University of Wisconsin-Madison, United States</i>	

Impact of Core Material Grades on Performance of Variable Speed Induction Motors Fed by Inverters	286
Katsumi Yamazaki, Koki Tanaka and Motomichi Ohto <i>Chiba Institute of Technology, Japan; Yaskawa Motor Corp., Japan</i>	

Electrical Monitoring of Mechanical Defects in Induction Motor Driven V-Belt-Pulley Speed Reduction Couplings	293
Tae-June Kang, Chanseung Yang, Yonghyun Park, Sang Bin Lee and Mike Teska <i>Korea University, Korea; SKF Condition Monitoring Center, United States</i>	

A Simple Method for Determining Equivalent Circuit Parameters of Double-Cage Induction Motors from No-Load and Locked-Rotor Tests	301
Shu Yamamoto, Hideaki Hirahara, Akira Tanaka and Takahiro Ara <i>Polytechnic University, Japan</i>	

Session 12: Axial Flux Machines
Chair(s): **Akira Chiba, Giulio De Donato**

An Axial Flux-Focusing Magnetically Geared Motor	307
M. Bahrami Kouhshahi, J.Z. Bird, V. Acharya, K. Li, M. Calvin and W. Williams <i>Portland State University, United States; University of North Carolina at Charlotte, United States</i>	

Design of a Novel Interior Permanent Magnet Axial Flux Machine	314
Burak Tekgun, Tausif Husain, Shuvajit Das, Yilmaz Sozer and Marv Hamdan <i>University of Akron, United States; Bendix Commercial Vehicle Systems, United States</i>	

A Comparative Study of Coreless and Conventional Axial Flux Permanent Magnet Synchronous Machines Designed for Low and High Speed Operation	321
Narges Taran, Vandana Rallabandi, Dan M. Ionel and Greg Heins <i>University of Kentucky, United States; Regal Beloit Corporation, Australia</i>	

Comparison of Dual Structure Axial Flux-Switching Permanent Magnet Machines	328
Ju Hyung Kim, Mingda Liu, Hao Ding and Bulent Sarlioglu <i>University of Wisconsin-Madison, United States</i>	

Session 13: Control of Electric Drives I
Chair(s): Roberto Petrella, Hinkkanen Marko

Optimal Torque Control of Synchronous Motor Drives: Plug-and-Play Method	334
Hafiz Asad Ali Awan, Zhanfeng Song, Seppo E. Saarakkala and Marko Hinkkanen <i>Aalto University, Finland; Tianjin University School of Electrical and Information Engineering, China</i>	

Self-Commissioning Technique for High Bandwidth Servo Motor Drives	342
Yen-Shin Lai and Min-Hsien Ho <i>National Taipei University of Technology, Taiwan</i>	

A Geometrical Linearization Approach for Salient-Pole PMSM Optimal Voltage/Current Constrained Control over Whole Speed Range	350
Li Yang, Rui Gao, Wensong Yu and Iqbal Husain <i>North Carolina State University, United States</i>	

Algebraic Weighting Factor Selection for Predictive Torque and Flux Control	357
Tobias Geyer <i>ABB Corporate Research, Switzerland</i>	

Session 14: Diagnostics and Fault Tolerant Systems in Drives
Chair(s): Giacomo Scelba, Antonio J. Marques Cardoso

Faulted Phase Location Identification for Adjustable Speed Drives in High Resistance Grounding System	365
Jiangang Hu, Lixiang Wei, Jeffrey McGuire and Zhijun Liu <i>Rockwell Automation Inc., United States</i>	

Fault Analysis in an Inverter-Fed Nine-Phase Induction Machine	371
Tamires Santos de Souza, Rodrigo Rodrigues Bastos and Braz J. Cardoso Filho <i>Federal University of Minas Gerais, Brazil</i>	

Fault Detection and Tolerant Capability of Parallel Connected Permanent Magnet Machines under Stator Turn Fault	379
Shih-Chin Yang, Yu-Liang Hsu, Po-Huan Chou, Cheng-Xin Liu, Guan-Ren Chen and Kang Li <i>National Taiwan University, Taiwan; Feng Chia University, Taiwan; Industrial Technology Research Institute, Taiwan</i>	

Comparison of Open-Phase Fault Detection for Permanent Magnet Machine Drives using Different Fault Signals	385
Shih-Chin Yang, Yu-Liang Hsu, Po-Huan Chou, Da-Ren Jian and Guan-Ren Chen <i>National Taiwan University, Taiwan; Feng Chia University, Taiwan; Industrial Technology Research Institute, Taiwan</i>	

Session 15: GaN Switching Performance

Chair(s): Enrico Santi, Muhammad Nawaz

Analysis of Oscillation in Bridge Structure based on GaN Devices and Ferrite Bead Suppression Method 391

Fangwei Zhao, Yan Li, Qing Tang and Lu Wang
Beijing Jiaotong University, China

Switching Transient Analysis for Normally-Off GaN Transistors with p-GaN Gate in a Phase-Leg Circuit 399

Ruilang Xie, Guangzhao Xu, Xu Yang, Hanxing Wang, Mofan Tian, Yidong Tian, Feng Zhang, Wenjie Chen, Laili Wang and Kevin J. Chen
Xi'an Jiaotong University, China; Hong Kong University of Science and Technology, Hong Kong

Optimization of the Balance between the Gate-Drain Capacitance and the Common Source Inductance for Preventing the Oscillatory False Triggering of Fast Switching GaN-FETs 405

Ryunosuke Matsumoto, Kazuhiro Umetani and Eiji Hiraki
Okayama University, Japan

Static and Dynamic Characterization of a GaN-on-GaN 600 V, 2 A Vertical Transistor 413

Amy Romero, Christina DiMarino, Rolando Burgos, Ray Li, Mary Chen, Yu Cao and Rongming Chu
Virginia Polytechnic Institute and State University, United States; HRL Laboratories LLC, United States

Session 16: Magnetics I

Chair(s): David Perreault, Ruxi Wang

Medium Frequency Transformer Leakage Inductance Modeling and Experimental Verification 419

Marko Mogorovic and Drazen Dujic
EPFL, Switzerland

Continuum Modeling of Inductor Hysteresis and Eddy Current Loss Effects in Resonant Circuits 425

Jason Pries, Lixin Tang and Tim Burress
Oak Ridge National Laboratory, United States

Characterization of Magnetoresistors for Contactless Current Sensing in Power Electronic Applications 433

Shahriar Jalal Nibir, Hossein Niakan and Babak Parkhideh
University of North Carolina at Charlotte, United States

Trapezoidal Characterization of Magnetic Materials with a Novel Dual Voltage Test Circuit 439

Richard Beddingfield, Paras Vora, David Storelli and Subhashish Bhattacharya
North Carolina State University, United States

Session 17: Power Conversion for Solar Photovoltaic Systems II

Chair(s): Pedro Rodriguez, Lixiang Wei

Three-Phase DC-DC PWM Boost Converter for Renewable Energy Applications 447

Adel Ali Abosnina and Gerry Moschopoulos
Western University, Canada

Power Command Compensation Structure to Improve the Dynamic Performance for Single Phase Transformer-Less Photovoltaic Inverters with Dynamic Power Decoupling 455
Yinglai Xia, Ziwei Yu and Raja Ayyanar
Texas Instruments, United States; Arizona State University, United States

A Novel Model Predictive Control for Single-Phase Grid-Connected Photovoltaic Inverters 461
Esmail Zangeneh Bighash, Seyed Mohammad Sadeghzadeh, Esmail Ebrahimzadeh, Yongheng Yang and Frede Blaabjerg
Shahed University, Iran; Aalborg University, Denmark

Power Pulsation Decoupling for a Two-Stage Single-Phase Photovoltaic Inverter with Film Capacitor 468
Jianwu Zeng, Meixian Zhuo, Hao Cheng, Taesic Kim, Vincent Winstead and Liangcai Wu
Minnesota State University, United States; Growatt New Energy Technology Co. Ltd., China; Texas A&M University-Kingsville, United States

Differential Power Processing of Photovoltaic Systems for High Energy Capture and Reduced Cost 475
Mohamed Badawy and Yilmaz Sozer
San Jose State University, United States; University of Akron, United States

Session 18: Power Converter Topologies for Renewable Energy
Chair(s): Mohammad B. Shadmand, Tiefu Zhao

Soft-Switching Isolated Tri-Port Converter for Integration of PV, Storage and Single-Phase AC Grid 482
Nishant Bilakanti, Liran Zheng, Rajendra Prasad Kandula, Karthik Kandasamy and Deepak Divan
Georgia Institute of Technology, United States

Power-Loss Analysis in 3-Level TNPC Inverters: Modulation Effects 490
Emanuel Serban, Cosmin Pondiche and Martin Ordonez
Schneider Electric, Canada; University of British Columbia, Canada

Modeling and Design for Integrated Coupled Inductors in Interleaved Three-Level DC/DC Converters 498
Ruiyang Qin and Fred C. Lee
Delta Products Corporation, United States; Virginia Polytechnic Institute and State University, United States

Design Considerations of a Full-Bridge Modular Multilevel Converter under Variable DC Link Voltage 504
Ahmed Allu, Milijana Odavic and Kais Atallah
University of Sheffield, United Kingdom

Geometry Optimization and Characterization of Three-Phase Medium Frequency Transformer for 10kVA Isolated DC-DC Converter 511
Youngsil Lee, Gaurang Vakil, Alan J. Watson and Patrick W. Wheeler
University of Nottingham, United Kingdom

Session 19: Renewable Impacts in Industrial Microgrids
Chair(s): Marco Liserre, Giovanna Oriti

High-Speed Algorithm for Renewable Energy based Microgrid Fault Detection and Protective Coordination 519
Hashim A. Al Hassan, Qiang Fu, Vijay Bhavaraju, Yi Yang and Brandon M. Grainger
University of Pittsburgh, United States; Eaton, United States

Increasing the Robustness of Islanded CERTS Microgrids with PV Microsources and Gensets during Dynamic Overload Conditions	526
Zhe Chen, Mitch Marks and T.M. Jahns <i>University of Wisconsin-Madison, United States</i>	

A Wind Energy Battery Charging System with Dynamic Current Limitation	534
Guilherme de C. Farias, João V.M. Caracas, José G. de Matos and Luiz A. de S. Ribeiro <i>Enova Energia, Brazil; Universidade Federal do Maranhão, Brazil</i>	

A Fast Fault Protection based on Direction of Bus-Side Capacitor Discharge Current for a High-Surety Power Supply	542
Haijin Li, Min Chen, Boping Yang, Frede Blaabjerg and Dehong Xu <i>Zhejiang University, China; Aalborg University, Denmark</i>	

A First Approach for the Energy Management System in DC Micro-Grids with Integrated RES of Smart Ships	550
Angelo Accetta and Marcello Pucci <i>ISSIA-CNR, Italy</i>	

Session 20: Control Aspects of Electrified Vehicles
Chair(s): Jin Ye, Ian Brown

Control Strategies for a High Frequency DC-DC Converter for Electrified Vehicles	558
Xin Jing, Brian A. Welchko, Constantin Stancu and Peter J. Savagian <i>General Motors Company, United States</i>	

Maximum Efficiency Control Strategy of PM Traction Machine Drives in GM Hybrid and Electric Vehicles	566
Brian Gallert, Gilsu Choi, Kibok Lee, Xin Jing and Yochan Son <i>General Motors Company, United States</i>	

Optimal Performance of a Full Scale Li-Ion Battery and Li-Ion Capacitor Hybrid Energy Storage System for a Plug-In Hybrid Vehicle	572
Phillip Kollmeyer, Mackenzie Wootton, John Reimers, Tyler Stiene, Ephrem Chemali, Megan Wood and Ali Emadi <i>McMaster University, Canada</i>	

Hybrid Balancing in a Modular Battery Management System for Electric-Drive Vehicles	578
Fan Zhang, M. Muneeb Ur Rehman, Regan Zane and Dragan Maksimovic <i>University of Colorado-Boulder, United States; Utah State University, United States</i>	

Development of Compact Power Control Unit for HEVs	584
Shinya Yano, Yasushi Nakayama, Hiroshi Kobayashi, Seiki Hiramatsu, Motoru Yoshida, Kohei Onda, Komei Hayashi and Koji Yamazaki <i>Mitsubishi Electric Corp., Japan</i>	

Session 21: Multi-Phase DC/AC Converters II
Chair(s): Parag Kshirsagar, Grahame Holmes

A Three-Phase Grid-Connected Inverter Equipped with a Shunt Instantaneous Reactive Power Compensator	589
Kazuto Takagi and Hideaki Fujita <i>Tokyo Institute of Technology, Japan</i>	

A New Three-Level Three-Phase Boost PWM Inverter 597
Yam P. Siwakoti, Stephan Liese, Jian Guo Zhu and Frede Blaabjerg
University of Technology Sydney, Australia; Fraunhofer-Institute for Solar Energy Systems, Germany; Aalborg University, Denmark

A Sine-Like Hysteresis Current Control Method in Application of Three-Phase Voltage Source Converter 603
Hongyan Zhao, Yan Li, Trillion Q. Zheng, Xianjin Huang, Fangwei Zhao, Haobo Guo and Zhenning Zi
Beijing Jiaotong University, China; State Grid Electric Power Research Institute, China

Evaluation of Modulation Techniques to Eliminate Neutral Point Oscillation of the Four Pole NPC Converter 610
Meng-jiang Tsai and Po-tai Cheng
National Tsing Hua University, Taiwan

Y-Connected Topologies Composed of Three Three-Leg Converters with Two-Level and Three-Level Legs 617
Rodrigo P. de Lacerda, Edgard L.L. Fabricio, Cursino B. Jacobina, Marício B.R. Correa and Ivan da Silva
Federal University of Campina Grande, Brazil; Federal Institute of Paraíba, Brazil

Session 22: Single-Phase DC/AC Converters II
Chair(s): Madhav Manjrekar, Vladimir Blasko

Loss Reduction of 13.56 MHz Inverter based on Frequency Multiplying Method 625
Koji Orikawa, Satoshi Ogasawara and Jun-ichi Itoh
Hokkaido University, Japan; Nagaoka University of Technology, Japan

A Bridge Modular Switched-Capacitor-based Multilevel Inverter 632
Liangzong He, Chen Cheng, Jixiao Nai and Wenxiang Chen
Xiamen University, China

Pulse Energy Modulation for a Single-Phase Bridge Inverter with Power Decoupling Capability 637
Shuang Xu, Liuchen Chang and Riming Shao
University of New Brunswick, Canada

A High Control Bandwidth Design Method for Aalborg Inverter under the Weak Grid Condition ... 645
Weimin Wu, Cong Zou, Houqing Wang, Min Huang, Frede Blaabjerg and Henry Shu-Hung Chung
Shanghai Maritime University, China; Aalborg University, Denmark; City University of Hong Kong, Hong Kong

A Comprehensive Analysis of DC-Link Current for Single Phase H-Bridge Inverter Under Harmonic Output Currents 652
Tao Wang and Shuai Lu
Chongqing University, China

Session 23: Power Quality Control
Chair(s): Zheng Wang, Tsorng-Juu Liang

Single-Phase AC-DC-AC Topology for Grid Voltage Compensation 659
Nayara B. de Freitas, Cursino B. Jacobina and Rodrigo P. de Lacerda
Federal University of Campina Grande, Brazil

Single-Phase AC-DC-AC Multilevel Converter for Grid Overvoltage based on an H-Bridge Connected in Series to the Five-Leg Converter 667
 Antonio de P.D. Queiroz, Cursino B. Jacobina, Ayslan C.N. Maia, Victor F.M.B. Melo, Nayara B. de Freitas and Gregory A. de A. Carlos
Federal University of Campina Grande, Brazil; Federal Institute of Paraíba, Brazil; Federal Institute of Alagoas, Brazil; Federal Institute of Pernambuco, Brazil

Effects of DC-Link Filter on Harmonic and Interharmonic Generation in Three-phase Adjustable Speed Drive Systems 675
 Hamid Soltani, Pooya Davari, Dinesh Kumar, Firuz Zare and Frede Blaabjerg
Aalborg University, Denmark; Danfoss Drives A/S, Denmark; University of Queensland, Australia

Control System for Shunt Active Power Filters with Adaptive Voltage Saturation 682
 Albino Amerise, Michele Mengoni, Luca Zarri, Angelo Tani, Giovanni Serra and Domenico Casadei
University of Bologna, Italy

Research on Improved Hybrid Power Quality Conditioner for VV Co-Phase Railway Power Supply System 688
 Chenmeng Zhang, Jianming Li, Xishan Wen, Baichao Chen, Jiaxin Yuan, Wenli Fei and Mangmang Chen
State Grid Sichuan Electric Power Research Institute, China; Wuhan University, China; Southwest Electric Power Design Institute, China

Session 24: Modeling and Control of Multilevel Converters
Chair(s): Yongdong Li, Vito Giuseppe Monopoli

A Distributed Control Technique for the Multilevel Cascaded Converter 693
 Ping-heng Wu, Yu-chen Su and Po-tai Cheng
National Tsing Hua University, Taiwan

A Capacitor Voltage Balancing Method for a Three Phase Modular Multilevel DC-DC Converter 701
 Mingming Jiang, Shuai Shao, Kuang Sheng and Junming Zhang
Zhejiang University, China

Modeling and Suppression of Circulating Currents for Multi-Paralleled Three-Level T-Type Inverters 708
 Zicheng Zhang, Alian Chen, Xiangyang Xing, Ke Li, Chunshui Du and Chenghui Zhang
Shandong University, China

GA Optimized SHE PWM Hybrid Cascaded H-Bridge Multilevel Inverter with Capacitor Voltage Balancing 714
 Abhinandan Routray, R.K. Singh and R. Mahanty
Indian Institute of Technology, India

Resilient Two Dimensional Redundancy based Fault-Tolerant Controller Array for Modular Multi-Level Converters 722
 Ali Azidehak, Rajat Agarwal, Nima Yousefpoor, Alexander G. Dean and Subhashish Bhattacharya
North Carolina State University, United States

Session 25: Switched Reluctance Machines

Chair(s): Davide Barater, Iqbal Husain

A Fast Control-Integrated and Multiphysics-based Multi-Objective Design Optimization of Switched Reluctance Machines 730

Sufei Li, Shen Zhang, Chen Jiang, J. Rhett Mayor, Thomas G. Habetler and Ronald G. Harley
Georgia Institute of Technology, United States; University of KwaZulu-Natal, South Africa

Acoustic Noise Mitigation for High Pole Count Switched Reluctance Machines through Skewing Method with Multiphysics FEA Simulations 738

Yusuf Yasa, Mohammed Elamin, Yilmaz Sozer, John Kutz, Joshua S. Tylenda and Ronnie L. Wright
University of Akron, United States; DCS Corporation, United States; US Army, United States

Investigation of Torque Ripple in Switched Reluctance Machines with Errors in Current and Position Sensing 745

Cong Ma, Rakesh Mitra, Prerit Pramod and Rakib Islam
Nexteer Automotive Corp., United States

Comparison of Current Waveforms for Noise Reduction in Switched Reluctance Motors 752

Jihad Furqani, Masachika Kawa, Kyohei Kiyota, and Akira Chiba
Tokyo Institute of Technology, Japan

Simultaneous Optimization of Geometry and Firing Angles of In-Wheel Switched Reluctance Motor ... 760

Bahareh Anvari and Hamid A. Toliyat
Texas A&M University, United States

Session 26: Induction Machines II

Chair(s): Renato Lyra, Nicola Bianchi

Induction Machine Efficiency Measurement using a Variable Frequency Drive Source 768

Emmanuel Agamloh, Andrea Cavagnino and Silvio Vaschetto
Advanced Energy Corp., United States; Politecnico di Torino, Italy

Frequency, Load, and Flux Impacts on Induction Machine Copper and Core Losses in the qd0-Frame 776

Yiqi Liu and Ali M. Bazzi
University of Connecticut, United States

Induction Machine Rapid Performance Tests 782

Maher Al-Badri, Pragasen Pillay and Pierre Angers
Concordia University, Canada; Hydro-Quebec, Canada

Nonintrusive Efficiency Estimation for Large Power and High Voltage Induction Motors 786

Haisen Zhao, Pengyu Li, Geng Chen, Yilong Wang, Yang Zhan, Guorui Xu and Xiaofang Liu
North China Electric Power University, China

Separation of Slip- and High-Frequency Flux Densities and its Application in Rotor Iron Loss Fine Analysis of Induction Motors 794

Haisen Zhao, Bing Li, Wang Yilong Yang Zhan, Guorui Xu and Dong Dong Zhang
North China Electric Power University, China; Xian Jiaotong University, China

Session 27: Medium Voltage Drives and High Power Drives

Chair(s): Navid Zargari, Shih-Chin Yang

Assessment of Medium Voltage SiC MOSFET Advantages in Medium Voltage Drive Application 801

Hanning Tang and Alex Q. Huang
North Carolina State University, United States

High-Speed Medium Voltage (MV) Drive Applications Enabled by Series Connection of 1.7 kV SiC MOSFET Devices 808

Kasunaidu Vechalapu, Samir Hazra, Utkarsh Raheja, Abhay Negi and Subhashish Bhattacharya
North Carolina State University, United States

Integrated Motor Drive Design for Weight Optimization 816

Benjamin Cheong, Paolo Giangrande, Michael Galea, Pericle Zanchetta and Patrick Wheeler
University of Nottingham, United Kingdom

DC Current Balance with Common-Mode Voltage Reduction for Parallel Current Source Converters ... 824

Li Ding and Yun Wei Li
University of Alberta, Canada

Position Sensorless Control of a Permanent Magnet Linear Motor Connected through a Long Cable ... 830

Hussain A. Hussain and Hamid A. Toliyat
Texas A&M University, United States

Session 28: Sensorless Drives I

Chair(s): Fernando Briz, Abraham Gebregergis

Sensorless Speed Measurement for n-Phase Induction Machines under Open-Phase Fault by Means of Rotor Slot Harmonics 836

Alejandro G. Yepes, Jesús Doval-Gandoy, Fernando Baneira and Hamid Toliyat
University of Vigo, Spain; Texas A&M University, United States

Analysis on the Position Estimation Error in Position-Sensorless Operation using Pulsating Square Wave Signal Injection 844

Chae-Eun Hwang, Younggi Lee and Seung-Ki Sul
Seoul National University, Korea

Enhanced Methodology for Injection-based Real-Time Parameter Estimation to Improve Back-EMF Self-Sensing in Induction Machine Deadbeat-Direct Torque and Flux Control Drives 851

Kang Wang, Robert D. Lorenz and Noor Aamir Baloch
University of Wisconsin-Madison, United States; Yaskawa Electric Corporation, Japan

Compensation of Position Estimation Error for Precise Position-Sensorless Control of IPMSM based on High-Frequency Pulsating Voltage Injection 859

Younggi Lee, Yong-Cheol Kwon, Seung-Ki Sul, Noor Aamir Baloch and Shinya Morimoto
Seoul National University, Korea; Yaskawa Electric Corporation, Japan

Full Torque-Range Low-Speed Sensorless Drive for Heavily Saturated IPMSMs by Manipulation of Convergence Point 865

Yong-Cheol Kwon, Joo Hyun Lee and Seung-Ki Sul
Seoul National University, Korea

Session 29: Magnetics II

Chair(s): Shashank Krishnamurthy, Shuo Wang

A High-Reliable Magnetic Design Method for Three-Phase Coupled Inductor used in Interleaved Multi-Phase Boost Converters 873

Jun Imaoka, Kenkichi Okamoto, Masahito Shoyama, Mostafa Noah, Shota Kimura and Masayoshi Yamamoto
Kyushu University, Japan; Shimane University, Japan

Design and Additive Manufacturing of Multi-Permeability Magnetic Cores 881

L. Liu, C. Ding, S. Lu, T. Ge, Y. Yan, Y. Mei, K.D.T. Ngo and G-Q. Lu
Virginia Polytechnic Institute and State University, United States; Tianjin University, China

Influence of Switching Frequency and Saturation of the Magnetic Material on the Volume of Common-Mode Inductors used in Power Converter EMI Filters 887

Bilel Zaidi, Arnaud Videt and Nadir Idir
University of Lille, France

Variable Inductor Modeling Revisited: The Analytical Approach 895

J. Marcos Alonso, Marina Perdigão, Marco A. Dalla Costa, Shu Zhang and Yijie Wang
University of Oviedo, Spain; University of Coimbra, Portugal; Federal University of Santa Maria, Brazil; Harbin Institute of Technology, China

Winding and Air Gap Configurations for Power Inductors to Reduce Near Magnetic Field Emission 903

Huan Zhang, Shuo Wang and Qinghai Wang
University of Florida, United States; Huawei Technologies Co., Ltd., China

Session 30: SiC Converter Applications

Chair(s): Jean-Luc Schanen, Yuxiang Shi

Impact of Next-Generation 1700V SiC MOSFETs in a 125kW PV Converter 911

Jon Zhang, Fenton L. Rees, Brett Hull, Jeffrey B. Casady, Scott Allen and John W. Palmour
Wolfspeed, a Cree Company, United States; F.L. Rees and Associates, United States

Operation of Planar and Trench SiC MOSFETs in a 10kW DC/DC-Converter Analyzing the Impact of the Body Diode 917

Abdullah Eial Awwad and Sibylle Dieckerhoff
Technical University of Berlin, Germany

High Efficiency Power Converter with SiC Power MOSFETs for Pulsed Power Application 925

Ruxi Wang, Juan Sabate, Xiaohu Liu and Krishna Mainali
GE Global Research Center, United States; Busek Co., Inc., United States

Influence of SiC Technology in a Railway Traction DC-DC Converter Design Evolution 931

Alejandro Rujas, Víctor M. López, Asier García-Bediaga, Aloña Berasategi and Txomin Nieva
IK4-Ikerlan. Power Electronics Area, Spain; CAF Power and Automotion, Spain

Design of a 250 kW, 1200 V SiC MOSFET-based Three-Phase Inverter by Considering a Subsystem Level Design Optimization Approach 939

Ajith H. Wijenayake, Kraig J. Olejniczak, David Simco, Stephen Minden, Matthew Feurtado, Brandon Passmore, Ty McNutt, Alex Lostetter and Daniel Martin
Wolfspeed, A Cree Company, United States

Session 31: Wireless Power Transfer I

Chair(s): Huang-jen Chiu, Yaow-Ming Chen

Tunable Impedance Matching Network based on Phase-Switched Impedance Modulation 947

Alexander S. Jurkov, Aaron Radomski and David J. Perreault

Massachusetts Institute of Technology, United States; MKS Instruments Inc., United States

Design 13.56MHz 10 kW Resonant Inverter using GaN HEMT for Wireless Power Transfer Systems 955

Nguyen Kien Trung and Kan Akatsu

Shibaura Institute of Technology, Japan

An Optimized Frequency and Phase Shift Control Strategy for Constant Current Charging and Zero Voltage Switching Operation in Series-Series Compensated Wireless Power Transmission 961

Yongbin Jiang, Junwen Liu, Xiufang Hu, Laili Wang, Yue Wang and Gaidi Ning

Xi'an Jiaotong University, China

High-Power-Transfer-Density Capacitive Wireless Power Transfer System for Electric Vehicle Charging 967

Sreyam Sinha, Brandon Regensburger, Kate Doubleday, Ashish Kumar, Saad Pervaiz and Khurram K. Afridi

University of Colorado-Boulder, United States

Modeling and Analysis of Wireless Power Transfer System with Constant-Voltage Source and Constant-Current Load 975

Yiming Zhang, Zhengming Zhao and Ye Jiang

Missouri University of Science and Technology, United States; Tsinghua University, China

Session 32: Energy Storage Systems

Chair(s): Rashmi Prasad, Dazhong Gu

An Online LiFePO₄ Battery Impedance Estimation Method for Grid-Tied Residential Energy Storage Systems 980

Andres Salazar, Carlos Restrepo, Yabiao Gao, Javad Mohammadpour Velni and Antonio Ginart

Sonnen Inc., United States; University of Georgia, United States; Smart Wires, Inc., United States

An Improved Voltage Balance Strategy for Renewable Generation Energy Storage System 987

Muxin Han, Fu Jiang, Heng Li, Rong Zhou, Zhiwu Huang and Jun Peng

Central South University, China

Design Recommendations for Energy Systems: A UK Domestic Study 992

Konstantina Panagiotou, Christian Klumpner, Mark Sumner and Pat Wheeler

University of Nottingham, United Kingdom

A Decentralized SOC Balancing Method in Cascaded H-Bridge based Storage Modules 1000

Guangze Shi, Yao Sun, Wenbin Yuan, Hua Han, Mei Su and Xiaochao Hou

Central South University, China

Cloud-based Battery Condition Monitoring Platform for Large-Scale Lithium-Ion Battery Energy Storage Systems using Internet-of-Things (IoT) 1004

Amit Adhikaree, Taesic Kim, Jitendra Vagdoda, Ason Ochoa, Patrick J. Hernandez and Young Lee

Texas A&M University-Kingsville, United States

Environmental Tests and Evaluations of Variable 18650 Cylindrical Li-Ion Cells for Space Cell's Qualification Establishment	1010
Jonghoon Kim, P.-Y. Lee, C.-O Youn, Woonki Na and Minho Jang <i>Chungnam National University, Korea; California State University-Fresno, United States; Korea Aerospace Research Institute, Korea</i>	
A Hybrid Vanadium Redox/Lithium-Ion Energy Storage System for Off-Grid Renewable Power ...	1016
Leong Kit Gan, Jorn Reniers and David Howey <i>University of Oxford, United Kingdom</i>	
Electrical Circuit Modeling of Lithium-Sulfur Batteries during Discharging State	1024
Daniel-Ioan Stroe, Vaclav Knap, Maciej Swierczynski and Erik Schaltz <i>Aalborg University, Denmark</i>	
Supercapacitor to Provide Ancillary Services to the Grid	1030
V. Gevorgian, E. Muljadi, Yusheng Luo, M. Mohanpurkar, R. Hovsapian and V. Koritarov <i>National Renewable Energy Laboratory, United States; Idaho National Laboratory, United States; Argonne National Laboratory, United States</i>	
Cascaded Multilevel qZSI Powered Single-Phase Induction Motor for Water Pump Application	1037
Syed Rahman, Mohammad Meraj, Atif Iqbal, Mohd Tariq, Ali I. Maswood, Lazhar Ben-Brahim and Rashid Alammari <i>Qatar University, Qatar; Nanyang Technological University, Singapore; Aligarh Muslim University, India</i>	
Session 33: AC/AC Converters	
Chair(s): Yam Siwakoti, Luca Zarri	
Single-Phase Trans-Z-Source AC-AC Converter with Safe-Commutation Strategy	1043
Jixiao Nai, Liangzong He and Yuzi Lin <i>Xiamen University, China</i>	
A Post-Fault Strategy to Control the AC-AC Modular Multilevel Converter under Input-Side Line-to-Ground Fault	1050
Qichen Yang and Maryam Saeedifard <i>Georgia Institute of Technology, United States</i>	
Single-Phase Universal Active Power Filter with Five-Leg AC/DC/AC Converter	1057
Phelipe L.S. Rodrigues, Cursino B. Jacobina, Nayara B. de Freitas and Mauricio B.R. Correa <i>Federal University of Campina Grande, Brazil</i>	
Modulation and Control Strategy for a Single-Phase to Three-Phase Indirect Matrix Converter Drives	1065
Yeongsu Bak, June-Seok Lee and Kyo-Beum Lee <i>Ajou University, Korea; Korea Railroad Research Institute, Korea</i>	
Switched Capacitor Impedance Matrix Converter	1071
M. Raghuram, Avneet K. Chauhan and Santosh K. Singh <i>Indian Institute of Technology, India</i>	
A Modular Three-Phase AC-AC Converter with Small Number of Film Capacitors for High-Voltage High-Current Applications	1076
Ehsan Afshari and Mahshid Amirabadi <i>Northeastern University, United States</i>	

Control Scheme of the Modular Multilevel Matrix Converter using Space Vector Modulation for Wide Frequency Range Operation 1084
Yushi Miura, Takuya Fujikawa, Tomoaki Yoshida and Toshifumi Ise
Osaka University, Japan

Investigations on the Family of Center-Point-Clamped AC-AC Direct Power Converters 1092
Pankaj Kumar Bhowmik and Madhav Manjrekar
University of North Carolina-Charlotte, United States

Session 34: Reliability, Diagnostics and Fault Analysis of Power Electronics
Chair(s): Wei Qiao, Huai Wang

Diagnosis of Open-Circuit Faults for Six-Level Hybrid Inverters 1099
Quoc Anh Le, Ngoc Dat Dao and Dong-Choon Lee
Can Tho University, Viet Nam; Yeungnam University, Korea

Design of Power Converter in DFIG Wind Turbine with Enhanced System-Level Reliability 1105
Dao Zhou, Guanguan Zhang and Frede Blaabjerg
Aalborg University, Denmark; Central South University, China

Comparative Study on the Crowbar Protection Topologies for a DFIG Wind Turbine 1112
Andreas Giannakis, Efthymios Koroniotis and Athanasios Karlis
Democritus University of Thrace, Greece

Photovoltaic Condition Monitoring using Real-Time Adaptive Parameter Identification 1119
Jason Poon, Palak Jain, Costas Spanos, Sanjib Kumar Panda and Seth R. Sanders
University of California-Berkeley, United States; National University of Singapore, Singapore

A Fast Fault Diagnosis Method for Submodule Failures in Modular Multilevel Converters 1125
Kunshan Xu, Shaojun Xie, Ye Yan, Zhao Zhang, Binfeng Zhang and Qiang Qian
Nanjing University of Aeronautics and Astronautics, China

On Self-Healing of Grid-Tied PV Inverters Considering Current Sensor Inaccuracy and Aging Degradation 1131
Mehrddad Biglarbegan, Hamidreza Jafarian and Babak Parkhideh
University of North Carolina at Charlotte, United States

Fault Tolerant Control Method for Interleaved DC-DC Converters under Open and Short Circuit Switch Faults 1137
Elham Pazouki, Jose Alexis De Abreu-Garcia and Yilmaz Sozer
University of Akron, United States

A General Fault Diagnosis Strategy for Modular DC-DC Converter System 1143
Hanyu Wang, Xuejun Pei, Yuhuan Wu and Yong Kang
Huazhong University of Science and Technology, China

Monitoring Transistor Degradation in Power Electronic Converters using Saturation-Region Resistance 1148
Lei Ren, Chunying Gong and Xin Chen
Nanjing University of Aeronautics and Astronautics, China

Session 35: AC Electrical Machines: Innovative Design Studies

Chair(s): Phillip Kollmeyer, Zi-Qiang Zhu

- Principles and Characteristics of an Ultralightweight Electromagnetic Resonance Coupling Machine With a Cage Rotor** 1154
Kazuto Sakai, Kenta Takijima and Kazuki Nihei
Toyo University, Japan
- Investigation on the Frequency Effects on Iron Losses in Laminations** 1161
Omar Bottesi, Sandro Calligaro and Luigi Alberti
Free University of Bozen-Bolzano, Italy; University of Padova, Italy
- The Effect of Modulating Ring Design on Induction Machine with Integrated Magnetic Gear Torque** 1169
Dalia Zaky Abdelhamid and Andrew M. Knight
University of Calgary, Canada
- Practical Considerations on the Off-Line Measurements of PMSM and SyRM Inductances** 1175
Andrea Cavagnino, Silvio Vaschetto and Emmanuel Agamloh
Politecnico di Torino, Italy; Advanced Energy, United States
- Decoupled Current Control with Novel Anti-Windup for PMSM Drives** 1183
Kahyun Lee, Jung-Ik Ha and Dwarakanath Simili
Seoul National University, Korea; General Motors, United States
- Foil Conductor Concentrated Coil Windings for Modular Permanent Magnet AC Machines** 1191
Michael Rios, Giri Venkataramanan and Annette Muetze
University of Wisconsin-Madison, United States; Graz University of Technology, Austria
- Synchronous Machine Field Excitation Utilizing a Single Phase Matrix Converter Excited Rotary Transformer** 1197
Jiayang Liu and Thomas A. Lipo
University of Wisconsin-Madison, United States

Session 36: Axial and Transversal Flux Machines

Chair(s): Akira Chiba, Ayman El-Refaie

- Mechanical and Thermal Performance of Transverse Flux Machines** 1205
Iftekhar Hasan, Tausif Husain, Yilmaz Sozer, Iqbal Husain and Eduard Muljadi
University of Akron, United States; North Carolina State University, United States; National Renewable Energy Laboratory, United States
- Maximum Torque Output Control of Hybrid Permanent Magnet Axial Field Flux-Switching Memory Machine** 1212
Gongde Yang, Mingyao Lin, Nian Li, Xinghe Fu and Kai Liu
Southeast University, China
- Design Considerations and Performance Improvement of a Dual-Stator PM Vernier Motor with Axial-Flux Loop** 1220
Fei Zhao, Liyi Li, Chunhua Liu and Byung-il Kwon
Harbin Institute of Technology, China; City University of Hong Kong, Hong Kong; Hanyang University, Korea

Design, Analysis and Prototyping of a Flux Switching Transverse Flux Machine with Ferrite Magnets	1227
Zhao Wan and Iqbal Husain <i>North Carolina State University, United States</i>	
MAGNUS – An Ultra-high Specific Torque PM Axial Flux Type Motor with Flux Focusing and Modulation	1234
Vandana Rallabandi, Narges Taran, Dan M. Ionel and Ion G. Boldea <i>University of Kentucky, United States; Univerisitatea Politecnica Timisoara, Romania</i>	
Three-Part Hybrid Rotor PM Machine with Variable Magnetization State	1240
Dheeraj Bobba, Timothy A. Burress, Jason Pries and Bulent Sarlioglu <i>University of Wisconsin-Madison, United States; Oak Ridge National Laboratory, United States</i>	
Designing the First Stage of a Series Connected Multistage Coaxial Magnetic Gearbox for a Wind Turbine Demonstrator	1247
K. Li, J. Wright, S. Modaresahmadi, D. Som, W. Williams and J.Z. Bird <i>University of North Carolina at Charlotte, United States; Portland State University, United States</i>	
A Comprehensive Review of Permanent Magnet Transverse Flux Machines for Direct Drive Applications	1255
Tausif Husain, Iftekhar Hasan, Yilmaz Sozer, Iqbal Husain and Eduard Muljadi <i>University of Akron, United States; North Carolina State University, United States; National Renewable Energy Laboratory, United States</i>	
Session 37: Utility Converters and Power Electronics Transformers	
Chair(s): Fred Wang, Jinwei He	
A Novel Current Control Strategy for a Back-to-Back HVDC Applications under Unbalanced Operation Conditions	1263
Mohammed Alharbi, Faris E. Alfaris and Subhashish Bhattacharya <i>North Carolina State University, United States</i>	
Voltage Balancing of Modular Smart Transformers based on Dual Active Bridges	1270
Sante Pugliese, Markus Andresen, Rosa Mastromauro, Giampaolo Buticchi, Silvio Stasi and Marco Liserre <i>Polytechnic of Bari, Italy; Christian-Albrechts-Universität zu Kiel, Germany; University of Florence, Italy</i>	
Three-Port Energy Router for Universal and Flexible Power Management in Future Smart Distribution Grids	1276
L. Tarisciotti, P. Zanchetta, S. Pipolo and S. Bifaretti <i>University of Nottingham, United Kingdom; University of Rome Tor Vergata, Italy</i>	
Design and Implementation of a Series Resonant Solid State Transformer	1282
Mohammad Rashidi, Mohamad Sabbah, Abedalsalam Bani-Ahmed, Adel Nasiri and Mohammad Hasan Balali <i>University of Wisconsin-Milwaukee, United States</i>	
Design and Implementation of a 7.2kV Single Stage AC-AC Solid State Transformer based on Current Source Series Resonant Converter and 15 kV SiC MOSFET	1288
Qianlai Zhu, Li Wang, Dong Chen, Liqi Zhang and Alex Q. Huang <i>North Carolina State University, United States</i>	

Research on an Improved Hybrid Unified Power Flow Controller 1296
Baichao Chen, Wenli Fei, Jiaxin Yuan and Cuihua Tian
Wuhan University, China

Session 38: Motor Drives I

Chair(s): Fabio Giulii Capponi, Radu Bojoi

Two-Phase Open-End Winding Induction Motor Drive using Improved Current Source Inverter ... 1304
Louelson A.L. de A.C. Costa, Montiê A. Vitorino, Edgar R. Braga-Filho, Maurício B.R. Corrêa
and Darlan A. Fernandes
Federal University of Campina Grande, Brazil; Federal University of Paraiba, Brazil

An Extended Analytical Approach for Obtaining the Steady-State Periodic Solutions of SPWM Single-Phase Inverters 1311
Xu Cheng, Yanfeng Chen, Xi Chen, Bo Zhang and Dongyuan Qiu
South China University of Technology, China

Reliability Analysis and Life Testing of Semiconductor Devices for In-Wheel Motor Drive System .. 1317
Chao Ji, Geoffrey Owen, Simon T.M. Brockway and Chris Hilton
Protean Electric Ltd., United Kingdom

Comparison of Operating Modes for a Brushless Doubly Fed Reluctance Motor Drive 1323
Ronald S. Rebeiro and Andrew M. Knight
University of Calgary, Canada

Sensorless Direct Torque Control of Induction Motors with Fault-Tolerant Extended Kalman Filtering 1331
Xin Wang
Southern Illinois University, United States

A Modulated Model Predictive Control Scheme for the Brushless Doubly-Fed Induction Machine 1338
Xuan Li, Tao Peng, Hanbing Dan, Guanguan Zhang, Weiyi Tang and Pat Wheeler
Central South University, China; University of Nottingham, United Kingdom

Session 39: Switching Devices I

Chair(s): Tanya Gachovska, Jun Wang

Comparative Assessment of 3.3kV/400A SiC MOSFET and Si IGBT Power Modules 1343
Claudiu Ionita, Muhammad Nawaz, Kalle Ilves, and Francesco Iannuzzo
ABB Corporate Research, Sweden; Aalborg University, Denmark

Characterization and Performance Evaluation of State-of-the-Art 3.3 kV 30 A Full-SiC MOSFETs 1350
Alinaghi Marzoughi, Rolando Burgos and Dushan Boroyevich
Virginia Polytechnic Institute and State University, United States

Research on an Improved DC-Side Snubber for Suppressing the Turn-Off Overvoltage and Oscillation in High Speed SiC MOSFET Application 1358
Mei Liang, Yan Li, Qian Chen, Yi Lu, Haihong Yu, Trillion Q. Zheng, Haobo Guo and Fangwei Zhao
Beijing Jiaotong University, China; State Grid Zhejiang Electric Power Corporation, China

A Modified Equivalent Circuit based Electro-Thermal Model for Integrated POL Power Modules 1366
Wenbo Liu, Sam Webb, Yan-Fei Liu, Laili Wang and Doug Malcolm
Queen's University, Canada; Sumida Technologies Inc., Canada

Investigation of Cascode Structure GaN Devices in ZCS Region of LLC Resonant Converter	1374
<i>Junlin Xiang, Xiaoyong Ren, Yakun Wang and Yue Zhang Nanjing University of Aeronautics and Astronautics, China</i>	
Design of High-Speed H-Bridge Converter using Discrete SiC MOSFETs for Solid-State Transformer Applications	1379
<i>Dong Dong, Mohammed Agamy, Gary Mandrusiak and Qin Chen GE Global Research, United States</i>	
Role of Parasitic Capacitances in Power MOSFET Turn-On Switching Speed Limits: A SiC Case Study	1387
<i>Davide Cittanti, Francesco Iannuzzo, Eckart Hoene and Kirill Klein Politecnico di Torino, Italy; Aalborg University, Denmark; Fraunhofer IZM, Germany</i>	
Analysis of False Turn-On Phenomenon of GaN HEMT with Parasitic Inductances for Propose Novel Design Method Focusing on Peak Gate Voltage	1395
<i>Seiya Ishiwaki, Toshihiro Iwaki, Yusuke Sugihara and Kimihiro Nanamori and Masayoshi Yamamoto Shimane University, Japan; Nagoya University, Japan</i>	
Gate Driver Design Considerations for Silicon Carbide MOSFETs including Series Connected Devices	1402
<i>Samir Hazra, Kasunaidu Vechalapu, Sachin Madhusoodhanan, Subhashish Bhattacharya and Kamalesh Hatua North Carolina State University, United States; Indian Institute of Technology Madras, United States</i>	
Session 40: Electric Vehicle Energy Management	
Chair(s): Kevin Bai, Anand Sathyan	
A Novel Dynamic Demand Control of an Electric Vehicle Integrated in a Solar Nanogrid with Energy Storage	1410
<i>Adamantios Bampoulas and Athanasios Karlis Democritus University of Thrace, Greece</i>	
Stackelberg Game based Energy and Reserve Management for a Fast Electric Vehicle Charging Station	1417
<i>Tianyang Zhao, Xuewei Pan, Shuhan Yao and Peng Wang Nanyang Technology University, Singapore; Harbin Institute of Technology, China</i>	
Multi-Time Scale Forecast for Schedulable Capacity of EVs based on Big Data and Machine Learning	1425
<i>Meiqin Mao, Yangyang Wang, You Yue and Liuchen Chang Hefei University of Technology, China</i>	
Three-Port Bidirectional CLLC Resonant Converter based Onboard Charger for PEV Hybrid Energy Management System	1432
<i>Xiaoying Lu and Haoyu Wang ShanghaiTech University, China</i>	
V2G Bi-directional Battery Charger with Flexible AC/DC Converter	1439
<i>Yaguang Liu, Wenxing Zhong, Haoyuan Weng, Zheqing Li, Min Chen, Changsheng Hu and Dehong Xu Zhejiang University, China</i>	

Session 41: Sensing and Control for Power Converters

Chair(s): Tsai-Fu Wu, Amir Yaznadi

- An Experimental Method for Extracting Stray Inductance of Bus Bars without High Bandwidth Current Measurement** 1446
Ye Jiang, Liqiang Yuan, Zhengming Zhao, Haitao Zhang, Rong Yi, Yali Ding and Wei Gu
Tsinghua University, China; Rongxin Huiko Electric Technology Co., Ltd., China; Anshan Information Engineering School, China
- Comparative Evaluations on Three High Resolution Sampling Schemes for Digital Boundary Control** 1451
Yuanbin He, Chun-tak Lai, Shu-hung Chung and Weimin Wu
Hangzhou Dianzi University, China; City University of Hong Kong, Hong Kong; Shanghai Maritime University, China
- Closed-Loop Control of a Capacitive-Link Universal Converter with Minimum Number of Voltage Sensors** 1457
Masih Khodabandeh and Mahshid Amirabadi
Northeastern University, United States
- Wavelet-based Prognostic-Oriented Temperature Sensing with Sigma-Delta ADCs in Power Applications** 1465
Giorgio Pietrini, Alessandro Soldati, Davide Barater and Carlo Concari
University of Parma, Italy
- Session 42: Modelling and Control of MMC**
- Chair(s): Yongdong Li, Tzung-Lin Lee**
- Delta-Sigma Modulators for Modular Multilevel Converters** 1473
Hao Jiang and Giri Venkataramanan
University of Wisconsin-Madison, United States
- Hybrid Asymmetric Cascaded Multilevel Inverters based on Three- and Nine-Level H-Bridges** 1479
Filipe A. da C. Bahia, Cursino B. Jacobina, Nady Rocha, Italo Roger F.M.P. da Silva, Reuben P.R. de Sousa
Federal University of Campina Grande, Brazil; Federal University of the Paraíba, Brazil; Federal Rural University of Pernambuco, Brazil
- Comparative Study of PES Net and SyCCo Bus: Communication Protocols for Modular Multilevel Converter** 1487
Hao Tu and Srdjan Lukic
North Carolina State University, United States
- Asymmetric Cascaded H-Bridge Topology with 25-Level Output Voltage based on Modular Multilevel DSCC Inverters** 1493
Filipe A. da C. Bahia, Cursino B. Jacobina, Nady Rocha, Italo Roger F.M.P. da Silva
Federal University of Campina Grande, Brazil; Federal University of the Paraíba, Brazil; Federal Rural University of Pernambuco, Brazil
- System-on-Chip Implementation of Embedded Real-Time Simulator for Modular Multilevel Converters** 1500
Mattia Ricco, Marius Gheorghe, Laszlo Mathe and Remus Teodorescu
Aalborg University, Denmark

A Novel Frequency Domain Control Method for Modular Multilevel Converters under Non-Sinusoidal Supply Conditions	1506
Rostan Rodrigues, Jun Li and Herbert L. Ginn III <i>ABB Inc., United States; University of South Carolina, United States</i>	
Modeling and Design of the Modular Multilevel Converter with Parametric and Model-Form Uncertainty Quantification	1513
Niloofer Rashidi Mehrabadi, Rolando Burgos, Dushan Boroyevich and Christopher Roy <i>Virginia Polytechnic Institute and State University, United States</i>	
Decoupled $\alpha\beta$ Model of Modular Multilevel Converter (MMCs)	1521
Yi-Hsun Hsieh and Fred C. Lee <i>Virginia Polytechnic Institute and State University, United States</i>	
Damping Analysis for Transients of Modular Multilevel Converter	1527
Haihao Jiang and Boon-Teck Ooi <i>McGill University, Canada</i>	
Session 43: Control in Microgrids	
Chair(s): Xiaonan Lu, Thomas Podlesak	
Variable Structure Robust Voltage Regulator Design for Microgrid Master-Slave Control	1532
Tong Yao and Raja Ayyanar <i>Arizona State University, United States</i>	
Stability Improvement of Current Control by Voltage Feedforward considering a Large Synchronous Inductance of Diesel Generator	1540
Jongmin Jo and Hanju Cha <i>Chungnam National University, Korea</i>	
Method to Reduce the Circulating Current of Paralleled Inverters with Different Capacities	1545
Xiang Li, Jiawei Chen and Jie Chen <i>Chongqing University, China; Nanjing University of Aeronautics and Astronautics, China</i>	
Novel Hybrid Energy Storage Control for a Single Phase Energy Management System in a Remote Islanded Microgrid	1552
Giovanna Oriti, Alexander L. Julian, Norma Anglani and Gabriel D. Hernandez <i>Naval Postgraduate School, United States; Power Engineering, United States; University of Pavia, Italy; United States Navy, United States</i>	
Dynamic Composite Load Signature Detection and Classification using Supervised Learning over Disturbance Data	1560
Kelly Tray, Phylcia Cicilio, Ted Brekken and Eduardo Cotilla-Sanchez <i>Oregon State University, United States</i>	
A Highly Reconfigurable System Emulator for Testing AC Microgrids	1567
Vijay A.S., Suryanarayana Doolla and Mukul C. Chandorkar <i>Indian Institute of Technology Bombay, India</i>	
An Unsupervised Approach for Disaggregating Major Loads in Small Commercial Buildings	1575
Saman Mostafavi, John Troxler and Robert W. Cox <i>University of North Carolina at Charlotte, United States</i>	

Autonomous Control of Active Power Electronics Loads for Frequency Control of Islanded Microgrid	1582
Guangqian Ding, Song Zhang, Jing Shan, Feng Gao and Xin Gu <i>University of Jinan, China; State Grid of China Technology College, China; State Grid Zaozhuang Power Supply Company, China; Shandong University, China</i>	

Tuesday, October 3

Session 44: Harmonic Compensation Techniques for Microgrids

Chair(s): Dehong Mark Xu, Frede Blaabjerg

A Unified Selective Harmonic Compensation Strategy using DG-Interfacing Inverter in both Grid-Connected and Islanded Microgrid	1588
Qicheng Huang and Kaushik Rajashekara <i>University of Houston, United States</i>	

Active Suppression of Photovoltaic System Related Harmonics in a DC Micro Grid	1594
R. Alsharif , M. Odavic and K. Atallah <i>University of Sheffield, United Kingdom</i>	

A Novel Harmonic Current Sharing Control Strategy for Parallel-Connected Inverters	1602
Yajuan Guan, Josep M. Guerrero, Mehdi Savaghebi, Juan C. Vasquez and Wei Feng <i>Aalborg University, Denmark; Tsinghua University, China</i>	

Harmonic Current Control for LCL-Filtered VSCs Connected to Ultra-Weak Grids	1608
Xiongfei Wang, Dongsheng Yang and Frede Blaabjerg <i>Aalborg University, Denmark</i>	

Session 45: Power Converters for HVDC Grids

Chair(s): Dianguo Xu, Brandon Grainger

Asymmetric Mixed Modular Multilevel Converter Topology in Bipolar HVDC Transmission Systems ...	1615
Jae-Jung Jung, Joon-Hee Lee and Seung-Ki Sul <i>Seoul National University, Korea</i>	

Dynamic Performance and Fault-Tolerant Capability of a TLC-MMC Hybrid DC-DC Converter for Interconnection of MVDC and HVDC Grids	1622
Shenghui Cui, Nils Soltau and Rik W. De Doncker <i>RWTH Aachen University, Germany</i>	

Efficient Modeling of Hybrid MMCs for HVDC Systems	1629
Lei Zhang, Jiangchao Qin, Di Shi and Zhiwei Wang <i>Arizona State University, United States; GEIRI North America, United States</i>	

A New Hybrid Modular Multilevel Converter with Increased Output Voltage Levels	1634
Mahendra B. Ghat, Anshuman Shukla and Ebin Cherian Mathew <i>Indian Institute of Technology Bombay, India; Power Grid Corporation of India Ltd., India</i>	

Session 46: Solid State Transformers

Chair(s): Alex Huang, Rolando Burgos

A Switched-Winding Transformer with Low Quiescent Loss to Meet the Level VI Efficiency Standard at High Power Density 1642

Weston D. Braun, Minjie Chen and David J. Perreault
Massachusetts Institute of Technology, United States; Princeton University, United States

A Winding Method of High Frequency High Voltage Transformer 1649

Junpeng Ji, Xingxia Zhang, Wenjie Chen, Shaoliang An and Xu Yang
Xi'an University of Technology, China; Xi'an Jiaotong University, China

Comparison of Voltage Control Methods of CHB Converters for Power Routing in Smart Transformer 1652

Vivek Raveendran, Giampaolo Buticchi, Marco Liserre and Alessandro Mercante
Christian-Albrechts-Universität zu Kiel, Germany; Wärtsilä Italia S.p.A, Italy

Generalized Average Modeling of DC Subsystem in Solid State Transformers 1659

Jacob A. Mueller and Jonathan W. Kimball
Missouri University of Science and Technology, United States

Session 47: Power Conversion for Solar Photovoltaic Systems III

Chair(s): Wuhua Li, Rajeev Kumar Singh

A Distributed Active and Reactive Power Control Strategy for Balancing Grid-tied Cascaded H-Bridge PV Inverter System 1667

Hamidreza Jafarian, Namwon Kim and Babak Parkhideh
University of North Carolina at Charlotte, United States

Advanced Photovoltaic Inverter Control Development and Validation in a Controller-Hardware-in-the-Loop Test Bed 1673

Kumaraguru Prabakar, Mariko Shirazi, Akanksha Singh and Sudipta Chakraborty
National Renewable Energy Laboratory, United States

DC Link Side Current Control of Inverters based on Integer Programming 1680

O. Salari, A. Nazemi, A. Bakhshai, K. Hashtrudi Zaad and P. Jain
Queen's University, Canada

GaN-based High Gain Soft Switching Coupled-Inductor Boost Converter 1687

Jinia Roy, Yinglai Xia and Raja Ayyanar
Arizona State University, United States; Texas Instruments, United States

Session 48: Multi-Phase AC/DC Converters

Chair(s): Fernando Briz, Norma Anglani

Soft-Switching Parameter Design for an Isolated Three-Phase AC/DC Converter 1694

Kazuma Suzuki, Wataru Kitagawa and Takaharu Takeshita
Nagoya Institute of Technology, Japan

Dynamic and Control Analysis of Modular Multi-Parallel Rectifiers (MMR) 1701

Firuz Zare, Arindam Ghosh, Pooya Davari and Frede Blaabjerg
University of Queensland, Australia; Curtin University, Australia; Aalborg University, Denmark

A Reconfigurable Three- and Single-Phase AC/DC Non-Isolated Bi-Directional Converter for Multiple Worldwide Voltages 1708
Daniel F. Opila, Eun Oh, Keith Kintzley and Jedediah Lomax
United States Naval Academy, United States

High-Frequency Link AC/DC Converter using Matrix Converter with Soft-Switching Technique 1715
Yuto Matsui, Kazuma Suzuki and Takaharu Takeshita
Nagoya Institute of Technology, Japan

Session 49: DC/DC Converters II
Chair(s): Dushan Borojevic, Grant Pitel

A High Gain Non-Isolated Soft-Switching Bidirectional DC-DC Converter with PPS Control 1723
Hyeonju Jeong, Minho Kwon and Sewan Choi
Seoul National University of Science and Technology, Korea

An Investigation on Zero-Voltage-Switching Condition in Synchronous-Conduction-Mode Buck Converter 1728
Chih-Shen Yeh, Xiaonan Zhao and Jih-Sheng Lai
Virginia Polytechnic Institute and State University, United States

Single-Wing Resonant Multilevel Converter Featuring Reduced Number of Resonant Inductors ... 1733
Boris Curuvija, Yanchao Li, Xiaofeng Lyu and Dong Cao
North Dakota State University, United States

Dual Active Bridge with Triple Phase Shift by obtaining Soft Switching in all Operation Range 1739
C. Calderon, A. Barrado, A. Rodriguez, A. Lazaro, C. Fernandez and P. Zumel
Universidad Carlos III de Madrid, Spain

Session 50: Single-Phase Grid Connected Converters
Chair(s): Diego G. Lamar, Andrea Formentini

Trapezium Current Mode (TPCM) Boundary Operation for Single Phase Grid-Tied Inverter 1745
JianTao Zhang, Rene A. Barrera-Cardenas, Takanori Isobe and Hiroshi Tadano
University of Tsukuba, Japan

Leakage Current Suppression and Ripple Power Reduction for Transformer-less Single-Phase Photovoltaic Inverters 1753
Xin Li, Zhongting Tang, Mei Su, Qi Zhu, Yonglu Liu and Yao Sun
Central South University, China

ZVRT Capability of Minimized-LCL-Filter-based Single-Phase Grid-Tied Inverter with High-Speed Gate-Block 1757
Satoshi Nagai, Keisuke Kusaka and Jun-ichi Itoh
Nagaoka University of Technology, Japan

DC to Single-phase AC Grid-Tied Inverter using Buck Type Active Power Decoupling without Additional Magnetic Component 1765
Jun-ichi Itoh, Tomokazu Sakuraba, Hiroki Watanabe and Nagisa Takaoka
Nagaoka University of Technology, Japan

Session 51: Sensorless Methods and State and Parameter Estimation

Chair(s): Yongsug Su, Maurizio Cirrincione

Online Equivalent Series Resistance Estimation Method for Condition Monitoring of DC-Link Capacitors 1773

Sundararajan Prasanth, Mohamed Halick Mohamed, Sathik, Firman Sasongko, Tan Chuan Seng, Mohd Tariq and Rejeki Simanjorang
Nanyang Technological University, Singapore; Rolls-Royce Singapore Pte. Ltd., Singapore

A Novel Current Estimation Technique for Digital Controlled Switching Converters Operating in CCM and DCM 1781

Rajat Channappanavar and Santanu Mishra
Indian Institute of Technology Kanpur, India

Distributed Balancing Control for Modular Multilevel Series/Parallel Converter with Capability of Sensorless Operation 1787

Zhongxi Li, Ricardo Lizana, Angel V. Peterchev and Stefan M. Goetz
Duke University, United States; Universidad Católica de la Santísima Concepción, Chile

A Novel Approach to the Grid Inductance Estimation based on Second Order Generalized Integrators 1794

Javier Moriano, Victor Bermejo, Emilio Bueno, Mario Rizo and Ana Rodriguez
University of Alcalá, Spain; Gamesa Electric, Spain

Session 52: Modeling and Control of Modular Multilevel Converter

Chair(s): Hirofumi Akagi, Navid Zargari

Optimal Submodule Capacitor Sizing for Modular Multilevel Converters with Common Mode Voltage Injection and Circulating Current Control 1802

Ziwei Ke, Jianyu Pan, Karun Potty, William Perdikakis, Arvind Shanmuganaatham, Muneer Al Sabbagh, Julia Zhang, Fang Luo, Jin Wang and Longya Xu
Ohio State University, United States

A New Insertion Index Selection Method to Control Modular Multilevel Converters 1809

Mohammad Sleiman, Luc-André Gregoire, Handy Fortin-Blanchette, Hadi Kanaan and Kamal Al-Haddad
École de Technologie Supérieure, Canada; OPAL-RT Technologies Inc., Canada; Saint-Joseph University, Lebanon

A Modified Circulating Current Suppressing Strategy for Nearest Level Control based Modular Multilevel Converter 1817

Xingxing Chen, Jinjun Liu, Shaodi Ouyang, Shuguang Song and Hongda Wu
Xi'an Jiaotong University, China

Independent Positive- and Negative-Sequence Control for MMC-SAPF with Unbalanced PCC Voltage 1823

Chengjing Li, Ke Dai, Derong Lin, Chen Xu, Cai Chen and Ziwei Dai
Huazhong University of Science and Technology, China; Rensselaer Polytechnic Institute, United States

Session 53: Large Synchronous Machines

Chair(s): Ayman El-Refaie, Mohammad Islam

Design of Field-Oriented-Control-based Brushless, Self-Excited Synchronous Field-Winding Machine with Combined Finite Element/Rectifier Model 1830

Abdi Zeynu and Heath Hofmann
University of Michigan, United States

Analysis of Magnetic Forces and Vibration in a Converter-Fed Synchronous Hydrogenerator 1838

Mostafa Valavi, Arne Nysveen, Roy Nilsen, Jean Le Besnerais and Emile Devillers
Norwegian University of Science and Technology, Norway; EOMYS Engineering, France

Performance Improvement of Simplified Synchronous Generators using an Active Power Filter 1845

Al-Hussein Abu-Jalala, Tom Cox, Chris Gerada, Mohamed Rashed, Tahar Hamiti and Neil Brown
University of Nottingham, United Kingdom; VEDECOM Institute, France; Cummins Power Generation, United Kingdom

Reducing MMF Harmonics and Core Loss Effect of Non-Overlap Winding Wound Rotor Synchronous Machine (WRSM) 1850

Karen S. Garner and Maarten J. Kamper
Stellenbosch University, South Africa

Session 54: Synchronous Reluctance Machines I

Chair(s): Robert D. Lorenz, Dan Ionel

The Loss of Self-Excitation Capability in Stand-Alone Synchronous Reluctance Generators 1857

Maged Ibrahim and Pragasen Pillay
Concordia University, Canada

Reluctance Synchronous Wind Generator Design Optimisation in the Megawatt, Medium Speed Range 1864

Eduan Howard and Maarten J. Kamper
Stellenbosch University, South Africa

Choice of Flux-Barriers Position in Synchronous Reluctance Machines 1872

Giacomo Bacco and Nicola Bianchi
University of Padova, Italy

Investigation of Torque Production and Torque Ripple Reduction Method for 6-Stator/7-Rotor-Pole Variable Flux Reluctance Machines 1880

Beomseok Lee, Z.Q. Zhu and L.R. Huang
University of Sheffield, United Kingdom

Session 55: Sensorless Drives II

Chair(s): Fabio Giulii Capponi, David Diaz Reigosa

Extending Low Speed Self-Sensing via Flux Tracking with Volt-Second Sensing 1888

Yang Xu, Yukai Wang, Ryo Iida and Robert D. Lorenz
University of Wisconsin-Madison, United States; Toshiba Mitsubishi-Electric Industrial, Japan

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Seung-Tae Lee, Young-Kyoun Kim and Jin Hur
Incheon National University, Korea; Osan University, Korea

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D.Q. Guan, D. Xiao, M.X. Bui and M.F. Rahman
University of New South Wales, Australia

Sensorless Commissioning of Synchronous Reluctance Machines Augmented with High Frequency Voltage Injection 1909
Paolo Pescetto and Gianmario Pellegrino
Politecnico di Torino, Italy

Session 56: PM and IPM Motor Drives I

Chair(s): Ramakrishnan Rajavenkitasubramony, Davide Barater

Self-Adaptation of MTPA Tracking Controller for IPMSM and SynRM Drives based on On-Line Estimation of Loop Gain 1917
Nicola Bedetti, Sandro Calligaro and Roberto Petrella
Gefran S.p.A., Italy; Free University of Bozen, Italy; University of Udine, Italy

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Xi Xiao, Shubei Zhang, Youshuang Ding and Yuyang Song
Tsinghua University, China

Enabling Driving Cycle Loss Reduction in Variable Flux PMSMs via Closed-Loop Magnetization State Control 1932
Apoorva Athavale, Daniel J. Erato and Robert D. Lorenz
University of Wisconsin-Madison, United States

Analysis and Design of IPMSM Drive System based on Visualization Technique in Discrete Time Domain 1940
Haoyuan Li, Xing Zhang, Shuying Yang, Fei Li, Jian Yang and Pengpeng Cao
Hefei University of Technology, China

Session 57: GaN Device and Gate Drive

Chair(s): Daniel Costinett, Chenhao Nan

Active Gate Current Control for Non-Insulating-Gate WBG Device 1947
He Li, Yousef M. Abdullah, Chengcheng Yao, Xiaodan Wang and Jin Wang
Ohio State University, United States

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Jianjing Wang, Dawei Liu, Harry C.P. Dymond, Jeremy J.O. Dalton and Bernard H. Stark
University of Bristol, United Kingdom

A 1-MHz Leakage-Compensating Bootstrap Driver for Normally-On Depletion-Mode GaN FET ... 1961
Yoontaek Lee, Sangwoo Han and Jaeha Kim
Seoul National University, Korea; Hongik University, Korea

Applications and Characterization of Four Quadrant GaN Switch 1967
Utkarsh Raheja, Ghanshyamsinh Gohil, Kijeong Han, Sayan Acharya, B. Jayant Baliga, Subhashish Bhattacharya, Michelle Labreque, Peter Smith and Rakesh Lal
North Carolina State University, United States; Transphorm Inc., United States

Session 58: Wide Band Gap Device Reliability

Chair(s): Jerry Hudgins, Tanya Gachovska

Ron Increase in GaN HEMTs – Temperature or Trapping Effects 1975

Jan Böcker, Carsten Kuring, Marvin Tannhäuser and Sibylle Dieckerhoff
Technische Universität Berlin, Germany; Siemens AG, Germany

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Claudiu Ionita, Muhammad Nawaz, Kalle Ilves, and Francesco Iannuzzo
ABB Corporate Research, Sweden; Aalborg University, Denmark

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Moinul Shahidul Haque and Seungdeog Choi
University of Akron, United States

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He Li, Xiao Li, Xiaodan Wang, Jin Wang, Yazan Alsmadi, Liming Liu and Sandeep Bala
Ohio State University, United States; Jordan University of Science and Technology, Jordan; ABB Corporate Research, United States

Session 59: Datacenters and Telecommunication Applications

Chair(s): Xinke Wu, Al-Thaddeus Avestruz

Single-Stage Isolated 48V-to-1.8V Point-of-Load Converter Utilizing an Impedance Control Network for Wide Input Range Operation 2003

Ashish Kumar and Khurram K. Afridi
University of Colorado-Boulder, United States

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Mohamed H. Ahmed, Chao Fei, Virginia Li, Fred C. Lee and Qiang Li
Virginia Polytechnic Institute and State University, United States

A Hybrid AC and DC Distribution Architecture in Data Centers 2017

Alexander Barthelme, Xiwen Xu and Tiefu Zhao
University of North Carolina at Charlotte, United States

Unidirectional Single-Phase AC-DC-AC Three-Level and Two-Level Three-Leg Converters 2023

Nustenil S.M.L. Marinus, Cursino B. Jacobina, Nady Rocha and Reuben P.R. de Sousa
Federal University of Campina Grande, Brazil; Federal Institute of Ceara, Brazil; Federal University of Paraiba, Brazil

Data Center Power Distribution System Reliability Analysis Tool based on Monte Carlo Next Event Simulation Method 2031

Yang Lei and Alex Q. Huang
North Carolina State University, United States

Resonant Filter based Buck Converters with Tunable Capacitor 2036

Ben Guo, Suman Dwari, Lee Yongduk, Joseph Mantese, Brian McCabe, Andy Ritter, Craig Nies, Shashank Priya, Khai Ngo, Lujie Zhang and Rolando Burgos
United Technologies Research Center, United States; AVX Corp., United States; Virginia Polytechnic Institute and State University, United States

An Enhanced Control Scheme for Uninterruptible Power Supply 2043
Jinghang Lu, Mehdi Savaghebi, Baoze Wei and Josep Guerrero
Aalborg University, Denmark

Session 60: Applications of Electric Traction and Propulsion

Chair(s): Bulent Sarlioglu, Suman Debnath

An Accurate Modeling Method for Electric Parameters Prediction of Contactless Slip Ring 2051
Guangming He, Qianhong Chen, Xin Chen and Pingping Xin
Nanjing University of Aeronautics and Astronautics, China

High Power Medium Frequency Power Electronic Traction Transformer based on Bidirectional Z-Source-Alike Impedance Network 2057
Hongbo Li, Zhixue Zhang and Jing Shang
CRRC Zhuzhou Institute Co., Ltd., China

Investigation of the RC-IGBT Application in High Speed Railway Converters 2062
Xianjin Huang, Dengwei Chang, and Trillion Q. Zheng
Beijing Jiaotong University, China

Battery Energy Storage System Integration to the More Electric Aircraft 270 V DC Power Distribution Bus using Peak Current Controlled Dual Active Bridge Converter 2068
Mohd Tariq, Ali I. Maswood, Chandana J. Gajanayake, Amit K. Gupta and Firman Sasongko
Nanyang Technological University, Singapore; Rolls-Royce Singapore Pte. Ltd, Singapore

Research on Excitation Control Method for the Three-Phase Brushless Asynchronous Excitation System of Wound-Field Synchronous Starter/Generators 2074
Zan Zhang, Weiguo Liu, Shuai Mao, Jichang Peng, Chenghao Sun, Tao Meng and Ningfei Jiao
Northwestern Polytechnical University, China

Optimal Gear Ratios Selection for a Nissan Leaf: A Case Study of InGear Transmission System ... 2079
Ahmed S. Abdelrahman, Khalil S. Algarny and Mohamed Z. Youssef
University of Ontario Institute of Technology, Canada

A Novel Hybrid Approach towards Drive-Cycle based Design and Optimization of a Fractional Slot Concentrated Winding SPMSM for BEVs 2086
Philip Korta, Lakshmi Varaha Iyer, Chunyan Lai, Kaushik Mukherjee, Jimi Tjong and Narayan C. Kar
University of Windsor, Canada

Session 61: Multilevel Converters

Chair(s): Sheldon Williamson, Pericle Zanchetta

A Novel Voltage Balance Circuit for Three-Level Diode-Clamped Inverter with Small Inductor 2093
Dongdong Cui, Zhida Zhou, Bo Yang, Qiongquan Ge and Cong Zhao
Institute of Electrical Engineering, CAS, China; University of Chinese Academy of Sciences, China

An Improved Phase-Shifted PWM Method for a Three-Phase Cascaded H-Bridge Multi-Level Inverter 2100
June-Seok Lee, Kyo-Beum Lee and Youngjong Ko
Korea Railroad Research Institute, Korea; Ajou University, Korea; University of Kiel, Germany

- Performance Assessment of the 5-Level 3-Phase Back to Back E-Type Converter** 2106
 Marco Di Benedetto, Alessandro Lidozzi, Luca Solero, Fabio Crescimbinì and Petar J. Grbovic
Roma Tre University, Italy; Huawei Technologies Dusseldorf GmbH, Germany
- Modeling and Voltage Balancing Control for a Hybrid Stacked Five-Level Converter** 2114
 Shuai Xu, Jianzhong Zhang and Xing Hu
Southeast University, China
- Flying Capacitor Resonant Pole Inverter Applying Five Voltage Levels** 2121
 Sjeff J. Settels, Jeroen van Duivenbode, Jorge L. Duarte and Elena A. Lomonova
Eindhoven University of Technology, Netherlands
- Single-Phase AC-DC-AC Multilevel Converter based on H-Bridges and Three-Leg Converters Connected in Series** 2129
 Antonio de P.D. Queiroz, Cursino B. Jacobina, Nayara B. de Freitas, Ayslan C.N. Maia and Victor F.M.B. Melo
Federal University of Campina Grande, Brazil; Federal Institute of Paraíba, Brazil; Federal Institute of Alagoas, Brazil; Federal Institute of Pernambuco, Brazil
- Control Strategy for Modular Multilevel Matrix Converters at High Output Frequencies** 2137
 Dennis Braeckle, Patrick Himmelmann, Mathias Schnarrenberger and Marc Hiller
Karlsruhe Institute of Technology, Germany
- Low-Voltage DC Input, High-Voltage Pulse Generator using Nano-Crystalline Transformer and Sequentially Charged MMC Sub-Modules, for Water Treatment Applications** 2144
 M.A. Elgenedy, A.M. Massoud, D. Holliday, S. Ahmed and B. Williams
University of Strathclyde, United Kingdom; Qatar University, Qatar; Texas A&M University at Qatar, Qatar
- Analysis of a Three Phase Five-Level Dual Tapped Inductor Quasi Impedance Source-Nested Neutral Point Clamped Converter** 2150
 Akinola A. Ajayi-Obe and Azeem Khan
University of Cape Town, South Africa

Session 62: DC/AC Converters

Chair(s): Sewan Choi, Carl Ho

- A Novel Wireless Control Strategy for Input-Series Output-Parallel Inverter System** 2156
 Xiaojian Jiang, Xiaopeng Cao, Liangcai Shu, Guangfu Ning and Wu Chen
Southeast University, China
- Comparative Analysis of Cascaded Inverters based on 5-Level and 3-Level H-Bridges** 2161
 Reuben P.R. Sousa, Cursino B. Jacobina, Filipe A.C. Bahia and Luciano M. Barros
Universidade Federal de Campina Grande, Brazil; Universidade Federal de Sergipe, Brazil
- Differential Power as a Metric to Optimize Power Converters and Architectures** 2168
 José A. Cobos, Helena Cristóbal, Diego Serrano, Regina Ramos, Jesús A. Oliver and Pedro Alou
Universidad Politécnica de Madrid, Spain
- The Phase-Controlled Class-D ZVS Inverter with Current Protection** 2176
 Yudai Nagata, Yuta Yamada, Yoshiki Fukumoto, Tatsuya Ikenari, Xiuqin Wei, Tadashi Suetsugu and Hiroo Sekiya
Chiba University, Japan; DAIHEN Corp., Japan; Chiba Institute of Technology, Japan; Fukuoka University, Japan

Hybrid Open-End Multilevel Six-Phase Machine Drive System with Reduced Harmonic Distortion 2184
Ivan da Silva, Cursino B. Jacobina, Ayslan C.N. Maia, Isaac S. de Freitas and Reuben P.R. Sousa
Federal University of Campina Grande, Brazil; Federal Institute of Alagoas, Brazil; Federal University of Paraiba, Brazil

DVR based on Three-Phase Converter Cascaded by Transformers with Only Two Pairs of Windings 2192
Joao Paulo R.A. Mello and Cursino B. Jacobina
Federal University of Campina Grande, Brazil

Coupled Inductor Implementation Improves Performance of Output Feedback ZVT in Full Bridge Inverters 2200
Yinglai Xia, Chenhao Nan, Siddharth Kulasekaran and Raja Ayyanar
Texas Instruments, United States; Google Inc., United States; Intel Corp., United States; Arizona State University, United States

Hybrid Single-Phase Multilevel Inverter with DC Bypass 2207
Liming Liu
ABB Corporate Research Center, United States

Session 63: DC/DC Converters
Chair(s): Wilson Eberle, Sudip Mazumder

Isolated and Wide Input Ranged Boost Full Bridge DC-DC Converter with Low Loss Active Snubber 2213
Satoshi Ikeda and Fujio Kurokawa
Panasonic Co. Ltd., Japan; Nagasaki Institute of Applied Science, Japan

Multi-Port Isolated LLC Resonant Converter for Distributed Energy Generation with Energy Storage 2219
Kevin Tomas-Manez, Zhe Zhang and Ziwei Ouyang
Technical University of Denmark, Denmark

A New PWM Shoot-through Control Technique to Reduce Switching Losses in Impedance Source DC/DC Converters 2227
Yuba Raj Kafle, Saad Ul Hasan and Graham E. Town
Macquarie University, Australia

An Isolated High-Voltage High-Frequency Pulsed Power Converter for Non-Thermal Plasma Ozone Generation 2232
Changqi You, Mengqi Wang and Jin Ye
University of Michigan-Dearborn, United States; San Francisco State University, United States

Evaluation of Isolated DC/DC Converter Topologies for Future HVDC Aerospace Microgrids 2238
Luca Tarisciotti, Alessandro Costabeber, Chen Linglin, Adam Walker and Mikiel Galea
University of Nottingham, United Kingdom

High-Efficiency High-Bandwidth Switch-Linear Hybrid Envelope-Tracking Power Supply with Slew Rate Split-Band Method 2246
Yang Leng, Xinbo Ruan, Qian Jin and Yazhou Wang
Nanjing University of Aeronautics and Astronautics, China

Quadratic Gain Converter with Output Voltage Ripple Mitigation 2253
Pedro Martin Garcia-Vite, Jesus Elias Valdez-Resendiz, Jonathan Carlos Mayo-Maldonado, Julio Cesar Rosas-Caro, Maria del Rosario Rivera-Espinosa and Antonio Valderrabano-Gonzalez
Instituto Tecnológico de Ciudad Madero, Mexico; Tecnológico de Monterrey, Mexico; Universidad Panamericana Guadalajara, Mexico

High Efficient Multiple-Input Positive Buck-Boost Converter 2260
Jeongtae Kim and Sungwoo Bae
Yeungnam University, Korea; Hanyang University, Korea

Dual Bridge LLC Resonant Converter with Frequency Adaptive Phase-Shift Modulation Control for Wide Voltage Gain Range 2265
S.M. Showybul Islam Shakib, Saad Mekhilef and Mutsuo Nakaoka
University of Malaya, Malaysia

Multiple-input Soft-switching Ćuk Converter 2272
Zhuoya Sun and Sungwoo Bae
Yeungnam University, Korea; Hanyang University, Korea

Session 64: PV Applications

Chair(s): Sonny Xue, Qin Lei

Powerline Communications Strategy Enabling Fully Decentralized Control of AC-Stacked PV Inverters 2277
Daniel Evans and Robert Cox
University of North Carolina at Charlotte, United States

A Simultaneous Voltage and Frequency Control Scheme for Photovoltaic Distributed Generation Units in Small-Scale Power Systems 2285
Hossein Saberi and Shahab Mehraeen
Louisiana State University, United States

Performance and Mitigation Strategy of Distributed AC-Stacked PV Inverter Architecture under Grid Background Harmonics 2291
Namwon Kim, Hamidreza Jafarian, Babak Parkhideh and Johan Enslin
University of North Carolina at Charlotte, United States; Clemson University, South Africa

An Analog MPPT Controller without Multiplier for PV Applications based on Improved P&O Method 2296
Chenxi Wang, Min Chen, Xinghua Zhang and Mingzhi Gao
Zhejiang University, China

An Integrated Single Inductor-Single Sensor based Photovoltaic Optimizer with an Optimal Current Point Tracking Strategy 2301
Tianhua Zhu, Xinlu He, Tong Guan, Feng Wang, Hao Yi and Fang Zhuo
Xi'an Jiaotong University, China

A Regulated Incremental Conductance (r-INC) MPPT Algorithm for Photovoltaic System 2305
Thusitha Randima Wellawatta, Young-Tae Seo, Hong-Hee Lee and Sung-Jin Choi
University of Ulsan, Korea

Dynamic Equivalent Circuit Modelling of Polycrystalline Silicon Photovoltaic Cells	2310
Olufemi I. Olayiwola and Paul S. Barendse <i>University of Cape Town, South Africa</i>	
Modular Cascaded Converter for MVDC-Connected Photovoltaic Systems	2318
Zheng Fan, Guangyao Qiao, Guangfu Ning and Liangcai Shu <i>Global Energy Interconnection Research Institute, China; Southeast University, China</i>	
An Efficient Ramp Rate and State of Charge Control for PV-Battery System Capacity Firming	2323
Amit Kumar Bhattacharjee, Issa Batarseh, Haibing Hu and Nasser Kutkut <i>University of Central Florida, United States; Advanced Charging Technologies, United States</i>	
Analysis of an Interleaved Current-Fed Capacitor-Less DC/AC Converter for PV Systems	2330
Yue Zhang, Zheng Wang and Ming Cheng <i>Southeast University, China</i>	
Session 65: EMI in Power Converters	
Chair(s): Khurram Afridi, Yaow-Ming Chen	
A Galvanic Isolated Voltage Probe for Noise Sources Identification in EMI / EMC Applications	2336
Zhuxian Xu, Chingchi Chen and Richard Kautz <i>Ford Motor Company, United States</i>	
Common Mode EMI Reduction Structure of EV/HEV Inverters for High-Speed Switching	2341
Akinori Okubo, Kraisorn Throngnumchai and Tetsuya Hayashi <i>Nissan Motor Co., Ltd., Japan</i>	
A Layout Method of Passive EMI Filter	2346
Junpeng Ji, Wenjie Chen, Xu Yang, Xingxia Zhang and Na Zhi <i>Xi'an Jiaotong University, China; Xi'an University of Technology, China</i>	
Magnetic Material Selection for EMI Filters	2350
Marcin Kacki, Marek S. Rylko, John G. Hayes and Charles R. Sullivan <i>SMA Magnetics Sp. z o.o., Poland; University College Cork, Ireland; Dartmouth College, United States</i>	
Session 66: Advances in Special Electrical Machines	
Chair(s): Greg Heins, Dan Ionel	
A High Voltage Pulsed Power Supply with Reduced Device Voltage Stress for Industrial Electrostatic Precipitators	2357
Ming Tang, Liangcai Shu, Guangyao Qiao, Guangfu Ning, Wu Chen, Xiaohui Qu and Baojian Ji <i>Southeast University, China; Global Energy Interconnection Research Institute, China; Nanjing University of Technology, China</i>	
Novel Reluctance Axis Shifted Machines with Hybrid Rotors	2362
Hui Yang, Ya Li, Heyun Lin, Z.Q. Zhu, Shukang Lyu, Haitao Wang, Shuhua Fang and Yunkai Huang <i>Southeast University, China; University of Sheffield, United Kingdom</i>	
Electromagnetic Design of an Ultra-High Speed Switched Reluctance Machine over 1 Million RPM	2368
Cheng Gong and Thomas Habetler <i>Georgia Institute of Technology, United States</i>	

Research on the Influence of Rotor Poles Number on Performances of Rotor Permanent-Magnet Flux-Switching Machines 2374
Peng Su, Wei Hua, Chuang Hou and Mingjin Hu
Southeast University, China

Wirelessly Powered Coil-Type Robot with 1D Self-Actuation Capability 2382
Jun Lee and Jung-Ik Ha
Seoul National University, Korea

A Switched Elastance Electrostatic Machine Constructed from Sustainable Elements for Rotational Actuators 2389
Graham Reitz, Bill Butrymowicz, Justin Reed, Baoyun Ge and Daniel C. Ludois
C-Motive Technologies Inc., United States; University of Wisconsin-Madison, United States

A dq-Axis Framework for Electrostatic Synchronous Machines and Charge Oriented Control 2396
Baoyun Ge, Aditya N. Ghule and Daniel C. Ludois
University of Wisconsin-Madison, United States

Session 67: Induction and Permanent Magnet AC Machines
Chair(s): Dong Jiang, Kyo-Beum Lee

State-Space Space-Vector Model of the Induction Motor Including Magnetic Saturation and Iron Losses 2404
Marcello Pucci
ISSIA-CNR, Italy

The Rotor Copper and Iron Loss Analysis of the Inverter-Fed Induction Motor Considering Rotor Slip Frequency 2412
Dongdong Zhang, Haisen Zhao and Thomas Wu
Xian Jiaotong University, China; North China Electric Power University, China; University of Central Florida, United States

GA-based Off-Line Parameter Estimation of the Induction Motor Model Including Magnetic Saturation and Iron Losses 2420
Angelo Accetta, Francesco Alonge, Maurizio Cirrincione, Filippo D'Ippolito, Marcello Pucci and Antonino Sferlazza
ISSIA-CNR, Italy; University of Palermo, Italy; University of South Pacific, Fiji; CNRS, LAAS, France

Simplified Equivalent Model of PMSM with Inter-Turn Fault 2427
Seung-Tae Lee and Jin Hur
Incheon National University, Korea

Analysis of Cogging Torque and Torque Ripple according to Unevenly Magnetized Permanent Magnets Pattern in PMSM 2433
Dong-ho Lee, Chae-lim Jeong and Jin Hur
Incheon National University, Korea

Optimized Design of PMSM with Hybrid Type Permanent Magnet for Improving Performance and Reliability 2439
Chae-Lim Jeong, Young-Kyoun Kim and Jin Hur
Incheon National University, Korea; Osan University, Korea

Reluctance Magnetic Gear and Flux Switching Magnetic Gear for High Speed Motor System	2445
Kohei Aiso, Kan Akatsu and Yasuaki Aoyama <i>Shibaura Institute of Technology, Japan; Hitachi, Ltd., Japan</i>	
Influence of Gear Ratio on Electromagnetic Performance and Geometries of Vernier Permanent Magnet Synchronous Machines	2453
Yue Liu and Z.Q. Zhu <i>University of Sheffield, United Kingdom</i>	
A Family of Vernier Permanent Magnet Machines Utilizing an Alternating Rotor Leakage Flux Blocking Design	2461
Wenbo Liu and Thomas A. Lipo <i>University of Wisconsin-Madison, United States</i>	
Session 68: Motor Drives II	
Chair(s): Giovanna Oriti, Ziaur Rahman	
A Novel Active Common-Noise Canceler Combining Feedforward and Feedback Control	2469
Shunsuke Ohara, Satoshi Ogasawara, Takemoto Masatsugu, Koji Orikawa and Yushin Yamamoto <i>Hokkaido University, Japan; Toshiba Mitsubishi-Electric Industrial Systems Corporation, Japan</i>	
Harmonics Performance and System Stability Evaluation between 18-Pulse and LCL Filter Based Active Front End Converters under Weak Grid Condition	2476
Kevin Lee, Wenxi Yao, Daniel Carnovale and Yuxi Huang <i>Eaton Corporation, United States; Zhejiang University, China</i>	
Harmonic Analysis of a Regulated DC Voltage Space Vector Modulation Technique for High Speed Electrical Drives	2484
Vito Giuseppe Monopoli, Pierluigi Sidella and Francesco Cupertino <i>Politecnico di Bari, Italy</i>	
Distributed Speed Control for Multi-Three Phase Electrical Motors with Improved Power Sharing Capability	2492
A. Galassini, A. Costabeber, C. Gerada and A. Tassarolo <i>University of Nottingham, United Kingdom; University of Trieste, Italy</i>	
Single-Stage Soft-Switching Solid-State Transformer for Bidirectional Motor Drives	2498
Liran Zheng, Rajendra Prasad Kandula, Karthik Kandasamy and Deepak Divan <i>Georgia Institute of Technology, United States</i>	
Session 69: Switching Devices II	
Chair(s): Ruxi Wang, Xiaoqing Song	
Aging Precursors and Degradation Effects of SiC-MOSFET Module under Highly Accelerated Power Cycling Conditions	2506
Haoze Luo, Francesco Iannuzzo, Frede Blaabjerg, Marcello Turnaturi and Emilio Mattiuzzo <i>Aalborg University, Denmark; Vishay Semiconductor Italiana, Italy</i>	
A Measurement Method to Extract the Transient Junction Temperature Profile of Power Semiconductors at Surge Conditions	2512
Yu Du, Rostan Rodrigues and Taosha Jiang <i>ABB Inc., United States</i>	

Lifetime Extension of a Multi-Die SiC Power Module using Selective Gate Driving with Temperature Feed-Forward Compensation 2520
Jeffrey Ewanchuk, Julio Brandelero and Stefan Mollov
Mitsubishi Electric Research Centre Europe, France

Degradation of SiC MOSFETs with Gate Oxide Breakdown under Short Circuit and High Temperature Operation 2527
Vamsi Mulpuri and Seungdeog Choi
University of Akron, United States

The Effect of Load Properties on the Reliability of Machine Drives – The Temperature and Stress Analysis of Power Module Bond Wires 2533
He Niu
General Motors Co., United States

Power Cycling Test of a 650 V Discrete GaN-on-Si Power Device with a Laminated Packaging Embedding Technology 2540
Sungyoung Song, Stig Munk-Nielsen, Christian Uhrenfeldt and Kjeld Pedersen
Aalborg University, Denmark

Gate Driver Design for a High Power Density EV/HEV Traction Drive using Silicon Carbide MOSFET Six-Pack Power Modules 2546
Rui Gao, Li Yang, Wensong Yu and Iqbal Husain
North Carolina State University, United States

Isolation Design Considerations for Power Supply of Medium Voltage Silicon Carbide Gate Drivers 2552
Tushar Batra, Ghanshyam Gohil, Arun Kumar Sesham, Nicholas Rodriguez and Subhashish Bhattacharya
North Carolina State University, United States

An Intelligent Medium Voltage Gate Driver with Enhanced Short Circuit Protection Scheme for 10kV 4H-SiC MOSFETs 2560
Ashish Kumar, Aishwarya Ravichandran, Shrishti Singh, Suyash Shah and Subhashish Bhattacharya
North Carolina State University, United States

Impact of Gate Control on Short-Circuit Capability of SiC/Si based Hybrid Switch 2567
Xi Jiang, Jun Wang, Zongjian Li, Linfeng Deng, Jiwu Lu, Xiaohao Wang, Cheng Zeng and Z. John Shen
Hunan University, China

Session 70: Wireless Power Transfer
Chair(s): Mark J Scott, Jin Wang

A Phase-Shift Soft-Switching Control Strategy for Dual Active Wireless Power Transfer System 2573
Fenghua Liu, Wanjun Lei, Tengbo Wang, Cheng Nie and Yue Wang
Xi'an Jiaotong University, China

Modeling and Experimentation of Multi-Coil Switching Coupler for Wireless Power Transfer Systems 2579
Pingan Tan, Chunxia Liu, Liangwei Ye and Tao Peng
Xiangtan University, China

Analysis and Optimization of 3-Coil Magnetically Coupled Resonant Wireless Power Transfer System for Stable Power Transmission	2584
Weiwei Ye, Lu Chen, Fuxin Liu, Xuling Chen and Xuehua Wang <i>Nanjing University of Aeronautics and Astronautics, China; Huazhong University of Science and Technology, China</i>	
A Double-Frequency Superposition Methodology for High Efficiency and Oriented Power Distribution of MCR WPT System with Two Receivers	2590
Yong Yang, Ze Ding, Fuxin Liu and Xuling Chen <i>Nanjing University of Aeronautics and Astronautics, China</i>	
Resonant Converter with Coupling and Load Independent Resonance for Omnidirectional Wireless Power Transfer Application	2596
Junjie Feng, Minfan Fu, Qiang Li and Fred C. Lee <i>Virginia Polytechnic Institute and State University, United States</i>	
ANN-based Algorithm for Estimation and Compensation of Lateral Misalignment in Dynamic Wireless Power Transfer Systems for EV Charging	2602
Reza Tavakoli and Zeljko Pantic <i>Utah State University, United States</i>	
Comparative Evaluation of Secondary-Side ZVS-PWM Controlled GaN-HFET Resonant Converters for Inductive Power Transfer	2610
Tomokazu Mishima and Eitaro Morita <i>Kobe University, Japan</i>	
Session 71: DC and Hybrid AC/DC Systems	
Chair(s): Meiqin Mao, Adel Nasiri	
Coordinated Control and Optimization of DC Power Systems	2618
Bhanu Babaiahgari, Md. Habib Ullah and Jae-Do Park <i>University of Colorado-Denver, United States</i>	
Controller Design of DC Microgrids with Multiple Sources and Constant Power Loads	2625
Luis Herrera, Benjamin Palmer, Xiu Yao and Bang-Hung Tsao <i>Rochester Institute of Technology, United States; University of Cincinnati, United States; University at Buffalo, United States; University of Dayton Research Institute, United States</i>	
A Study on High-Efficiency Floating Multi-Terminal Power Flow Controller for Next-Generation DC Power Networks	2631
Kenji Natori, Toru Tanaka, Yoshinori Takahashi and Yukihiko Sato <i>Chiba University, Japan</i>	
Operational Cost Reduction Based on Distributed Adaptive Droop Control Technique in DC Microgrids	2638
Mohamed Zaery, Emad M. Ahmed, Mohamed Orabi and Mohamed Youssef <i>Aswan University, Egypt; University of Ontario Institute of Technology, Canada</i>	
Hurst Exponent-based Adaptive Detection of DC Arc Faults	2645
Yousef Abdullah, Boxue Hu, Wei Zhou, Yafeng Wang, Jin Wang and Amin Emrani <i>Ohio State University, United States; Ford Motor Company, United States</i>	

Session 72: Applications of MMC

Chair(s): Dianguo Xu, Maryam Saeedifard

- Impact of DC Fault in Multi-Terminal DC Grid on Connected AC System Stability** 2651
Shuoting Zhang, Yalong Li and Fred Wang
University of Tennessee, United States
- Analysis of Single-Phase-to-Ground Faults at the Valve-Side of HB-MMCs in Bipolar HVDC Systems** 2659
Gen Li, Jun Liang, Fan Ma, Carlos E. Ugalde-Loo, Haifeng Liang and Hui Li
Cardiff University, United Kingdom; Naval University of Engineering, China; North China Electric Power University, China; Beijing Information Science & Technology University, China
- Feedback Linearization Applicable to the State-Space Modelling of an HVDC Terminal based on Modular Multilevel Converter** 2666
Diego A. Montoya-Acevedo, Julian C. Buitrago-Herrera and Andres Escobar-Mejia
Universidad Tecnológica de Pereira, Columbia
- Simulation of Modular Multilevel Converter and DC Grids on FPGA with Sub-Microsecond Time-Step** 2673
Hui Pang, Fei Zhang, Hailong Bao, Géza Joós, Weihua Wang, Wei Li, Luc-Andre Gregoire and Xuebing Zhai
Global Energy Interconnection Research Institute, China; McGill University, Canada; State Grid Shanghai Municipal Electric Power Co., China; OPAL-RT Technologies Inc., Canada
- Interactions between Bandwidth Limited CPLs and MMC based MVDC Supply** 2679
Uzair Javaid, Alexandre Christe, Francisco D. Freijedo and Drazen Dujic
EPFL, Switzerland
- Medium-Voltage DC Grid Connection using Modular Multilevel Converter** 2686
Seyyedmahdi Jafarishiadeh, Mehdi Farasat and Arash Khoshkbar Sadigh
Louisiana State University, United States; Extron Electronics, United States
- A Power Hardware-in-the-Loop-Simulation (P-HILS) System using Two Modular Multilevel DSCC Converters for a Synchronous-Motor Drive** 2692
Kenichiro Saito and Hirofumi Akagi
Tokyo Institute of Technology, Japan
- Switching Function based Analysis of the Modular Multilevel Converter for Low/Medium Voltage Applications** 2700
Josiah O. Haruna, Olorunfemi Ojo and Rere Fatumbi
Tennessee Technological University, United States
- Fast Control of a Modular Multilevel Converter STATCOM using Optimized Pulse Patterns** 2707
Vedrana Spudić and Tobias Geyer
ABB Corporate Research Center, Switzerland
- A Modular Multilevel Converter with Isolated Energy-Balancing Modules for MV Drives Incorporating Symmetrical Six-Phase Machines** 2715
Mohamed S. Diab, B.W. Williams, Derrick Holliday, Ahmed M. Massoud and Shehab Ahmed
University of Strathclyde, United Kingdom; Qatar University, Qatar; Texas A&M University at Qatar, Qatar

Session 73: Batteries and Wireless EV Charging

Chair(s): Veda Prakash Galigekere, Jin Ye

A Star-Structured Switched-Capacitor Equalizer for Series-Connected Battery Strings 2723

Yunlong Shang, Bing Xia, Fei Lu, Chenghui Zhang, Naxin Cui, Chunyu Wang and Chris Mi
Shandong University, China; San Diego State University, United States; University of California-San Diego, United States

A Multiplexing LCL Module using Individual Transmitters for Dynamic Wireless Charging of Electric Vehicles 2728

Shaocong Zhou, Chunbo Zhu, Chunlai Yu and C.C. Chan
Harbin Institute of Technology, China; Heilongjiang Electric Power Research Institute, China

Robust Double D Topology for Roadway IPT Applications 2734

Matthew G.S. Pearce, Hanyu Gao, Amrit Ramadugu, Grant A. Covic and John T. Boys
University of Auckland, New Zealand

A Sorting Balance Control for Battery Sources in a Single Phase Multilevel Inverter 2742

Chun-Yu Yang, Yaow-Ming Chen and Kai-Cheung Juang
National Taiwan University, Taiwan; Industrial Technology Research Institute, Taiwan

Active Cell Balancing Algorithm for Serially Connected Li-Ion Batteries based on Power to Energy Ratio 2748

Geon-Hong Min and Jung-Ik Ha
Seoul National University, Korea

Battery Impedance Measurement using Sinusoidal Ripple Current Emulator 2754

Md. Kamal Hossain, S.M. Rakiul Islam and Sung-Yeul Park
University of Connecticut, United States

A New Magnetic Coupler for EVs Chargers based on Plug-In and IPT Technologies 2760

Emanuel G. Marques, Sandra V. da Silva and A.M.S. Mendes
University of Coimbra/Instituto de Telecomunicações, Portugal

Sensorless Estimation of Coupling Coefficient based on Current and Voltage Harmonics Analysis for Wireless Charging System 2767

Mostak Mohammad and Seungdeog Choi
University of Akron, United States

High Power Density Z-Source Resonant Wireless Charger with Line Frequency Sinusoidal Charging 2773

Hulong Zeng, Xiaorui Wang and Fang Zheng Peng
Michigan State University, United States

Session 74: AC/DC Converters

Chair(s): Wuhua Li, Praveen Jain

Investigation of Power Rectifier under Non-Sinusoidal Input based on Hybrid Multilevel Converter ... 2779

Alan Felinto, Cursino B. Jacobina, Edgard L.L. Fabricio, Victor F.M.B. Melo and João P.R.A. Mello
Federal University of Campina Grande, Brazil; Federal Institute of Paraiba, Brazil; Federal Institute of Pernambuco, Brazil

Series Connected Three-Phase AC-DC Power Converters	2787
Reuben P.R. Sousa, Cursino B. Jacobina and Luciano M. Barros <i>Universidade Federal de Campina Grande, Brazil; Universidade Federal de Sergipe, Brazil</i>	
A Novel Filter Structure to Suppress Harmonic Currents based on the Sequence of Sideband Harmonics	2795
Sungjae Ohn, Hyun-Sam Jung and Seung-Ki Sul <i>Virginia Polytechnic Institute and State University, United States; Seoul National University, Korea</i>	
Asymmetrical Cascaded Three-Phase AC-DC Converters with Injection Transformers	2803
Joao Paulo R.A. Mello and Cursino B. Jacobina <i>Federal University of Campina Grande, Brazil</i>	
Voltage Independence Control of Split-DC Bus for a Three-Phase/Level T-Type Converter with Unbalanced Loads	2811
Wenlong Ding, Jiajun Liu, Bin Duan, Xiangyang Xing and Chenghui Zhang <i>Shandong University, China</i>	
Single-Stage AC-DC Converters Operating with a Resonant Network and Discrete Switching Frequency	2817
Javad Khodabakhsh and Gerry Moschopoulos <i>Western University, Canada</i>	
Capacitor-Isolated Structure with Brightness and Color Controlling for Multicolor LED Strings	2823
Ruihong Zhang, Henry Shu-hung Chung, Xuanlyu Wu, Xiaohua Wu, Xiaobin Zhang and Jinrong Wang <i>Northwestern Polytechnical University, China; City University of Hong Kong, Hong Kong</i>	
Session 75: Modeling and Control of Multilevel Converters	
Chair(s): S. Ali Khajehoddin, Rostan Rodrigues	
An Optimized Neutral-Point Potential Balancing Algorithm for Seven-Level ANPC Inverters	2831
Weihui Sheng and Qiongquan Ge <i>University of Chinese Academy of Sciences, China; Institute of Electrical Engineering, CAS, China</i>	
A Model Predictive Control based Fault-Tolerant Control Strategy for T-Type Three-Level Inverters ...	2839
Jie Chen, Alian Chen, Chenghui Zhang and Ke Li <i>Shandong University, China</i>	
A Repetitive Control Scheme for Circulating Current Suppression in Parallel Three-Level T-Type Inverters under Unbalanced Conditions	2846
Changwei Qin, Alian Chen, Xiangyang Xing, Chunshui Du, Guangxian Zhang, Chenghui Zhang and Wenlong Ding <i>Shandong University, China</i>	
Low Frequency Operation and Comparison Study of 4-Level Hybrid Clamped Converter with Modular Multilevel Converter	2852
Jianyu Pan, Risha Na and Longya Xu <i>Ohio State University, United States</i>	
Control of the Hybrid Cascaded Converter under Unbalanced Conditions	2858
Yu-chen Su, Ping-heng Wu and Po-tai Cheng <i>National Tsing Hua University, Taiwan</i>	

Active Neutral-Point Clamped Five-Level Inverter General Modulation based on Phase-Disposition 2866
Fusheng Wang, Zhen Li, Yilin Lyu, Hang Fu, Fei Li and Hieu Thanh Do
Hefei University of Technology, China; Hung Yen University of Technology and Education, Viet Nam

Mixed Single-Phase Three-Level NPC Inverter with Hybrid Modulation Technology 2873
Liming Liu
ABB Corporate Research Center, United States

Session 76: Modeling and Control of Grid Connected Converters
Chair(s): Jiacheng Wang, Kyo-Beum Lee

Flexible Power Control of Virtual Synchronous Generators under Unbalanced Grid Voltage Conditions 2881
Meng Chen, Xiangning Xiao, Chang Yuan and Shun Tao
North China Electric Power University, China

Visualization Analysis of Grid-Connected Inverter System based on Z-Domain D-Partition Method 2889
Fei Li, Jizhong Xi, Haoyuan Li, Mingyao Ma, Wenxiang Zhou, Peng Liu and Fan Wu
Hefei University of Technology, China

Systematic Control Design for Half-Bridge Converters with LCL Output Filters through Virtual Circuit Similarity Transformations 2895
Korawich Niyomsatian, Piet Vanassche, Ruth V. Sabariego and Johan Gyselinck
KU Leuven, Belgium; Université libre de Bruxelles, Belgium; Triphase NV, Belgium

State Estimation of IEEE 14 Bus with Unified Interphase Power Controller (UIPC) using WLS Method 2903
Mohammad Amin Chitsazan, Mohammad Sami Fadali and Andrzej M. Trzynadlowski
University of Nevada, United States

Control of a Three-Phase Inverter under Unbalanced Grid Conditions 2909
Vikram Roy Chowdhury, Subhajyoti Mukherjee, Pourya Shamsi and Mehdi Ferdowsi
Missouri University of Science and Technology, United States

Three-Phase Short-Circuit Fault Implementation in Converter based Transmission Line Emulator 2914
Shuoting Zhang, Bo Liu, Sheng Zheng, Yiwei Ma, Fred Wang and Leon M. Tolbert
University of Tennessee, United States

Impedance-Phase Reshaping of LCL-filtered Grid-Connected Inverters to improve the Stability in a Weak Grid 2921
Yan Du, Linbo Cui, Xiangzhen Yang, Jianhui Su and Fei Wang
Hefei University of Technology, China; Shanghai University, China

A Control Method to Mimic Synchronous Generator Characteristics for Two-Stage Converters 2927
Jun Zhu, Feng Gao, Xifeng Liu and Jing Xiao
Shandong University, China; Shandong Electric Power Maintenance Company, China

Study on the Inertia Optimization of Grid-friendly Single-Phase Synchronverter 2934
Hong Li, Xiaochao Zhang, Tiancong Shao and Trillion Q. Zheng
Beijing Jiaotong University, China

Predictive Frequency-based Sequence Estimator for Control of Grid-Tied Converters under Highly Distorted Conditions 2940
Cristian Blanco, Pablo García, Ángel Navarro-Rodríguez and Mark Sumnery
University of Oviedo, Spain; University of Nottingham, United Kingdom

Single-Loop All-Pass-Filter-based Active Damping for VSCs with LCL Filters Connected to the Grid ... 2948
Javier Roldán-Pérez, Emilio Bueno, R. Peña-Alzolaz, and Alberto Rodríguez-Cabero
IMDEA Energy Institute, Spain; Alcalá de Henares University, Spain; University of Strathclyde, United Kingdom

Session 77: Power Quality
Chair(s): Xiaoqiang Guo, Feng Gao

Single-Phase Universal Active Power Filter based on Four-Leg AC/DC/AC Converters 2954
Phelipe L.S. Rodrigues, Cursino B. Jacobina, Mauricio B.R. Correa and Italo Roger F.M.P. da Silva
Federal University of Campina Grande, Brazil; Federal Rural University of Pernambuco, Brazil

A Transformer-Less Unified Power Quality Conditioner having Fast Dynamic Control 2962
Sui-pung Cheung, Shun-cheung Yeung, Shu-hung Chung, Wai-lun Lo and Weimin Wu
City University of Hong Kong, Hong Kong; Chu Hai College of Higher Education, Hong Kong; Shanghai Maritime University, China

Application of Singular Value Sensitivity on Harmonic Resonance Analysis for Inverter-based Power Systems 2969
Zhikang Shuai, Yang Li, John Shen and Yi Hong
Hunan University, China; Illinois Institute of Technology, United States

Harmonics Compensation with Constant DC-Capacitor Voltage-Control-based Strategy of Smart Charger for Electric Vehicles in Single-Phase Three-Wire Distribution Feeders under Distorted Source Voltages and Load Currents Conditions 2975
Fuka Ikeda, Kei Nishikawa, Yuki Okamoto, Hiroaki Yamada, Toshihiko Tanaka and Masayuki Okamoto
Yamaguchi University, Japan; Ube College, Japan

Power Quality Improvement Utilizing Photovoltaic Generation Connected to a Weak Grid 2983
Hanny H. Tumbelaka, Eduard Muljadi and Wenzhong Gao
Petra Christian University, Indonesia; National Renewable Energy Laboratory (NREL), United States; University of Denver, United States

A New Control Scheme based on R-APF for Harmonic Power Sharing in Islanded Microgrids 2991
Zhirong Zeng, Hao Yi, Fang Zhuo and Zhenxiong Wang
Xi'an Jiaotong University, China

Performance Evaluation of Shunt-Series Switched Multi-Functional Grid-Connected Inverter for Voltage Regulation 2996
Wooyoung Choi, Woongkul Lee and Bulent Sarlioglu
University of Wisconsin-Madison, United States

A Grid-Voltage-Sensorless Resistive Active Power Filter with Series LC-Filter 3004
Haofeng Bai, Xiongfei Wang and Frede Blaabjerg
Aalborg University, Denmark

Session 78: Stability of Converter Systems

Chair(s): Jian Sun, Xiongfei Wang

A Comprehensive Study on the Gate-Loop Stability of the SiC MOSFET 3012
Xudong Wang, Zhengming Zhao, Yicheng Zhu, Kainan Chen and Liqiang Yuan
Tsinghua University, China

Flexible PFC Control Featuring Adaptive Gain, Mode Estimation, and Dual Feedforward Compensation 3019
Joshua Ivaldi and Sung-Yeul Park
University of Connecticut, United States

A Stability Analysis Method based on Floquet Theory for Multi-stage DC-DC Converters System 3025
Hong Li, Zhongya Guo, Fang Ren, Xiaochao Zhang and Bo Zhang
Beijing Jiaotong University, China; South China University of Technology, China

Stability Enhancement of Single-Loop Inverter-Side Current Feedback Controlled Grid-Connected Inverters with LCL Filters 3030
Teng Liu, Zeng Liu, Jinjun Liu, Yiming Tu and Zipeng Liu
Xi'an Jiaotong University, China

Design of Online Supplementary Adaptive Dynamic Programming for Current Control in Power Electronic Systems 3038
Ujjwol Tamrakar, Naresh Malla, Dipesh Shrestha, Zhen Ni and Reinaldo Tonkoski
South Dakota State University, United States

A Comparative Benchmark of Digital Delay Compensation Techniques based on a Graphical Approach 3044
Minghui Lu, Xiongfei Wang, Poh Chiang Loh, Tomislav Dragicevic and Frede Blaabjerg
Aalborg University, Denmark

Session 79: Other Topics in Control, Modeling and Optimization of Power Converters

Chair(s): Luca Solero, Grant Pitel

Control of a Single Phase Inverter with Multiple Modulation Strategies based on Plant Inversion 3049
R. Ramos, D. Serrano, J.A. Oliver and J.A. Cobos
Universidad Politecnica de Madrid, Spain

Derivation of Transfer Function of LLC Current Resonant Converter using Numerical Calculation 3056
Masahito Shoyama, Takuma Sagara, Yusuke Yamashita, Jun Imaoka, Yu Yonezawa and Yoshiyasu Nakashima
Kyushu University, Japan; Fujitsu Laboratories Ltd., Japan

FPGA-based Direct Repetitive Control for High Performance Ground Power Units 3063
Alessandro Lidozzi, Luca Solero, Fabio Crescimbin, Chao Ji, Stefano Bifaretti and Pericle Zanchetta
Roma Tre University, Italy; Protean Electric Ltd., United Kingdom; University of Roma Tor Vergata, Italy; University of Nottingham, United Kingdom

Interleaved Hybrid Control Concept for Multiphase DC-DC Converters 3069
Georgios Tsolaridis and Juergen Biela
ETH Zurich, Switzerland

Active Damping of Power Converters with Modular Basic Crossover Correction Cells	3077
V. Spinu, R.B. Dai, M. Lazar, J.L. Duarte <i>Eindhoven University of Technology, Netherlands</i>	
Training Neural-Network-based Controller on Distributed Machine Learning Platform for Power Electronics Systems	3083
Wenguan Wang, Henry Shu-hung Chung, Ralph Cheng, C.S. Leung, Xiaoqing Zhan, Alan Wai-lun Lo, J. Kwok, Chun Jason Xue and Jun Zhang <i>City University of Hong Kong, Hong Kong; Chu Hai College of Higher Education, Hong Kong; Hong Kong University of Science and Technology, Hong Kong; South China University of Technology, China</i>	
FPGA Implementation of a Real-Time Model Predictive Controller for Hybrid Power Systems	3090
Seyed Ata Raziei and Zhenhua Jiang <i>University of Dayton, United States</i>	
Equivalent Circuit Model for Modular High Voltage Power Generation Architectures	3098
Saijun Mao, Jelena Popovic, Jan Abraham Ferreira, Chengmin Li and Wuhua Li <i>Delft University of Technology, Netherlands; Zhejiang University, China</i>	
Improved Delayed Signal Cancellation-based SRF-PLL for Unbalanced Grid	3103
Tuomas Messo, Jussi Sihvo, Dongsheng Yang, Xiongfei Wang and Frede Blaabjerg <i>Tampere University of Technology, Finland; Aalborg University, Denmark</i>	
Session 80: Analysis Techniques in Electrical Machines	
Chair(s): Peter Wung, Wei Xu	
Numerical and Experimental Evaluation of Magnetostriction and Magnetic Forces on Transformer Stacks and Joints for the Assessment of Core Vibrations	3111
Jan Rens, Sigrid Jacobs, Maarten Van Poucke and Emmanuel Attrazic <i>ArcelorMittal Global R&D, Belgium; ArcelorMittal Saint Chely d Apcher, France</i>	
Reliability Analysis of an Adaptive Third-Harmonic Differential Voltage Stator Ground Fault Protection Scheme using a Lab-Scale Generating Station	3119
Amir Negahdari, Khaled Al Jaafari, Hamid A. Toliyat, Nader Safari-Shad and Russ Franklin <i>Texas A&M University, United States; Petroleum Institute, United Arab Emirates; University of Wisconsin-Platteville, United States; Alliant Energy, United States</i>	
An Improved Core-Loss Calculation Method for Doubly Salient Electromagnetic Motor	3125
Wanying Jia, Lan Xiao, Hongfei Wu and Deming Zhu <i>Nanjing University of Aeronautics and Astronautics, China; Electronic Technology Institute, China</i>	
Damper Current Analysis of Hydro-Generators Considering Interbar Currents	3130
Yang Zhan, Kangkang Kong, Guorui Xu and Haisen Zhao <i>North China Electric Power University, China</i>	
Active Cooling for On-Machine Device	3137
Xikai Sun, Paul J. Grosskreuz and Mark R. Cooper <i>Rockwell Automation, China; Rockwell Automation, United States</i>	
Improved Analytical Modeling of High Frequency Conductive Losses in Isolated Rectangular Conductor	3145
Xiaohui Wang, Li Wang, Ling Mao and Yaojia Zhang <i>Nanjing University of Aeronautics and Astronautics, China</i>	

Nonlinear Analytical Model of an Inductance Considering Saturation and Temperature Variation 3150

Hilmi Gurleyen, Erkan Mese, Ju Hyung Kim and Bulent Sarlioglu

Yildiz Technical University, Turkey; Ege University, Turkey; University of Wisconsin-Madison, United States

Session 81: AC Electrical Machines: Performance Estimation

Chair(s): Avoki Omekanda, Ronghai Qu

Detection and Estimation of High-Resistance Connection for Inverter-Fed Permanent Magnet Synchronous Machine Drives 3155

Jun Hang, Shichuan Ding, Hao Li and Qunjing Wang

Anhui University, China

A Model-based Signal Processing Method for Fault Diagnosis in PMSM Machine 3160

Mehrdad Heydarzadeh, Mohsen Zafarani, Enes Ugur, Bilal Akin and Mehrdad Nourani

University of Texas at Dallas, United States

Separation of Induction Motor Rotor Faults and Low Frequency Load Oscillations through the Radial Leakage Flux 3165

Taner Goktas, Muslum Arkan, M. Salih Mamis and Bilal Akin

Inonu University, Turkey; University of Texas at Dallas, United States

Efficiency Estimation of Induction Machines using Nonintrusive No-Load Low Voltage Test 3171

M. Aminu, P. Barendse and A. Khan

University of Cape Town, South Africa

Assembly Effects on Stator Cores of Small Synchronous Reluctance Motors 3179

Zbigniew Gmyrek and Andrea Cavagnino

Lodz University of Technology, Poland; Politecnico di Torino, Italy

Analysis of Stator/Rotor Pole Combinations in Variable Flux Reluctance Machines using Magnetic Gearing Effect 3187

L.R. Huang, Z.Q. Zhu, J.H. Feng, S.Y. Guo, J.X. Shi and W.Q. Chu

Sheffield University, United Kingdom; CRRC Zhuzhou Institute Co. Ltd., China

Methods for d-/q-Axis Saturation Stator-to-Rotor Mutual inductance of Salient-Pole Synchronous Machine 3195

Hongyu Wang

Ohio State University, United States

Influence of Magnetoresistance and Temperature on Permanent Magnet Condition Estimation Methods using High Frequency Signal Injection 3201

Daniel Fernandez Alonso, David Reigosa, Maria Martinez, Juan Guerrero and Fernando Briz

University of Oviedo, Spain

Stator Inductance Estimation for Permanent Magnet Motors Using the PWM Excitation 3208

Ramakrishnan Raja, Tomy Sebastian, Mengqi Wang and Mazharul Chowdhury

Halla Mechatronics, United States; University of Michigan-Dearborn, United States

Session 82: Component Technologies

Chair(s): Ben Guo, Tsorng-Juu Liang

Reduction of the Parasitic Capacitance of a Power Inductor through Conductors Placement 3215

Shushu Zhu, Xibo Yuan and Phil Mellor

Nanjing University of Aeronautics and Astronautics, China; University of Bristol, United Kingdom

A Half-Turn Winding for Compact, High-Current, High-Turns-Ratio, Low-Leakage-Inductance Transformer 3222

K.V. Iyer, M. Cai, D. Murthy-Bellur, B. Palmer and N. Mohan

Cummins Inc., United States; University of Minnesota, United States; Purdue University, United States

Power Loss Evaluation for Active and Magnetic Components in a SiC MOSFET-based Power Electronic System 3228

Yi Deng, Zach Pan, Harish Suryanarayana, Arun Kadavelugu, Liming Liu, Christopher Belcastro and Esa-Kai Paatero

ABB Corporate Research Center, United States; ABB Power Solutions, United States; ABB Oy, Finland

A Method for Hotspot Temperature Estimation of Aluminum Electrolytic Capacitors 3235

Holger Jedtberg, Giampaolo Buticchi, Marco Liserre and Huai Wang

Kiel University, Germany; Aalborg University, Denmark

Effect of Conductive Magnetic Field Concentrators on the Performance of Anisotropic Magnetoresistors in High Frequency Contactless Current Sensing 3242

Shahriar Jalal Nibir and Babak Parkhideh

University of North Carolina at Charlotte, United States

Optimized Design for Three Port Transformer Considering Leakage Inductance and Parasitic Capacitance 3247

Ritwik Chattopadhyay, Mark A. Juds, Ghanshyamsinh Gohil, Srinivas Gulur, Paul R. Ohodnicki and Subhashish Bhattacharya

North Carolina State University, United States; Eaton Corporate Research and Technology, United States; National Energy Technology Laboratory, United States

A Tunable Inductor based on a Magnetic Flux Valve 3255

Junwei Cui, Haosen Wang, Liyan Qu and Wei Qiao

University of Nebraska-Lincoln, United States

Session 83: Renewable Energy and Grid Integration

Chair(s): Dehong Mark Xu, Yilmaz Sozer

An Adaptive DC-Bus Stabilizer for Single-Phase Grid-Connected Renewable Energy Source System 3260

Rong Zeng, Zhiqiang Wang and Madhu Sudhan Chinthavali

Oak Ridge National Laboratory, United States

Phase Stability Enhancement in big Power Networks using Renewable Generation Units Controlled by SPC 3266

Mostafa Abdollahi, Jose Ignacio Candela, Joan Rocabert, Raul Santiago Munoz Aguilar and Juan Ramon Hermoso

Technical University of Catalonia, Spain

Single-Phase to Three-Phase Generation System based on Doubly-Fed Induction Generator	3274
Nady Rocha, Ítalo A. Cavalcanti de Oliveira, Edison Roberto Cabral da Silva and Cursino Brandao Jacobina <i>Federal University of Paraíba, Brazil; Federal University of Campina Grande, Brazil</i>	
Wind Energy Conversion System based on DFIG with Series Grid Side Converter without Transformer	3281
Italo A. Cavalcanti de Oliveira, Nady Rocha, Edison Roberto Cabral da Silva, Luanna M. Silva de Siqueira, Ely Cavalcanti de Menezes and Cursino Brandao Jacobina <i>Federal University of Paraíba, Brazil; Federal University of Campina Grande, Brazil</i>	
Sensorless HCS MPPT Based Control Strategy for the DPF-WECS	3289
Ying Zhu, Jun Hang, Haixiang Zang and Jingtao Zhao <i>Hohai University, China; Anhui University, China; NARI Technology Development Co., Ltd., China</i>	
Impedance Modeling and Control of STATCOM for Damping Renewable Energy System Resonance	3295
Yang Zhang, Xin Chen and Jian Sun <i>Nanjing University of Aeronautics and Astronautics, China; Rensselaer Polytechnic Institute, United States</i>	
Modeling, Analysis and Parameters Design of Rotor Current Control in DFIG-based Wind Turbines for Dynamic Performance Optimizing	3303
Yuanzhu Chang and Jiabing Hu <i>Huazhong University of Science and Technology, China</i>	
Predictive Voltage Control of Direct Matrix Converter with Reduced Number of Sensors for the Renewable Energy and Microgrid Applications	3309
Jianwei Zhang, Li Li, Zahra Malekjamshidi and David G. Dorrell <i>University of Technology Sydney, Australia; University of KwaZulu-Natal, South Africa</i>	

Wednesday, October 4

Session 84: Wind Energy Systems

Chair(s): Dinesh Kumar, Wei Qiao

Field Excitation Scheme using a Machine-Side 4-Leg Converter in MW-Range WRSG Wind Turbine Systems	3316
Yongsug Suh and Thomas A. Lipo <i>Chonbuk National University, Korea; University of Wisconsin-Madison, United States</i>	
Modeling and Control of Interconnected Wind Turbine Drivetrains	3324
Mohsen Farbood, Elaheh Taheran Fard, Mokhtar Sha-Sadeghi, Afshin Izadian and Taher Niknam <i>Shiraz University of Technology, Iran; Purdue School of Engineering and Technology, United States</i>	
Medium Voltage Power Conversion Architecture for High Power PMSG based Wind Energy Conversion System (WECS)	3329
Sayan Acharya, Samir Hazra, Kasunaidu Vechalapu and Subhashish Bhattacharya <i>North Carolina State University, United States</i>	
A Universal Multiple-Vector-based Model Predictive Direct Power Control for Doubly Fed Induction Generators	3337
Yongchang Zhang, Donglin Xu and Dong Jiang <i>North China University of Technology, China; Huazhong University of Science and Technology, China</i>	

Session 85: Droop Control in Microgrids

Chair(s): Sara Ahmed, Amir Yaznadi

Breaking the Boundary: A Droop and Master-Slave Hybrid Control Strategy for Parallel Inverters in Islanded Microgrids 3345

Shike Wang, Zeng Liu, Jinjun Liu, Ronghui An and Meng Xin
Xi'an Jiaotong University, China

Hybrid Impedance-based Modelling and Stability Analysis of IMG-PICDPS 3353

Meiqin Mao, Yong Ding, Yatao Shen and Liuchen Chang
Hefei University of Technology, China

A Hybrid Adaptive Droop Control Technique with Embedded DC-Bus Voltage Regulation for Single-Phase Microgrids 3359

Sajjad M. Kaviri, Hadis Hajebrahimi, Majid Pahlevani, Praveen Jain and Alireza Bakhshai
Queen's University, Canada; University of Calgary, Canada

Enforcing Coherency in Droop-Controlled Inverter Networks through use of Advanced Voltage Regulation and Virtual Impedance 3367

Philip J. Hart, R.H. Lasseter and T.M. Jahns
University of Wisconsin-Madison, United States

Session 86: Grid Connected Converter Stability

Chair(s): Johan HR Enslin, Suryanarayana Doolla

Stabilization of Grid-Connected Inverter System with Feed-Forward Control 3375

Toshiji Kato, Kaoru Inoue and Yusuke Nakajima
Doshisha University, Japan

Impedance-based Stability Criterion for Multiple Offshore Inverters Connected in Parallel with Long Cables 3383

Xin Zhang, Henry Shu-Hung Chung, Ling Ling Cao, Jeff Po Wa Chow and Weimin Wu
Nanyang Technological University, Singapore; City University of Hong Kong, Hong Kong; Hong Kong Polytechnic University, Hong Kong; Shanghai Maritime University, China

DAH-FF Approach to Improve the Current Quality and Stability of the LCL Type Grid-Connected Inverter 3390

Xin Zhang, Henry Shu-hung Chung, Yuan-Bin He, Chun-Tak Lai and Weimin Wu
Nanyang Technological University, Singapore; City University of Hong Kong, Hong Kong; Hangzhou Dianzi University, China; Shanghai Maritime University, China

Power Factor Correction Capacitors for Multiple Parallel Three-Phase ASD Systems: Analysis and Resonance Damping 3398

Yongheng Yang and Frede Blaabjerg
Aalborg University, Denmark

Session 87: Control and Modulation of Multi-Phase AC/DC Converters

Chair(s): Adam Skorek, Dong Cao

Direct Power Control of PWM Rectifier with Elimination of DC Voltage Oscillations and Current Harmonics under Unbalanced Network 3405

Yongchang Zhang, Jie Liu, Jihao Gao and Haitao Yang
North China University of Technology, China; University of Technology Sydney, Australia

Improved SVPWM Schemes for Vienna Rectifiers without Current Distortion	3410
Houjian Xu, Wenxi Yao and Shuai Shao <i>Zhejiang University, China</i>	
Improved Eight-Segment PWM Scheme with Non-Equally Distributed Zero-Vector Intervals for a Three-Phase Isolated Buck Matrix-Type Rectifier	3415
Jahangir Afsharian, Dewei Xu, Bin Wu, Bing Gong and Zhihua Yang <i>Ryerson University, Canada; Murata Power Solution, Canada</i>	
A Modified SVPWM Strategy Applied to a Three-Phase Three-Port Bidirectional AC-DC Rectifier for Efficiency Enhancement	3420
Hongfei Wu, Tingting Liu, Tianyu Yang, Jiangfeng Wang, Shun Ding and Yan Xing <i>Nanjing University of Aeronautics and Astronautics, China</i>	
Session 88: DC/DC Converter Topologies	
Chair(s): Regan Zane, Wilson Eberle	
High Efficiency LC Resonant Boost Topology: Analysis and Design	3427
Hamed Valipour and Martin Ordonez <i>University of British Columbia, Canada</i>	
A Zero-Voltage Switching, Physically Flexible Multilevel GaN DC-DC Converter	3433
Derek Chou, Yutian Lei and Robert C.N. Pilawa-Podgurski <i>University of Illinois at Urbana-Champaign, United States</i>	
A Switched-Capacitor based High Conversion Ratio Converter for Renewable Energy Applications: Principle and Generation	3440
Kerui Li, Zhijian Yin, Yongheng Yang, Huai Wang and Frede Blaabjerg <i>Aalborg University, Denmark</i>	
Design of Very-High-Frequency Synchronous Resonant DC-DC Converter for Variable Load Operation	3447
Lei Gu, Wei Liang and Juan Rivas Davila <i>Stanford University, United States</i>	
Session 89: AC-AC Converters I	
Chair(s): Junichi Itoh, Lee Empringham	
A Ride-Through Method using Input-Filter Capacitors for Three-Level Indirect Matrix Converter based Open-End Winding Drive	3455
Santhosh Krishnamoorthi, Saurabh Tewari, Siddharth Raju, Abhijit Kshirsagar, Daniel Opila and Ned Mohan <i>University of Minnesota, United States; MTS Systems Corporation, United States; United States Naval Academy, United States</i>	
A Family of Highly Reliable and Efficient Inductive-Link Universal Power Converters	3462
Khalegh Mozaffari and Mahshid Amirabadi <i>Northeastern University, United States</i>	
Matrix Converter Open Circuit Fault Diagnosis with Asymmetric One Zero SVM	3470
Jiawei Zhang, Lee Empringham, Liliana De Lillo, Hanbing Dan and Patrick Wheeler <i>University of Nottingham, United Kingdom</i>	

A Versatile Inductive-Link Three-Phase Converter Topology 3476

Khalegh Mozaffari and Mahshid Amirabadi
Northeastern University, United States

Session 90: Reliability, Diagnostic, and Faults Analysis in Power Converters I
Chair(s): Ke Ma, Marco Liserre

An Active Capacitor with Self-Power and Internal Feedback Control Signals 3484

Haoran Wang and Huai Wang
Aalborg University, Denmark

Impacts of Rotor Current Control Targets on DC-Link Capacitor Lifetime in DFIG-based Wind Turbine during Grid Voltage Unbalance 3489

Holger Jedtberg, Marius Langwasser, Rongwu Zhu, Giampaolo Buticchi and Marco Liserre
Christian-Albrechts-Universität zu Kiel, Germany

Aging Assessment of Discrete SiC MOSFETs under High Temperature Cycling Tests 3496

Enes Ugur and Bilal Akin
University of Texas at Dallas, United States

Live Condition Monitoring of Switching Devices using SSTDR Embedded PWM Sequence: A Platform for Intelligent Gate-Driver Architecture 3502

Sourov Roy and Faisal Khan
University of Missouri-Kansas City, United States

Session 91: Design Optimization of Power Converters
Chair(s): Fred Wang, Arijit Banerjee

Efficiency Optimization of DC-DC Solid State Transformer based on Modular Multilevel Converters 3508

Lei Zhang, Zhe Zhao and Jiangchao Qin
Arizona State University, United States

Mission-Profile based Multi-Objective Optimization of Power Electronics Converter for Wind Turbines 3514

Ghanshyamsinh Gohil, Remus Teodorescu, Tamas Kerekes, Frede Blaabjerg and Subhashish Bhattacharya
North Carolina State University, United States; Aalborg University, Denmark

Reducing Reverse Conduction and Switching Losses in GaN HEMT-based High-Speed Permanent Magnet Brushless DC Motor Drives 3522

Woongkul Lee, Di Han, Wooyoung Choi and Bulent Sarlioglu
University of Wisconsin-Madison, United States

Design by Optimization Methodology: Application to a Wide Input and Output Voltage Ranges Interleaved Buck Converter 3529

Mylène Delhommais, Jean-Luc Schanen, Frédéric Wurtz, Cécile Rigaud and Sylvain Chardon
Université Grenoble Alpes, France; TRONICO-ALCEN, France

Session 92: Thermal and Faults of Electric Machines

Chair(s): Yilmaz Sozer, Sang Bin Lee

An Enhanced Active DC-Flux Injection based Approach for Thermal Monitoring of Induction Machines with Direct Torque Control Schemes 3537

Sufei Li, Shen Zhang, Chen Jiang, Lijun He and Ronald G. Harley
Georgia Institute of Technology, United States; General Electric, United States; University of KwaZulu-Natal, South Africa

Comparison of Thermal Stresses Developed during Transients on a Damaged Rotor Cage 3545

Vicente Climente-Alarcon, Antero Arkkio and Jose A. Antonino-Daviu
Aalto University, Finland; Universitat Politecnica de Valencia, Spain

A High-Frequency Torque Injection-Based Rotor Thermal Monitoring Scheme for Direct-Torque-Controlled Interior Permanent Magnet Synchronous Machines 3552

Shen Zhang, Sufei Li, Lijun He, José A. Restrepo and Thomas G. Habetler
Georgia Institute of Technology, United States; GE Global Research, United States; Universidad Simón Bolívar, Venezuela

Evaluation of the Detectability of Rotor Faults and Eccentricities in Induction Motors via Transient Analysis of the Stray Flux 3559

Jose Antonino-Daviu, Alfredo Quijano-Lopez, Vicente Climente-Alarcon and Hubert Razik
Universitat Politecnica de Valencia, Spain; Aalto University, Finland; Université Claude Bernard Lyon 1, France

Session 93: PM Machines and Windings

Chair(s): Abraham Gebregergis, Greg Heins

Preliminary Study on Differences in the Performance Characteristics of Concentrated and Distributed Winding IPM Machines with Different Rotor Topologies 3565

Alireza Pouramin, Rukmi Dutta and M.F. Rahman
University of New South Wales, Australia

Shaft-to-Frame Voltage Mitigation Method by Changing Winding-to-Rotor Parasitic Capacitance of IPMSM 3571

Jun-Kyu Park, Se-Hyun Rhyu and Jin Hur
Korea Electronics Technology Institute (KETI), Korea; Incheon National University, Korea

Current Control Strategy for Dynamic Winding Reconfiguration of a Brushless DC Motor 3577

Florian Copt, Douglas Martins Araujo, Christian Koechli and Yves Perriard
EPFL, Switzerland

Design and Analysis of a Low Cost and High Power Density PM-Assisted Synchronous Reluctance Machine for Automotive Electric Power Management 3583

Lei Hao, Murali Pandi, Chandra Mavuru, Chandra Namuduri, Avoki Omekanda and Thomas Nehl
General Motors R&D Center, United States; General Motors India Technical Center, India

Session 94: Energy Efficient Motor Drives

Chair(s): Sayeed Mir, Gui-Jia Su

Open-Ended Induction Motor Drive with a Floating Capacitor Bridge at Variable DC Link Voltage 3591

Albino Amerise, Michele Mengoni, Luca Zarrì, Angelo Tani, Sandro Rubino and Radu Bojoi
University of Bologna, Italy; Politecnico di Torino, Italy

Dynamic Loss Minimization Control of Linear Induction Machine	3598
Dong Hu, Wei Xu, Renjun Dian, Yi Liu and Jianguo Zhu <i>Huazhong University of Science and Technology, China; University of Technology Sydney, Australia</i>	
Dynamic Loss Minimizing Control of a PM Servomotor Operating Even at the Voltage Limit when using DB-DTFC	3604
Huthaifa Flieh, Robert D. Lorenz, Eigo Totoki, Shinichi Yamaguchi and Yuichiro Nakamura <i>University of Wisconsin-Madison, United States; Mitsubishi Electric Corp., Japan</i>	
Comparison of Postfault Control Strategies in Terms of Converter Losses for Dual Three-Phase Machines	3612
Fernando Baneira, Jesús Doval-Gandoy, Alejandro G. Yepes, Óscar López and Diego Pérez-Estévez <i>University of Vigo, Spain</i>	
Session 95: Induction Motor Drives	
Chair(s): Marcello Pucci, Jingbo Liu	
A Three-Dimensional Predictive Current Trajectory Control Method for Open-End Winding Induction Motor	3620
Bohang Zhu and Kaushik Rajashekara <i>University of Texas at Dallas, United States; University of Houston, United States</i>	
Comparison of Steady-State Induction Motor-Drive Efficiency Control Schemes	3626
Andrew Strandt and Lixiang Wei <i>Rockwell Automation, United States</i>	
Model Predictive Direct Flux Vector Control of Multi Three-Phase Induction Motor Drives	3633
S. Rubino, R. Bojoi, S.A. Odhano and P. Zanchetta <i>Politecnico di Torino, Italy; University of Nottingham, United Kingdom</i>	
Open-End Six-Phase Machine Drive System with Six Three-Leg Converters	3641
Nayara B. de Freitas, Cursino B. Jacobina, Victor F.M.B. Melo, Bruna S. Gehrke and Louelson A.L. de A.C. Costa <i>Federal University of Campina Grande, Brazil; Federal Institute of Pernambuco, Brazil</i>	
Session 96: Packaging I	
Chair(s): Jelena Popovic, Zhuxian Xu	
Bonding of Large Substrates by Silver Sintering and Characterization of the Interface Thermal Resistance	3649
Shan Gao, Zhenwen Yang, Yansong Tan, Xin Li, Xu Chen, Zhan Sun and Guo-Quan Lu <i>Virginia Polytechnic Institute and State University, United States; Tianjin University, China; Harbin Institute of Technology, China</i>	
A High Power-Density and High Efficiency Insulated Metal Substrate based GaN HEMT Power Module	3654
Juncheng Lu, Di Chen and Lyubov Yushyna <i>GaN Systems Inc., Canada</i>	
A High Power Density Multichip Phase-Leg IGBT Module with Void-Free Die Attachment using Nanosilver Paste	3659
Shancan Fu, Yunhui Mei, Xin Li and Guo-Quan Lu <i>Tianjin University, China; Virginia Polytechnic Institute and State University, United States</i>	

Paralleling 650 V/ 60 A GaN HEMTs for High Power High Efficiency Applications 3663
Nidhi Haryani, Jun Wang and Rolando Burgos
Virginia Polytechnic Institute and State University, United States

Session 97: LED Drivers

Chair(s): S. Ali Khajehoddin, Marcos Alonso

Application of Artificial Neural-Network to Control the Light of Multi-Color LED System 3669
Xiaoqing Zhan, Wenguan Wang and Henry Shu-hung Chung
City University of Hong Kong, Hong Kong

GaN-based High-Power-Density Electrolytic-Free Universal Input LED Driver 3676
Saad Pervaiz, Ashish Kumar and Khurram K. Afridi
University of Colorado-Boulder, United States

Forward-Flyback Converter for LED Driving with Reduced Number of Components 3684
Jong-Woo Kim, Jung-Muk Choe and Jih-Sheng Lai
Virginia Polytechnic Institute and State University, United States

High Frequency DC-DC AC-LED Driver based on ZCS-QRCs 3688
Ignacio Castro, Sergio Lopez, Kevin Martin, Manuel Arias, Diego G. Lamar and Javier Sebastian
University of Oviedo, Spain

Session 98: Wind Energy Applications

Chair(s): Nathan Weise, Eduard Muljadi

Wind Turbine Bearing Fault Diagnosis based on Sparse Representation of Condition Monitoring Signals 3696
Jun Wang, Wei Qiao and Liyan Qu
University of Nebraska-Lincoln, United States

Performance Evaluation of Slip Couplers with Spoke- and Surface-Mounted PM for Wind Energy Applications 3703
N. Dumakude and M.J. Kamper
Stellenbosch University, South Africa

Small Signal Modeling of Wind Farms 3710
Esmail Ebrahimzadeh, Frede Blaabjerg, Xiongfei Wang, Claus Leth Bak, Torsten Lund, Gert K. Andersen, Carlos Gómez Suárez and Jens-Jacob Berg
Aalborg University, Denmark; Vestas Wind Systems A/S, Denmark

Battery-Free Power Management Circuit for Impact-Type Micro Wind Piezoelectric Energy Harvester 3717
Nan Chen and Tingcun Wei
Northwestern Polytechnical University, China

Session 99: Power Sharing Techniques in Microgrids

Chair(s): Koji Orikawa, Josep M. Guerrero

A Proportional Harmonic Power Sharing Scheme for Hierarchical Controlled Microgrids Considering Unequal Feeder Impedances and Nonlinear Loads 3722
Hong Li, Yang Han, Ping Yang, Jingqi Xiong, Congling Wang and Josep M. Guerrero
University of Electronic Science and Technology of China, China; Aalborg University, Denmark

Adaptive Synchronous Reference Frame Virtual Impedance Controller for Accurate Power Sharing in Islanded AC-Microgrids: A Faster Alternative to the Conventional Droop Control 3728
Carlos Andres Macana and Hemanshu R. Pota
University of New South Wales, Australia

Decentralized Economical-Sharing Scheme for Cascaded AC Microgrids 3736
Lang Li, Huawen Ye, Zhangjie Liu, Hua Han, Yao Sun and Mei Su
Central South University, China

Using Consensus Control for Reactive Power Sharing of Distributed Electric Springs 3741
Jie Chen, Shuo Yan and S.Y. Ron Hui
University of Hong Kong, Hong Kong; Imperial College London, United Kingdom

Session 100: DC Circuit Breaker Design

Chair(s): Ty McNutt, Rob Cuzner

Fault Discrimination using SiC JFET based Self-Powered Solid State Circuit Breakers in a Residential DC Community Microgrid 3747
Karthik Palaniappan, Willy Sedano, Nicholas Hoeft, Robert Cuzner and Z. John Shen
University of Wisconsin-Milwaukee, United States; Illinois Institute of Technology, United States

Optimization of Operation Temperature of Gate Commutated Thyristors for Hybrid DC Breaker 3754
Gang Lyu, Jiapeng Liu, Wenpeng Zhou, Rong Zeng, Xueqiang Zhang and Patrick Palmer
Tsinghua University, China; University of Cambridge, United Kingdom

A Topology of the Multi-Port DC Circuit Breaker for Multi-Terminal DC System Fault Protection ... 3760
Wenjun Liu, Fei Liu, Xiaoming Zha, Chao Chen and Tianyi Yu
Wuhan University, China

Optimization of a Z-Source, Ultra-Fast Mechanically Switched, High Efficiency DC Circuit Breaker 3764
Landon Mackey, Md Rifat Kaisar Rachi, Chang Peng and Iqbal Husain
North Carolina State University, United States

Session 101: LLC Converters

Chair(s): Regan Zane, Rivas-davila Juan

Efficiency Improvement of Three-Phase LLC Resonant Converter using Phase Shedding 3771
Sayed Abbas Arshadi, Martin Ordonez, Mehdi Mohammadi and Wilson Eberle
University of British Columbia, Canada

LLC Synchronous Rectification using Homopolarity Cycle Modulation 3776
Mehdi Mohammadi and Martin Ordonez
University of British Columbia, Canada

A Lagrangian Dynamics Model of Integrated Transformer Incorporated in a Multi-phase LLC Resonant Converter 3781
Mostafa Noah, Kazuhiro Umetani, Shun Endo, Hiraki Ishibashi, Jun Imaoka and Masayoshi Yamamoto
Shimane University, Japan; Okayama University, Japan; Kyushu University, Japan; Nagoya University, Japan

DC/DC Fixed Frequency Resonant LLC Full-Bridge Converter with Series-Parallel Transformers for 10kW High Efficiency Aircraft Application 3788
Y.E. Bouvier, U. Borović, M. Vasić, J.A. Oliver, P. Alou, J.A. Cobos, F. Árevalo, J.C. García-Tembleque and J. Carmena
Universidad Politecnica de Madrid, Spain; Indra Sistemas S.A., Spain

Session 102: AC-AC Converters II
Chair(s): Patrick Wheeler, Luca Zarri

Improvement of the Input-Output Quality of Three-Level NPC Inverters with Small DC-Link 3796
Hyo-Chul In, Seok-Min Kim and Kyo-Beum Lee
Ajou University, Korea

Transformer-based Single-Phase AC-DC-AC Topology for Grid Issues Mitigation 3802
Nayara B. de Freitas, Cursino B. Jacobina and Bruna S. Gehrke
Federal University of Campina Grande, Brazil

Control of Solid-State-Transformer for Minimized Energy Storage Capacitors 3809
Takanori Isobe, Hiroshi Tadano, Zijin He and Yang Zou
University of Tsukuba, Japan

Analysis and Design of LC Filters for the 5-Level 3-Phase Back to Back E-Type Converter 3816
Marco Di Benedetto, Alessandro Lidozzi, Luca Solero, Fabio Crescimbin and Petar J. Grbovic
Roma Tre University, Italy; Huawei Technologies Dusseldorf GmbH, Germany

Session 103: Reliability, Diagnostic, and Faults Analysis in Power Converters II
Chair(s): Yilmaz Sozer, Mario Pacas

Thermal Stress Mitigation by Active Thermal Control: Architectures, Models and Specific Hardware 3822
Alessandro Soldati, Fabrizio Dossena, Giorgio Pietrini, Davide Barater, Carlo Concarì and Francesco Iannuzzo
University of Parma, Italy; Aalborg University, Denmark

Impacts of PV Array Sizing on PV Inverter Lifetime and Reliability 3830
Ariya Sangwongwanich, Yongheng Yang, Dezso Sera and Frede Blaabjerg
Aalborg University, Denmark

Reliability Metrics Extraction for Power Electronics Converter Stressed by Thermal Cycles 3838
Ke Ma, Ui-Min Choi and Frede Blaabjerg
Shanghai Jiao Tong University, China; Aalborg University, Denmark

Study of PWM Frequency and its Impact to Adjustable Speed Drive Reliability 3844
Lixiang Wei, Jeffrey McGuire and Jiangang Hu
Rockwell Automation, United States

Session 104: Modulation Techniques I
Chair(s): Babak Parkhideh, Minjie Chen

Impact of Carrier Phase Shift PWM on the DC Link Current of Single and Interleaved Three-Phase Voltage Source Converters 3851
Zhongyi Quan and Yunwei Li
University of Alberta, Canada

A DPWM-Controlled Three-Level T-Type Inverter for Photovoltaic Generation Considering Unbalanced Neutral-Point Voltage 3856
Mohammad M. Hashempour, Meng-Ying Yang and Tzung-Lin Lee
National Sun Yat-sen University, Taiwan

Over-Modulation Associated to Flash Memory based Multi-Optimal PWM for Three-Phase Inverters 3863
Dorin O. Neacșu and Brad Lehman
Northeastern University, United States; Technical University of Iasi, Romania

Stability Performance of Multi-connected Inverters with Global Synchronous Pulse Width Modulation 3871
Tao Xu and Feng Gao
Shandong University, China

Session 105: Modeling and Control of Grid Connected Converters I
Chair(s): Paolo Mattavelli, Carl Ho

Improved Resonant Current Controller for Grid-Tied Converters 3877
Diego Pérez-Estévez, Jesús Doval-Gandoy, Alejandro G. Yepes, Óscar López and Fernando Baneira
University of Vigo, Spain

Filter Capacitor Current Estimation and Grid Current Control in LCL based Grid Connected Inverter 3885
Subhajyoti Mukherjee, Vikram Roy Chowdhury, Pourya Shamsi and Mehdi Ferdowsi
Missouri University of Science and Technology, United States

A Dual Loop Current Control Structure with Improved Disturbance Rejection for Grid Connected Converters in the Synchronous Rotating Reference Frame 3890
Srinivas Gulur, Vishnu Mahadeva Iyer and Subhashish Bhattacharya
North Carolina State University, United States

Multi-Frequency Current Controller for Grid-Tied Converters 3897
Diego Pérez-Estévez, Jesús Doval-Gandoy, Alejandro G. Yepes, Óscar López and Fernando Baneira
University of Vigo, Spain

Session 106: Synchronous Reluctance Machines II
Chair(s): Ziaur Rahman, David Dorrell

Synchronous Reluctance Motor with Concentrated Windings for IE4 Efficiency 3905
Matteo Gamba, Gianmario Pellegrino, Eric Armando and Simone Ferrari
Politecnico di Torino, Italy

Carbon-Fiber Wrapped Synchronous Reluctance Traction Motor 3913
Kevin Grace, Steven Galioto, Karthik Bodla and Ayman El-Refaie
General Electric, United States

A Novel Fabrication and Assembly Method for Synchronous Reluctance Machines 3921
Chirag Desai, Hetal Mehta and Pragasen Pillay
Concordia University, Canada; Happy Engineering, India

High Speed Motors: A Comparison between Synchronous PM and Reluctance Machines 3927
Cristian Babetto, Giacomo Bacco, Grazia Berardi and Nicola Bianchi
University of Padova, Italy

Session 107: Variable Flux PM Machines

Chair(s): Sang Bin Lee, Zi-Qiang Zhu

Magnet Design Consideration of a Variable-Flux PM Machine 3935
Amirmasoud Takbash and Pragasen Pillay
Concordia University, Canada

Comparative Study of Variable Flux Memory Machines with Parallel and Series Hybrid Magnets 3942
Hao Hua, Z.Q. Zhu, Adam Pride, Rajesh Deodhar and Toshinori Sasaki
University of Sheffield, United Kingdom; IMRA Europe SAS, United Kingdom

Design of Variable Magnetization Pattern Machines for Dynamic Changes in the Back-EMF Waveform 3950
Ryoko Imamura, Teng Wu and Robert D. Lorenz
University of Wisconsin-Madison, United States

Performance Assessment of Ferrite- and Neodymium-Assisted Synchronous Reluctance Machines 3958
Riccardo Leuzzi, Paolo Cagnetta, Francesco Cupertino, Simone Ferrari and Gianmario Pellegrino
Politecnico di Bari, Italy; Politecnico di Torino, Italy

Session 108: PM and IPM Motor Drives II

Chair(s): Ali Bazzi, Prerit Pramod

Permanent Magnet Synchronous Machine Drive Control using Analog Hall-Effect Sensors 3966
David Reigosa, Daniel Fernandez, Cristina Gonzalez, Sang Bin Lee and Fernando Briz
University of Oviedo, Spain

A New Zero-Sequence Current Suppression Control Strategy for Five-Phase Open-Winding FTFCW-IPM Motor Driving System 3972
Ronghua Cui, Ying Fan and Ming Cheng
Southeast University, China

An Effective Voltage Control Loop for a Deep Flux-Weakening in IPM Synchronous Motor Drives 3979
Virginia Manzolini, Davide Da Ru and Silverio Bolognani
University of Padova, Italy

Real-Time Disturbance Compensation Algorithm for the Current Control of PMSM Drives 3987
Milo De Soricellis, Davide Da Rù and Silverio Bolognani
University of Padova, Italy; Robert Bosch GmbH, Germany

Session 109: Packaging II

Chair(s): Zhuxian Xu, Muhammad Nawaz

A Novel Low Inductive 3D SiC Power Module based on Hybrid Packaging and Integration Method ... 3995
Zhizhao Huang, Yuxiong Li, Lichuan Chen, Yifan Tan, Cai Chen, Yong Kang and Fang Luo
Huazhong University of Science and Technology, China; University of Arkansas, United States

Design of a Novel, High-Density, High-Speed 10 kV SiC MOSFET Module 4003
Christina DiMarino, Mark Johnson, Bassem Mouawad, Jianfeng Li, Dushan Boroyevich, Rolando Burgos,
Guo-Quan Lu and Meiyu Wang
Virginia Polytechnic Institute and State University, United States; University of Nottingham, United Kingdom

Flexible Epoxy-Resin Substrate based 1.2 kV SiC Half Bridge Module with Ultra-Low Parasitics and High Functionality 4011
Xin Zhao, Bo Gao, Yifan Jiang, Liqi Zhang, Sizhen Wang, Yang Xu, Kenji Nishiguchi, Yoshi Fukawa and Douglas C. Hopkins
North Carolina State University, United States; Risho Kogyo Co., Ltd, Japan; TOYOTech LLC, United States

New Industrial Module Package with Matched CTE Materials 4019
Mark Steiner, Eric Motto and John Donlon
Powerex, Inc., United States

Session 110: Wireless Power Transfer II

Chair(s): ChunTaek Rim, Shuo Wang

Achieving Low Magnetic Flux Density and Low Electric Field Intensity for an Inductive Wireless Power Transfer System 4022
Guangqi Zhu and Robert D. Lorenz
University of Wisconsin-Madison, United States

FOM-rd Plane: An Effective Design and Analysis Methodology for Resonant Energy Link in Inductive Power Transfer 4030
Chae-Ho Jeong, Hee-Su Choi and Sung-Jin Choi
University of Ulsan, Korea

Output Voltage Control for Series-Series Compensated Wireless Power Transfer System without Direct Feedback from Measurement or Communication 4035
Euihoon Chung, Gyu Cheol Lim, Jung-Ik Ha and Ki Young Kim
Seoul National University, Korea; Samsung Electronics Co., Ltd., Korea

Magnetizable Concrete Composite Materials for Road-Embedded Wireless Power Transfer Pads 4041
Reza Tavakoli, A. Echols, U. Pratik, Zeljko Pantic, Fray Pozo, Amir Malakooti and Marc Maguire
Utah State University, United States

Session 111: PV Plants and PV Farms

Chair(s): Rajapandian Ayyanar, Fei Gao

AC Impedance Derivation of Utility Scale PV Farm 4049
Ye Tang, Rolando Burgos, Chi Li and Dushan Boroyevich
Virginia Polytechnic Institute and State University, United States

A New Approach for Increasing Energy Harvest in Large Scale PV Plants Employing a Novel Voltage Balancing Topology 4055
Ahmed Salah Morsy, Sinan A. Sabeeh Al-Obaidi and Prasad Enjeti
Texas A&M University, United States

On-Line Health Monitoring of PV Plants 4061
Matam Manjunath, B. Venugopal Reddy, Y. Zhao and Brad Lehman
National Institute of Technology Goa, India; Northeastern University, United States

Hybrid Solar Plant with Synchronous Power Controllers Contribution to Power System Stability ... 4069

Daniel Remon, Antoni M. Cantarellas, Jorge Martinez-Garcia, Juan M. Escano and Pedro Rodriguez
Technical University of Catalonia, Spain; Abengoa, Spain; Loyola University Andalusia, Spain

Session 112: Droop Techniques for Microgrid Operation

Chair(s): Rolando Burgos, Hui Li

Comparison between Inverters based on Virtual Synchronous Generator and Droop Control 4077

Xin Meng, Zeng Liu, Jinjun Liu, Shike Wang, Baojin Liu and Ronghui An
Xi'an Jiaotong University, China

Hybrid Isochronous-Droop Control for Power Management in AC Microgrids 4085

Inam Ullah Nutkani, Lasantha Meegahapola, Donald Grahame Holmes and Chee Shen Lim
RMIT University, Australia; University of Southampton, Malaysia

Improved Droop Control Strategy based on Improved PSO Algorithm 4092

Zishun Peng, Jun Wang, Daqiang Bi, Z. John Shen, Yuxing Dai and Yeting Wen
Hunan University, China; Tsinghua University, China

A Modified Q-V Droop Control for Accurate Reactive Power Sharing in Distributed Generation Microgrid 4099

Jiuyang Zhou and Po-Tai Cheng
National Tsing Hua University, Taiwan

Session 113: Control in DC Microgrids

Chair(s): Tomislav Dragicevic, Xiaonan Lu

Admittance-type RC-mode Droop Control to introduce Virtual Inertia in DC Microgrids 4107

Zheming Jin, Lexuan Meng, Renke Han, Josep M. Guerrero and Juan C. Vasquez
Aalborg University, Denmark

Power-based Droop Control Suppressing the Effect of Bus Voltage Harmonics for DC Microgrids 4113

Guangyuan Liu, Tommaso Caldognetto, Paolo Mattavelli and Paolo Magnone
University of Padova, Italy

Containment-based Distributed Coordination Control to Achieve Both Bounded Voltage and Precise Current Sharing in Reverse-Droop-based DC Microgrid 4121

Renke Han, Haojie Wang, Zheming Jin, Lexuan Meng and Josep M. Guerrero
Aalborg University, Denmark; North China Electric Power University, China

A High-Efficiency Interleaved Single-Phase AC-DC Converter with Common-Mode Voltage Regulation for 380 V DC Microgrids 4128

Fang Chen, Rolando Burgos and Dushan Boroyevich
Virginia Polytechnic Institute and State University, United States

Session 114: Resonant DC/DC Converters

Chair(s): Hongliang Wang, Aleksandar Prodic

An Improved Voltage Balancing Technique for a Soft-Switched High-Gain Converter with Low Voltage Stress using Duty Ratio Control for Wind Energy Application 4136

Mehdi Abbasi and John Lam
York University, Canada

A Power Converter for an Electrostatic Precipitator using SiC MOSFETs 4144
Pedro J. Villegas, Juan A. Martin Ramos, Juan Diaz Gonzalez and Juan A. Martinez Esteban
University of Oviedo, Spain

A Hybrid Resonant Three-Level Converter for Renewable Energy in MVDC Collection Systems 4152
Guangfu Ning, Xiaopeng Cao, Liangcai Shu, Wu Chen and Baojian Ji
Southeast University, China; Nanjing University of Technology, China

**Time Domain Analysis of LLC Resonant Converters in the Boost Mode for Battery
Charger Applications** 4157
Navid Shafiei, Mohammad Ali Saket and Martin Ordonez
University of British Columbia, Canada

Session 115: Modular Multilevel Converters (MMC)
Chair(s): Luca Solero, Rostan Rodrigues

**A Fault-Tolerant Operation Scheme for a Modular Multilevel Converter with a Distributed
Control Architecture** 4163
Shunfeng Yang, Yi Tang, Pengfei Tu and Peng Wang
Nanyang Technological University, Singapore

**Redistributed Pulse Width Modulation of MMC Battery Energy Storage System under Submodule
Fault Condition** 4171
Xin Gu, Feng Gao, Farooq Aamir, Xifeng Liu and Jing Xiao
Shandong University, China; Shandong Electric Power Maintenance Company, China

Compensation Method of Arm Current Sensor Scaling Error in MMC System 4177
Belete Belayneh Negesse, Chang-Hwan Park and Jang-Mok Kim
Pusan National University, Korea

A Novel Sub-module Topology for MMC against DC Side Short-Circuit Faults 4185
Yao Xue, Xiaofeng Yang, Trillion Q. Zheng, Bowei Chen and Yan Li
Beijing Jiaotong University, China; Electric Power Research Institute, China

Session 116: Reliability, Diagnostic, and Faults Analysis for Power Devices
Chair(s): Behrooz Mirafzal, Jun Wang

**Fault Detection Method for IGBT Open-Circuit Faults in the Modular Multilevel Converter based
on Predictive Model** 4190
Kunshan Xu, Shaojun Xie, Ye Yan, Zhao Zhang, Binfeng Zhang and Qiang Qian
Nanjing University of Aeronautics and Astronautics, China

Asymmetric Power Device Rating Selection for Even Temperature Distribution in NPC Inverter 4196
Ui-Min Choi and Frede Blaabjerg
Aalborg University, Denmark

**Impact of Lifetime Model Selections on the Reliability Prediction of IGBT Modules in Modular
Multilevel Converters** 4202
Yi Zhang, Huai Wang, Zhongxu Wang, Yongheng Yang and Frede Blaabjerg
Aalborg University, Denmark

Open-circuit Fault Diagnosis of Switching Devices in a Modular Multilevel Converter with Distributed Control 4208
Shunfeng Yang, Yi Tang and Peng Wang
Nanyang Technological University, Singapore

Session 117: Modulation Techniques II

Chair(s): Jason Lai, Martin Ordonez

New Constraint in SHE-PWM for Single Phase Inverter Applications 4215
Mohammad Sharifzadeh, Hani Vahedi and Kamal Al-Haddad
University du Quebec, Canada; Ossiaco Inc., Canada

Novel Modulation Schemes and Switching Pattern for Z-Source Ultra-Sparse Matrix Converter 4223
Amir Masoud Bozorgi, Mehdi Farasat and Ekrem Karaman
Louisiana State University, United States; Warner Power LLC, United States

A New Adaptive Switching Frequency Modulation for Optimizing Low Power Cascaded Buck-Boost Converter 4230
Xi Chen, Anirudh Pise, Issa Batarseh and John Elmes
University of Central Florida, United States; Advanced Power Electronics Corporation, United States

An Improved Modulation Strategy for the Three-Phase Z-Source Inverters (ZSIs) 4237
Ahmed Abdelhakim, Pooya Davari, Frede Blaabjerg and Paolo Mattavelli
University of Padova, Italy; Aalborg University, Denmark

Session 118: Modeling and Control of Grid Connected Converters II

Chair(s): Jian Sun, Mahshid Amirabadi

Improved Control Strategy of Grid Connected Inverter without Phase Locked Loop on PCC Voltage Disturbance 4244
Liang Chen, Heng Nian, Boliang Lou and HongYang Huang
Zhejiang University, China; State Grid Zhejiang Electric Power Company, China

Automated and Scalable Optimal Control of Three-Phase Embedded Power Grids including PLL 4252
David Dewar, Andrea Formentini and Pericle Zanchetta
University of Nottingham, United Kingdom

Optimal Variable Switching Frequency Scheme for Grid Connected Full Bridge Inverters with Bipolar Modulation Scheme 4260
Yinglai Xia, Jinia Roy and Raja Ayyanar
Texas Instruments, United States; Arizona State University, United States

Grid-Connected Power Converters with Distributed Virtual Power System Inertia 4267
Jingyang Fang, Xiaoqiang Li and Yi Tang
Nanyang Technological University, Singapore

Session 119: Linear Machines

Chair(s): Siavash Pakdelian, David Diaz Reigosa

Comparative Study of Coreless-Type PM Linear Synchronous Machines with Non-Overlapping Windings 4274
Seun Guy Min and Bulent Sarlioglu
University of Wisconsin-Madison, United States

Comparative Study of Novel Tubular Flux-Reversal Transverse Flux Permanent Magnet Linear Machine 4282
Shaohong Zhu, Tom Cox and Chris Gerada
University of Nottingham, United Kingdom

Electrical Losses Minimization of Linear Induction Motors Considering the Dynamic End-Effects ... 4288
A. Accetta, M.C. Di Piazza, M. Luna and M. Pucci
ISSIA-CNR, Italy

Design and Performance Investigation of Doubly Salient Slot Permanent Magnet Linear Machines 4295
Yiming Shen, Qinfen Lu and Lijian Wu
Zhejiang University, China

Session 120: PM Motor Design, Control and Testing
Chair(s): Junichi Asama, Andrea Cavagnino

Inductance Testing According to the New IEEE Std 1812 – Application and Possible Extensions for IPM Machines 4302
Vandana Rallabandi, Narges Taran, Dan M. Ionel and Ping Zhou
University of Kentucky, United States; ANSYS, Inc., United States

Parametric Design Method for SPM Machines Including Rounded PM Shape 4309
Chao Lu, Simone Ferrari, Gianmario Pellegrino, Claudio Bianchini and Matteo Davoli
Politecnico di Torino, Italy; University of Modena and Reggio Emilia, Italy

Investigation of Different Servo Motor Designs for Servo Cycle Operations and Loss Minimizing Control Performance 4316
Huthaifa Flieh, Robert D. Lorenz, Eigo Totoki, Shinichi Yamaguchi and Yuichiro Nakamura
University of Wisconsin-Madison, United States; Mitsubishi Electric Corp., Japan

Synchronous SVPWM for Field-Oriented Control of PMSM using Phase-Lock Loop 4324
Lifan Xiao, Jian Li, Junhua Chen, Ronghai Qu and Yongqian Xiong
Huazhong University of Science and Technology, China

Session 121: Drive Applications
Chair(s): Mazharul Chowdhury, Annette Muetze

Over-Voltage Mitigation on SiC based Motor Drives through an Open End Winding Configuration ... 4332
S. De Caro, S. Foti, T. Scimone, A. Testa, G. Scelba, M. Pulvirenti and S. Russo
University of Messina, Italy; University of Catania, Italy; STMicroelectronics, Italy

A Fault Monitoring System for a Reciprocating Pump Driven by a Linear Motor for Oil Pumping Systems 4338
Hussain A. Hussain and Hamid A. Toliyat
Texas A&M University, United States

The Impact of Grid Unbalances on the Reliability of DC-Link Capacitors in a Motor Drive 4345
Huai Wang, Pooya Davari, Dinesh Kumar, Firuz Zare and Frede Blaabjerg
Aalborg University, Denmark; Danfoss Drives A/S, Denmark; University of Queensland, Australia

Achieving Zero Common Mode Voltage Generation in a Balanced Inverter with Neutral-Point Diode-Clamping 4351
Di Han, Silong Li, Woongkul Lee and Bulent Sarlioglu
University of Wisconsin-Madison, United States

Session 122: High Voltage Devices
Chair(s): Daniel Costinett, Ruxi Wang

Development of PSpice Modeling Platform for 10kV/100 A SiC MOSFET Power Module 4358
João Martins, Muhammad Nawaz, Kalle Ilves and Francesco Iannuzzo
ABB Corporate Research, Sweden; Aalborg University, Denmark

Continuous Switching Operation of 15 kV FREEDM Super-Cascode 4366
Soumik Sen, Xiaoqing Song, Liqi Zhang and Alex Q. Huang
North Carolina State University, United States; ABB Corporate Research Center, United States

Experimental Optical Transistor for All-Optical SiC ETO Thyristor 4373
Alireza Mojab and Sudip K. Mazumder
University of Illinois at Chicago, United States

Modeling and Power Loss Evaluation of Ultra Wide Band Gap Ga2O3 Device for High Power Applications 4377
Inhwan Lee, Avinash Kumar, Ke Zeng, Uttam Singisetti and Xiu Yao
State University of New York at Buffalo, United States

Session 123: Wireless Power Transfer III
Chair(s): Xu She, Alireza Safaee

The Effect of Matrix Power Repeaters on Magnetic Field Distribution of IPT Systems 4383
Rong Hua, Aiguo Patrick Hu and Ho Fai Leung
University of Auckland, New Zealand

Soft-Switching Self-Tuning H-Bridge Converter for Inductive Power Transfer Systems 4388
Masood Moghaddami, Andres Cavada and Arif I. Sarwat
Florida International University, United States

Load-Independent Transconductance and ZPA Input for Symmetrical Resonant Converter in IPT System 4393
Jiang-Hua Lu, Guo-Rong Zhu, Jin Jiang, Wen-Jing Li and Bo Li
Wuhan University of Technology, China; University of Western Ontario, Canada

Design of Wireless Power Transfer System for Devices Carried by a Freely Moving Animal in Cage ... 4398
Jeff Po Wa Chow, Henry Shu Hung Chung, Leanne Lai Hang Chan, Nathan Judson McDannold and Sai Chun Tang
City University of Hong Kong, Hong Kong; Brigham and Women's Hospital, United States

Session 124: Solar Photovoltaic Technologies
Chair(s): Afshin Izadian, Yongheng Yang

Subcell Modelling of Partially Shaded Solar Photovoltaic Panels 4406
Pallavi Bharadwaj and Vinod John
Indian Institute of Science, India

Effect of Water on Parasitic Capacitance of Photovoltaic Panel	4414
Shaolin Yu, Jianing Wang and Xing Zhang <i>Hefei University of Technology, China</i>	
An Application of Support Vector Machine to PV Power Forecasting under Different Weather Conditions	4420
Utpal Kumar Das, Kok Soon Tey, Mohd Yamani Idna Idris, Saad Mekhilef and Mutsuo Nakaoka <i>University of Malaya, Malaysia</i>	
High Performance Buck-Boost Converter based PV Characterisation Set-Up	4425
Pallavi Bharadwaj and Vinod John <i>Indian Institute of Science, India</i>	
Session 125: Control and Design Techniques for Microgrids I	
Chair(s): Josep M. Guerrero, Mohammad B.Shadmand	
A Stabilization Method of LC Input Filter in DC Microgrids Feeding Constant Power Loads	4433
Hao Wang, Hua Han, Zhangjie Liu, Yao Sun, Mei Su, Xiaochao Hou and Peng Yang <i>Central South University, China</i>	
Model-Predictive-Control-based Distributed Control Scheme for Bus Voltage Unbalance and Harmonics Compensation in Microgrids	4439
Jia Liu, Yushi Miura and Toshifumi Ise <i>Osaka University, Japan</i>	
Smart Inverter Volt-Watt Control Design in High PV Penetrated Distribution Systems	4447
Mahsa Ghapandar Kashani, Maziar Mobarrez and Subhashish Bhattacharya <i>North Carolina State University, United States</i>	
Virtual Resistance Technique for Power Limit Management of Microgrid DG Inverters	4453
Siddhesh Shinde, S. Milad Tayebi, Hu Haibing, Nasser Kutkut and Issa Batarseh <i>University of Central Florida, United States; Nanjing University of Aeronautics & Astronautics, China</i>	
Session 126: Datacenters and Telecommunication Applications	
Chair(s): Al-Thaddeus Avestruz, Ashish Kumar	
A High Efficiency Resonant Switched-Capacitor Converter for Data Center	4460
Yanchao Li, Xiaofeng Lyu, Dong Cao, Shuai Jiang and Chenhao Nan <i>North Dakota State University, United States; Google Inc., United States</i>	
A Series-Stacked Architecture with 4-to-1 GaN-based Isolated Converters for High-Efficiency Data Center Power Delivery	4467
Yizhe Zhang, Enver Candan and Robert C.N. Pilawa-Podgurski <i>University of Illinois at Urbana-Champaign, United States</i>	
Improved Model Predictive Control for High Voltage Quality in Microgrid Applications	4475
T. Dragicevic, M. Alhasheem, M. Lu, and F. Blaabjerg <i>Aalborg University, Denmark; Arab Academy for Science, Technology and Maritime Transport, Egypt</i>	
Virtual Resistance-based Control Strategy for DC link Regeneration Protection and Current Sharing in Uninterruptible Power Supply	4481
Jinghang Lu, Yajuan Guan, Mehdi Savaghebi and Josep Guerrero <i>Aalborg University, Denmark</i>	

Session 127: Power Electronics in Electrified Vehicles

Chair(s): Matthias Preindl, Gui-Jia Su

Range Extension of Electric Vehicles by Two Battery HEECS Chopper based Power Train 4488

Ayataro Tamura, Koji Kobayashi, Yukinori Tsuruta, Kazuaki Kojima, Hidemine Obara and Atsuo Kawamura
Yokohama National University, Japan

A Delta-Structured Switched-Capacitor Equalizer for Series-Connected Battery Strings 4493

Yunlong Shang, Bing Xia, Jufeng Yang, Chenghui Zhang, Naxin Cui and Chris Mi
Shandong University, China; San Diego State University, United States; University of California-San Diego, United States; Nanjing University of Aeronautics and Astronautics, China

An Automatic EMI Filter Design Methodology for Electric Vehicle Application 4497

Dong Zhang, Tao Fan, Puqi Ning and Xuhui Wen
China Academy of Sciences, China

1.8MHz Isolated DC-DC Converter with Multi-Transformer Structure for Automotive Applications 4504

Goh Teck Chiang, Shuji Tomura and Takahide Sugiyama
Toyota Central R&D Labs., Inc., Japan

Session 128: DAB DC/DC Converters

Chair(s): Alessandro Costabeber, Madhav Manjrekar

Wide Range ZVS Operation of Three-Phase Dual Active Bridge Converters using Reduced Coupling Factor Transformers 4512

Carlos Teixeira, Jan Riedel, Brendan McGrath and Donald Grahame Holmes
RMIT University, Australia

Modelling and Analysis of the Transformer Current Resonance in Dual Active Bridge Converters 4520

Zian Qin, Zhan Shen and Frede Blaabjerg
Aalborg University, Denmark

A Novel ISOP Current-Fed Modular Dual-Active-Bridge (CF-MDAB) DC-DC Converter with DC Fault Ride-Through Capability for MVDC Application 4525

Yuxiang Shi, Ran Mo, Hui Li and Zhiguo Pan
ABB Inc., United States; Florida State University, United States

Design Considerations for a High-Power Dual Active Bridge DC-DC Converter with Galvanically Isolated Transformer 4531

Youngsil Lee, Alan J. Watson, Gaurang Vakil and Patrick W. Wheeler
University of Nottingham, United Kingdom

Session 129: MMC Modulation and Control

Chair(s): Pericle Zanchetta, Jean-Luc Schanen

Lagrange-based Optimization of Cell Voltage and Arm Current with Zero-Sequence Current Injection in Modular Multilevel Converter 4538

Tsai-Fu Wu, Chun-Wei Huang and Tzu-Chieh Chou
National Tsing Hua University, Taiwan

Discontinuous PWM Scheme for a Modular Multilevel Converter with Advanced Switching Losses Reduction Ability 4546
Min-Gyo Jeong, Seok-Min Kim and Kyo-Beum Lee
Ajou University, Korea

Dynamic Matrix Predictive Control on DC-AC Modular Multilevel Converter: Design, Control and Real-Time Simulation 4552
Isaac Gonzalez-Torres, Homero Miranda, Cesar Mendez-Barrios, Victor Cardenas, Jose Espinoza, Marcos I. Gonzalez and Marcelo Perez
Universidad Autónoma de San Luis Potosí, Mexico; Concepcion University, Chile; Universidad Tecnica Federico Santa Maria, Chile

Capacitor Voltage Ripples Characterization and Reduction of Hybrid Modular Multilevel Converter with Circulating Current Injection 4560
Cong Zhao, Yaohua Li, Fei Xu, Zixin Li, Ping Wang and Ming Lei
Chinese Academy of Sciences, China; University of Chinese Academy of Sciences, China

Session 130: Control of Grid Connected Converter

Chair(s): Joseph Olorunfemi Ojo, Xiongfei Wang

An Envelope-based Detection Method for Resonance Damping in Grid-Connected Converters 4568
Chia-Tse Lee, Akira Kikuchi and Tomomichi Ito
Hitachi, Ltd., Japan

Manitoba Inverter – Single Phase Single-Stage Buck-Boost VSI Topology 4576
Carl Ngai Man Ho and Ken King Man Siu
University of Manitoba, Canada

Direct Decoupled Active and Reactive Predictive Power Control of Grid-Tied Quasi-Z-Source Inverter for Photovoltaic Applications 4582
Sarthak Jain, Sivasai Praneeth Nanduri, Mohammad B. Shadmand, Robert S. Balog and Haitham Abu-Rub
Texas A&M University, United States; Kansas State University; United States; Texas A&M University at Qatar, Qatar

Optimal Phase Shifted Method to Reduce Current Ripples for a Parallel Grid-Connected Voltage Source Inverter under Unequal DC-Link Voltage 4589
June-Hee Lee and Kyo-Beum Lee
Ajou University, Korea

Session 131: Modeling and Control of AC-DC Converters

Chair(s): Frede Blaabjerg, Marco Dalla Costa

A Robust Deadbeat Predictive Power Control with Sliding Mode Disturbance Observer for PWM Rectifiers 4595
Haitao Yang, Yongchang Zhang, Jiejunyi Liang, Nong Zhang and Paul Walker
University of Technology, Sydney, Australia; North China University of Technology, China

A Control Strategy to Compensate for Current and Voltage Measurement Errors in Three-Phase PWM Rectifiers 4601
Trinh Quoc Nam, Choo Fook Hoong, Tang Yi and Wang Peng
Nanyang Technological University, Singapore

Carrier based PWM for Reduced Capacitor Voltage Ripple in Three-Phase Three-Switch Buck-Type Rectifier System 4609
Beomseok Chae, Yongsug Suh and Tahyun Kang
Chonbuk National University, Korea; Milimsyscon Co., Korea

Direct Power Control of PWM Rectifier under Unbalanced Network using Extended Power Theory 4617
Yongchang Zhang, Jie Liu and Jihao Gao
North China University of Technology, China

Session 132: Model Predictive Control of Power Converters I
Chair(s): Ralph Kennel, Tobias Geyer

Modulated Model Predictive Control for Active Split DC-bus 4-leg Power Supply 4622
S. Bifaretti, S. Pipolo, A. Lidozzi, L. Solero, L. Tarisciotti and P. Zanchetta
University of Rome Tor Vergata, Italy; Roma Tre University, Italy; University of Nottingham, United Kingdom

On the Inherent Relationship between Finite Control Set Model Predictive Control and SVM-based Deadbeat Control for Power Converters 4628
Yongchang Zhang, Jie Liu and Shengwen Fan
North China University of Technology, China

Predictive Current Control for Stabilizing Power Electronics based AC Power Systems 4634
M.A. Awal, Iqbal Husain and Wensong Yu
North Carolina State University, United States

Computationally Efficient Long-Horizon Direct Model Predictive Control for Transient Operation 4642
Petros Karamanakos, Tobias Geyer and Ricardo P. Aguilera
Tampere University of Technology, Finland; ABB Corporate Research, Switzerland; University of Technology Sydney, Australia

Session 133: Thermal Model of Electric Machines
Chair(s): Davide Barater, Rashmi Prasad

Improved Thermal Model for Predicting End-Windings Heat Transfer 4650
Gabriele Luca Basso, Yew Chuan Chong, James Goss and Dave Staton
Royal Institute of Technology, Sweden; Motor Design Ltd, United Kingdom

Reducing the Complexity of Thermal Models for Electric Machines via Sensitivity Analyses 4658
B. Assaad, K. El kadri Benkara, G. Friedrich, S. Vivier and A. Michon
Renault SAS, France; Université de technologie de Compiègne, France; CETIM, France

Importance of Thermal Modeling for Design Optimization Scenarios of Induction Motors 4666
Gerd Bramerdorfer, Andrea Cavagnino and Silvio Vaschetto
Johannes Kepler University Linz, Austria; Politecnico di Torino, Italy

Reduced Lumped Parameter Thermal Model for External Rotor Permanent Magnet Motor Design 4673
Aitor Tovar-Barranco, Fernando Briz, Amaia López-de-Heredia and Irma Villar
IK4-Ikerlan, Spain; Universidad de Oviedo, Spain

Session 134: PM Machines, Demagnetization, Eccentricity and Losses

Chair(s): Gianmario Pellegrino, Bulent Sarliglu

On-Line Detection of Rotor Eccentricity for PMSMs based on Hall-Effect Field

Sensor Measurements 4678

Yonghyun Park, Daniel Fernandez, Sang Bin Lee, Doosoo Hyun, Myung Jeong, Suneel Kumar Kommuri, Changhee Cho, David Reigosa and Fernando Briz

Korea University, Korea; University of Oviedo, Spain; Gyeonggi College of Science & Technology, Korea

Detection of Demagnetization in Permanent Magnet Synchronous Machines using Hall-Effect Sensors 4686

David Reigosa, Daniel Fernandez, Yonghyun Park, Alberto B. Diez, Sang Bin Lee and Fernando Briz

University of Oviedo, Spain

Demagnetization Study of an Interior Permanent Magnet Synchronous Machine Considering Transient Peak 3 Phase Short-Circuit Current 4694

Seong Taek Lee

BorgWarner, United States

Reduction of Inverter Carrier Harmonic Losses in Interior Permanent Magnet Synchronous Motors by Optimizing Rotor and Stator Shapes 4699

Katsumi Yamazaki, Yusuke Togashi, Takeshi Ikemi, Shunji Ohki and Ryoichi Mizokami

Chiba Institute of Technology, Japan; Nissan Motor Co., Ltd., Japan

Session 135: Control of Electric Drives II

Chair(s): Michael Harke, Alireza Fatemi

Robust Control for High Performance Induction Motor Drives based on Partial State-Feedback Linearization 4707

A. Accetta, F. Alonge, M. Cirrincione, F. D'Ippolito, M. Pucci, R. Rabbeni and A. Sferlazza

University of Palermo, Italy; University of the South Pacific, Fiji; ISSIA CNR, Italy; CNRS, LAAS, France

The Vector Space Decomposition based Control for Multiple-Channel Indirect Matrix Converter Fed Dual Three-Phase PMSM Drives 4714

Yang Xiao and Zheng Wang

Southeast University, China

Predictive Current Control for Induction Motor using Online Optimization Algorithm with Constrains 4720

Zhiguo Wang, Zedong Zheng, Yongdong Li, Boran Fan and Guibin Li

Tsinghua University Beijing, China; Xinjiang University, China

Implementing Observer-based Design Methodology for Deadbeat-Direct Torque and Flux Control with Back-EMF Self-Sensing using Rapid Control Prototyping 4726

Shang-Chuan Lee and Robert D. Lorenz

University of Wisconsin-Madison, United States

Session 136: Emerging Applications

Chair(s): Jin Wang, Mark J Scott

Design of a Linear Permanent Magnet Synchronous Motor for Needle-Free Jet Injection 4734

Nick N.L. Do, Andrew J. Taberner and Bryan P. Ruddy

University of Auckland, New Zealand

- An Energy Harvesting Scheme for Dielectric Elastomer Generators** 4741
 Ramanuja Panigrahi, Santanu Mishra, Arpit Kumar Srivastava and Sumit Basu
Indian Institute of Technology Kanpur, India
- A Bipolar Self-Start up Boost Converter for Thermoelectric Energy Harvesting** 4747
 Keita Taeda and Hirotaka Koizumi
Tokyo University of Science, Japan
- Comparative Analysis and Evaluation of High Voltage Power Generation Architectures** 4753
 Saijun Mao, Jelena Popovic, Jan Abraham Ferreira, Chengmin Li and Wuhua Li
Delft University of Technology, Netherlands; Zhejiang University, China

Thursday, October 5

Session 137: Other Topics in Renewable Energy Applications

Chair(s): Fei Gao, John Lam

- Performance of Anti-Islanding of an Improved Reactive Power Variation Method based on Positive Feedback** 4761
 Jongmin Jo and Hanju Cha
Chungnam National University, Korea
- Shaping of PWM Converter Admittance with Outer Power Control Loop** 4766
 Byeong-Heon Kim and Seung-Ki Sul
North Carolina State University, United States; Seoul National University, Korea
- Hydrokinetic Powered Irrigation Network Automation: A Scalable Architecture for the Enablement of Real-Time Automated Decentralized Control of the Irrigation Water Delivery System in Developing Countries** 4773
 Mohammad A. Bharmal, Syeda Q. Akbar, Sana Noor, Rabiya Farooq and Nauman A. Zaffar
Lahore University of Management Sciences, Pakistan
- Wind Farm Grounding System Analysis** 4780
 Massood Keshavarz Siahpoosh, Li Li and David G. Dorrell
University of Technology Sydney, Australia; University of KwaZulu-Natal, South Africa

Session 138: Power Quality of Grid Connected Converters I

Chair(s): Brandon Grainger, Stefano Bifaretti

- Diversifying the Role of Distributed Generation Grid Side Converters for Improving the Power Quality of Distribution Networks using Advanced Control Techniques** 4786
 Zunaib Ali, Nicholas Christofides, Lenos Hadjidemetriou and Elias Kyriakides
Frederick University, Cyprus; University of Cyprus, Cyprus
- Circulating Resonant Current Suppression for Current-Controlled Inverters based on Output Impedance Shaping** 4794
 Qiang Qian, Binfeng Zhang, Zhaohui Ni, Shaojun Xie, Jinming Xu and Kunshan Xu
Nanjing University of Aeronautics and Astronautics, China
- Sensorless Unbalance Correction as an Ancillary Service for LV 4-Wire/3-Phase Power Converters ...** 4799
 Andres Suárez-González, Pablo García, Ángel Navarro-Rodríguez, Geber Villa and Jose M. Cano
University of Oviedo, Spain

Convertible Static Transmission Controller Model and Supervisory Vector Control for Operation under Unbalanced Grid Conditions 4806
Faris E. Alfaris and Subhashish Bhattacharya
North Carolina State University, United States

Session 139: Control and Design Techniques for Microgrids II
Chair(s): Ron Hui, Tsai-Fu Wu

Operation Optimization for Multi-microgrids Based on Centralized-Decentralized Hybrid Hierarchical Energy Management 4813
Meiqin Mao, Yangyang Wang, Liuchen Chang and Yan Du
Hefei University of Technology, China

Coordinated Failure Response and Recovery in a Decentralized Microgrid Architecture 4821
Abedalsalam Bani-Ahmed, Mohammad Rashidi and Adel Nasiri
University of Wisconsin-Milwaukee, United States

Analysis and Improvement of Synchronous Stability of Micro-Grids with Parallel Connected Inverters 4826
Vikram Roy Chowdhury, Subhajyoti Mukherjee, Pourya Shamsi and Mehdi Ferdowsi
Missouri University of Science and Technology, United States

Smart Resistor: Trajectory Control of Constant Power Loads in DC Microgrids 4832
Eric Bauer, Karun Arjun Potty, He Li and Jin Wang
Ohio State University, United States

Session 140: Wireless Charging for EV
Chair(s): ChunTaek Rim, Dong Dong

Load Power Agnostic 6.6 kW Wireless EV Charger with LCL Tuned Primary and Secondary Side Regulation 4839
Veda P. Galigekere, Omer C. Onar, Madhu Chinthavali, and Zhiqiang Wang
Oak Ridge National Laboratory, United States

High Power Factor Z-Source Resonant Wireless Charger with Soft Switching 4845
Hulong Zeng and Fang Zheng Peng
Michigan State University, United States

Bifurcation Phenomenon Limits for Three Phase IPT Systems with Constant Coupling Coefficient 4851
Ugaitz Iruretagoyena, Asier Garcia-Bediaga, Luis Mir, Haritza Camblong and Irma Villar
IK4-Ikerlan Technology Research Centre, Spain; University of the Basque Country, Spain; École Supérieure des Technologies Industrielles Avances, France

A Practical Static Simulator for Dynamic Wireless Charging of Electric Vehicle using Receiver Open Circuit Voltage Equivalent 4859
Shuangcheng Song, Qianfan Zhang, Chunbo Zhu and Diri Wang
Harbin Institute of Technology, China

Session 141: Multilevel Converters Applications

Chair(s): Sheldon Williamson, Liliana De Lillo

Low-Voltage-Ride-Through Control of a Modular Multilevel SDBC Inverter for Utility-Scale Photovoltaic Systems 4865

Paul Sochor, Hirofumi Akagi and Nadia M.L. Tan
Tokyo Institute of Technology, Japan; Universiti Tenaga Nasional, Malaysia

Common-Mode Voltage Analysis and Suppression in Five-Level Modular Composited Converter 4873

Jiawei Hu, Junsong Tang, Ye Mei, Senjun Hu, Wuhua Li and Xiangning He
Zhejiang University, China

Low Voltage Ride through Performance of a STATCOM based on Modular Multilevel Cascade Converters for Offshore Wind Application 4879

Takaaki Tanaka, Huai Wang, Ke Ma and Frede Blaabjerg
Aalborg University, Denmark; Fuji Electric Co., Ltd., Japan; Shanghai Jiao Tong University, China

Asymmetrical Hybrid Unidirectional T-Type Rectifier for High-Speed Gen-Set Applications 4887

S. Foti, A. Testa, G. Scelba, V. Sabatini, A. Lidozzi and L. Solero
University of Messina, Italy; University of Catania, Italy; Roma Tre University, Italy

Session 142: MMC New Topologies

Chair(s): Andrea Formentini, Marcello Pucci

ESBC: An Enhanced Modular Multilevel Converter with H-Bridge Front End 4894

Emmanuel Amankwah, Alessandro Costabeber, Omar Jasim, David Trainer and Jon Clare
The University of Nottingham, United Kingdom; GE Energy Connections, United Kingdom

Investigation of a New Modular Multilevel Converter with DC Fault Blocking Capability 4902

Xing Hu, Jianzhong Zhang, Shuai Xu and Yongjiang Jiang
Southeast University, China

A New Hybrid MMC with Integrated Battery Energy Storage 4908

Ping Wang, Tao Zhang and Rui Li
Shanghai Jiao Tong University, China

Enhanced Modular Multilevel Converter based Battery Energy Storage System 4914

Xiaofeng Yang, Yao Xue, BOWEI Chen, Fan Yang, Trillion Q. Zheng and Youyun Wang
Beijing Jiaotong University, China; Tianshui Electric Drive Research Institute Co. Ltd., China

Session 143: Modeling and Control of DC-DC Converters I

Chair(s): Praveen Jain, Petros Karamanakos

Seamless Transition of the Operating Zones for the Extended-Duty-Ratio Boost Converter 4920

Jinia Roy and Raja Ayyanar
Arizona State University, United States

A Digital Closed-Loop Control Strategy for Maintaining the 180° Phase Shift of an Interleaved BCM Boost Converter for PFC Applications 4927

Robert T. Ryan, John G. Hayes, Richard Morrison and Diarmuid Hogan
University College Cork, Ireland; Excelsys Technologies, Ireland

Digital Type II Compensation with Forced-Output Control of an Interleaved Two-Phase Coupled-Inductor Boost Converter 4935
Brendan C. Barry, John G. Hayes, Robert T. Ryan, Marek S. Rylko, Robert Stala, Adam Penczek and Andrzej Mondzik
University College Cork, Ireland; SMA Magnetics Sp. z.o.o. R&D, Poland

Dual-Frequency On-Off Control for a 20 MHz Class E DC-DC Converter 4942
Ying Li, Xinbo Ruan, Jiandong Dai and Zhihong Ye
Nanjing University of Aeronautics and Astronautics, China; Lite-On Technology, China

Session 144: Model Predictive Control of Power Converters II
Chair(s): Jian Guo Zhu, Jose Rodriguez

Long Horizon Linear MPC of Grid-Connected VSIs: Regulation Problems and a Plug-In Solution 4950
Chee Shen Lim, Sze Sing Lee, Xin Kong and Inam Ullah Nutkani
University of Southampton Malaysia Campus, Malaysia; Agency for Science Technology and Research, Singapore; Royal Melbourne Institute of Technology, Australia

Voltage Sensorless Improved Model Predictive Direct Power Control for Three-Phase Grid-Connected Converters 4957
Amir Masoud Bozorgi, Hosein Gholami-Khesht, Mehdi Farasat, Shahab Mehraeen and Mohammad Monfared
Louisiana State University, United States; Ferdowsi University of Mashhad, Iran

Finite Control Set Model Predictive Control Assisted by a Linear Controller for True Parameter Uncertainty Compensation 4964
Rodrigo Mendez, Daniel Sbarbaro, Jose Espinoza and Christian Rojas
Concepcion University, Chile

Model Predictive Control of Dual-Mode Operations Z-Source Inverter: Islanded and Grid-Connected 4971
Sally Sajadian and Reza Ahmadi
University of Kansas, United States

Session 145: Stability in Power Converters
Chair(s): Yam Siwakoti, Jiangchao Qin

LCL Filter Design based on Non-Minimum-Phase Stability Region for Grid-Connected Inverters in Weak Grid 4978
Fang Liu, Jie Zhang, Haizhen Xu, Xing Zhang, Wenguang Zhao and Meng Wang
Hefei University of Technology, China

A Way of Increasing Stability Margin of Current Control in VSCs Connected to the Grid through LCL Filters 4983
Leonardo Marin, Pedro Rodriguez, Ignacio Candela and Joan Rocabert
Polytechnic University of Catalonia, Spain

Small-Signal Modeling of Single-Phase PLLs using Harmonic Signal-Flow Graphs 4989
Shahil Shah and Leila Parsa
Rensselaer Polytechnic Institute, United States; University of California-Santa Cruz, United States

Current-Mode Controlled Single-Inductor Dual-Output Buck Converter with Ramp Compensation 4996
Yao Wang, Jianping Xu, Shuhan Zhou, Tianyang Zhao and Kai Liao
Southwest Jiaotong University, China; Southwest Minzu University, China; Nanyang Technological University, Singapore

Session 146: High Torque Machines

Chair(s): Hamid A. Toliyat, Wei Xu

A New Perspective on the PM Vernier Machine Mechanism 5001
Kangfu Xie, Dawei Li, Ronghai Qu, Xiang Ren and Yuan Pan
Huazhong University of Science and Technology, China

Internal Rotor Airgap-Less Electric Motors 5009
Omar Nezamuddin, Maryam Alibeik, Rishikesh Bagwe, Matthew Rubin and Euzeli dos Santos Jr.
Purdue University-Indianapolis, United States; Indiana University, United States

Design, Construction, and Analysis of a Large Scale Inner Stator Radial Flux Magnetically Geared Generator for Wave Energy Conversion 5017
Matthew Johnson, Matthew C. Gardner, Hamid A. Toliyat, Steven Englebretson, Wen Ouyang and Colin Tschida
Texas A&M University, United States; ABB Inc., United States

Magnetic Gearing Effect in Vernier Permanent Magnet Synchronous Machines 5025
Yue Liu and Z.Q. Zhu
University of Sheffield, United Kingdom

Session 147: Small PM Motors

Chair(s): Akira Chiba, Rajib Mikail

Design Optimization of a Small Single-Phase Motor with Auxiliary Permanent Magnet 5033
Mauro Andriollo, Andrea Tortella and Stefano Trubian
University of Padova, Italy

Slotless Lightweight Motor for Drone Applications 5041
Md Sariful Islam, Iqbal Husain and Rajib Mikail
North Carolina State University, United States; ABB Inc., United States

Novel 4/4 Stator/Rotor Single-Phase Asymmetric-Stator-Pole Doubly Salient Permanent Magnet Machine 5049
Mingjie He, Wei Xu and Caiyong Ye
Huazhong University of Science and Technology, China

Design Optimization of a Line-start PMSM Considering Transient and Steady-state Performance Objectives 5057
Alber J. Sorgdrager, Rong-Jie Wang and Andre J. Grobler
Stellenbosch University, South Africa; North-West University, South Africa

Session 148: Electric Drives for Wind and Other Renewable Integration

Chair(s): Jiangbiao He, Yue Zhao

Power Conversion and Control of a Magnetic Gear Integrated Permanent Magnet Generator for Wave Energy Generation 5065
Samir Hazra, Prathamesh Kamat, Subhashish Bhattacharya, Wen Ouyang and Steven Englebretson
North Carolina State University, United States; ABB Corporate Research Center, United States

A Novel Active Damping Scheme for use with Regenerative Converters 5073

Mahesh Swamy

Yaskawa America, Inc., United States

Model Predictive Power Control of a Brushless Doubly Fed Twin Stator Induction Generator 5080

Xinchi Wei, Ming Cheng, Wei Hua, Jianguo Zhu and Haitao Yang

Southeast University, China; University of Technology Sydney, Australia

A New Rotor Speed Observer for Stand-Alone Brushless Doubly-Fed Induction Generators 5086

Yi Liu, Wei Xu, Teng Long and Frede Blaabjerg

Huanggang Normal University, China; Huazhong University of Science and Technology, China; University of Cambridge, United Kingdom; Aalborg University, Denmark

Session 149: SiC Switching I

Chair(s): Francesco Iannuzzo, Shashank Krishnamurthy

Low Inductance Switching for SiC MOSFET based Power Circuit 5093

Edward Shelton, Xueqiang Zhang, Tianqi Zhang, Nikita Hari and Patrick Palmer

University of Cambridge, United Kingdom

Self-Supplied Isolated Gate Driver for SiC Power MOSFETs based on Bi-Level Modulation Scheme 5101

Jorge Garcia, Emre Gurpinar, Alberto Castellazzi and Pablo Garcia

University of Oviedo, Spain; University of Nottingham, United Kingdom

Multi-Level Active Gate Driver for SiC MOSFETs 5107

Harry C.P. Dymond, Dawei Liu, Jianjing Wang, Jeremy J.O. Dalton and Bernard H. Stark

University of Bristol, United Kingdom

Analytical Investigation on Design Instruction to Avoid Oscillatory False Triggering of Fast Switching SiC-MOSFETs 5113

Yusuke Sugihara, Kimihiro Nanamori, Seiya Ishiwaki, Yuma Hayashi, Kyota Aikawa, Kazuhiro Umetani,

Eiji Hiraki and Masayoshi Yamamoto

Shimane University, Japan; Okayama University, Japan; Nagoya University, Japan

Session 150: New Device, Circuit and Control Strategies

Chair(s): Xiu Yao, Lihua Chen

Comparison of 1.7kV, 450A SiC-MOSFET and Si-IGBT based Modular Three Phase Power Block 5119

Sayan Acharya, Xu She, Rajib Datta, Maja Harfman Todorovic and Gary Mandrusiak

North Carolina State University, United States; GE Global Research, United States

A Fast Dynamic Photovoltaic Simulator with Instantaneous Output Impedance Matching Controller 5126

Isuru D.G. Jayawardana, Carl Ngai Man Ho, Mandip Pokharel and Gerardo Escobar

University of Manitoba, Canada; Universidad Autonoma del Carmen, Mexico

High-Frequency Induction Heating for Small-Foreign-Metal Particle Detection using 400 kHz SiC-MOSFETs Inverter 5133

Takuya Shijo, Shinya Kurachi, Yuki Uchino, Yujiro Noda, Hiroaki Yamada and Toshihiko Tanaka

Yamaguchi University, Japan

Compact Integrated Gate Drives and Current Sensing Solution for SiC Power Modules 5139
Dazhong Gu and Parag Kshirsagar
United Technologies Research Center, United States

Session 151: Energy Storage Systems

Chair(s): Jae-Do Park, Bilal Akin

Fractional Converter for High Efficiency High Power Battery Energy Storage System 5144
Fei Xue, Ruiyang Yu and Alex Huang
North Carolina State University, United States

Investigation of Hybrid Electrode Optimization for Energy Storage Applications with Varying Energy and Power Requirements using HPPC Cycling 5151
Kevin J. Frankforter, M. Isabel Tejedor-Tejedor, Marc A. Anderson and Thomas M. Jahns
University of Wisconsin-Madison, United States; IMDEA Energy Institute, Spain

Modeling and State-Space Feedback Design of the Battery Current Controller for the Energy Stored Quasi-Z-Source Inverter 5159
Dongqi Fan, Yujie Wang, Sideng Hu, Min Chen and Xiangning He
Zhejiang University, China

A Novel Battery Management System using a Duality of the Adaptive Droop Control Theory 5164
Sifat M. Chowdhury, Mohamed Badawy, Yilmaz Sozer and J. Alexis De Abreu-Garcia
University of Akron, United States; San Jose State University, United States

Session 152: Power Conversion Systems for AC and DC Grids

Chair(s): Yazan Alsmadi, Srdjan Lukic

A Modular SCR-based DC-DC Converter for Medium-Voltage Direct-Current (MVDC) Grid Applications 5170
Abdulgafor Alfares, Ehsan Afshari, Mahshid Amirabadi and Brad Lehman
Northeastern University, United States

N-Series Modules based on SST for Mobile Power Substations 5178
Cheng Deng, Tao Yang and Juan Carlos Balda
University of Arkansas, United States; Xiangtan University, China

Re-Synchronization Strategy for the Synchronous Power Controller in HVDC Systems 5186
Cristian Verdugo, Jose Ignacio Candela and Pedro Rodriguez
Polytechnic University of Catalonia, Spain; Loyola Andalucía University, Spain

A Design Method of MMC-HVDC Physical Simulation System 5192
Liu Dong, He Zhiyuan, Gao Lu and Kou Longze
Global Energy Interconnection Research Institute, China

Session 153: Power Quality of Grid Connected Converters II

Chair(s): Liuchen Chang, Jonathan Kimball

Four-Wired Dynamic Voltage Restorers based on Cascade Open-End Winding Transformers 5198
Gregory A.A. Carlos, Cursino B. Jacobina, Joao P.R.A. Mello and Alexandre C. Oliveira
Federal Institute of Alagoas, Brazil; Federal University of Campina Grande, Brazil

Investigation of CCL Filter for Multilevel Selective Harmonic Compensation (SHC) with Staircase Waveform 5206
Hui Zhao, Shuo Wang, Amirhossein Moeini and Le Yang
University of Florida, United States

Power Electronics Intelligence at the Network Edge (PINE) 5214
Hung-Ming Chou, Le Xie, Prasad Enjeti and P.R. Kumar
Dominion Energy, United States; Texas A&M University, United States

Performance Investigation of Hybrid Active Filter During Low Load Condition 5222
Richard Beddingfield, David Storelli, Hesam Mirzaee and Subhashish Bhattacharya
North Carolina State University, United States; Quanta Technology, United States

Session 154: Modeling and Monitoring of Batteries I
Chair(s): Veda Prakash Galigekere, Fei Gao

On-Board State-of-Health Estimation based on Charging Current Analysis for LiFePO₄ Batteries 5229
Jufeng Yang, Bing Xia, Wenxin Huang and Chris Mi
Nanjing University of Aeronautics and Astronautics, China; San Diego State University, United States; University of California-San Diego, United States

A Compact Unified Methodology via a Recurrent Neural Network for Accurate Modeling of Lithium-Ion Battery Voltage and State-of-Charge 5234
Ruxiu Zhao, Phillip J. Kollmeyer, Robert D. Lorenz and Thomas M. Jahns
University of Wisconsin-Madison, United States

A Novel Li-Ion Battery Pack Modeling Considering Single Cell Information and Capacity Variation ... 5242
Jaehyung Lee, Jung-Hoon Ahn and Byoung Kuk Lee
Sungkyunkwan University, Korea

A Real-Time Condition Monitoring for Lithium-Ion Batteries using a Low-Priced Microcontroller 5248
Taesic Kim, Amit Adhikaree, Daewook Kang, Myoung-ho Kim, Chang-Yeol Oh and Juwon Baek
Texas A&M University-Kingsville, United States; Korea Electrotechnology Research Institute, Korea

Session 155: Multilevel Converters I
Chair(s): Pericle Zanchetta, Luca Solero

Interleaved Operation of Paralleled Neutral-Point Clamped Inverters with Reduced Circulating Current 5254
Zhi-Xiang Zou, Frederik Hahn, Sebastian Brueske, Sandro Guenter, Giampaolo Buticchi, Marco Liserre and Friedrich W. Fuchs
Christian-Albrechts-Universität zu Kiel, Germany

A New Modulation Method for a Five-Level Hybrid-Clamped Inverter with Reduced Flying Capacitor Size 5262
Boran Fan, Kui Wang, Zedong Zheng, Lie Xu and Yongdong Li
Tsinghua University, China

A Novel Multilevel Converter with Reduced Switch Count for Low and Medium Voltage Applications 5267
Margarita Norambuena, Jose Rodriguez, Samir Kouro and Akshay Rathore
Universidad Tecnica Federico Santa Maria, Chile; Universidad Andres Bello, Chile; Concordia University, Canada

Five-Level Reduced Hybrid Inverter with Coupled Inductors 5273
Diego A. Acevedo-Bueno, Juliano C. Leal da Silva, Edison Roberto C. da Silva and Montie A. Vitorino
UFCEG, Brazil; UFPB, Brazil

Session 156: PFC Converters

Chair(s): Gerry Moschopoulos, Giacomo Scelba

Dynamic Response Optimization for Interleaved Boost PFC Converter with Improved Dual Feedforward Control 5280
Lei Bai, Xiaoyong Ren, Qi Hui, Yu Wu, Kunqi Li, Zhehui Guo and Yue Zhang
Nanjing University of Aeronautics and Astronautics, China; State Grid Nanjing Power Supply Company, China

Manitoba Rectifier – Bridgeless Buck-Boost PFC 5287
Ken King Man Siu and Carl Ngai Man Ho
University of Manitoba, Canada

Low THD Multipliers for BCM Buck and Cascaded Buck-Boost PFC Converters 5293
Ramanujam Ramabhadran, Yehuda Levy, Bruce Roberts and Pradeep V.
GE Global Research, United States

Multi-Objective Optimisation of a Bidirectional Single-Phase Grid Connected AC/DC Converter (PFC) with Two Different Modulation Principles 5298
Johan Le Leslé, Rémy Caillaud, Florent Morel, Nicolas Degrenne, Cyril Buttay, Roberto Mrad, Christian Vollaire and Stefan Mollov
Mitsubishi Electric R&D Centre Europe, France; Université de Lyon, France

Session 157: Modeling and Control of DC-DC Converters II

Chair(s): Xinbo Ruan, Khurram Afridi

Approximate-Model-based Predictive Current Control for Buck Converter in CCM 5306
Benfei Wang, Liang Xian, Abhisek Ukil and Hoay Beng Gooi
Nanyang Technological University, Singapore

Stable Output Current Estimation for Switching Power Converter 5312
Hidenori Maruta, Shingo Watanabe, Nobumasa Matsui, Fujio Kurokawa and Ilhami Colak
Nagasaki University, Japan; Nagasaki Institute of Applied Science, Japan; Nisantasi University, Japan

Design and Optimization of the High Frequency Transformer for a 800V/1.2MHz SiC LLC Resonant Converter 5317
Suxuan Guo, Pengkun Liu, Liqi Zhang and Alex Q. Huang
North Carolina State University, United States; Texas Instruments Inc., United States

Extension of Zero-Voltage-Switching Range in Dual Active Bridge Converter by Switched Auxiliary Inductance 5324
Hayato Higa and Jun-ichi Itoh
Nagaoka University of Technology, Japan

Session 158: Modeling and Control of DC-AC Converters I

Chair(s): Luca Zarri, Yi Tang

IGBT-SiC Dual Fed Ground Power Unit 5332

Luca Rovere, Andrea Formentini, Giovanni Lo Calzo, Pericle Zanchetta, Andrea Cassia and Mario Marchesoni

University of Nottingham, United Kingdom; University of Genova, Italy

Multi-Rate Modeling for Low Switching Frequency VSCs Applying Multi-Sampling Control 5339

Hao Tian, Yun Wei Li and Qing Zhao

University of Alberta, Canada

H-Infinity Current Control of the LC Coupled Voltage Source Inverter 5347

Lucas Koleff, Lourenco Matakas Jr., Diego Colon and Eduardo Pellini

University of Sao Paulo, Brazil

Analytical Averaged Loss Model of Three-Phase T-type STATCOM with Virtual Zero Level Modulation 5355

Jun Wang, Xibo Yuan, Yonglei Zhang, Kfir J. Dagan, Xu Liu, David Drury, Phil Mellor and Andrew Bloor

University of Bristol, United Kingdom; Safran Electrical and Power UK, United Kingdom

Session 159: EMI in Power Converters

Chair(s): Jason Lai, Lixiang Wei

A Symmetrical Resonant Converter and PCB Transformer Structure for Common Mode Noise Reduction 5362

Bin Li, Qiang Li, Fred C. Lee and Yuchen Yang

Virginia Polytechnic Institute and State University, United States

Aperiodic Pulse-Modulation Technique to Reduce Peak EMI in Impedance-Source DC-DC Converters 5369

Saad Ul Hasan, Yuba Raj Kafle and Graham E. Town

Macquarie University, Australia

Integrated Common Mode and Differential Mode Inductors with Low Near Magnetic Field Emission 5375

Huan Zhang, Boyi Zhang and Shuo Wang

University of Florida, United States

Design, Implementation, and Evaluation of a GaN-based Four-Leg Inverter with Minimal Common Mode Voltage Generation 5383

Di Han, Silong Li, Wooyoung Choi and Bulent Sarlioglu

University of Wisconsin-Madison, United States

Session 160: High Speed Machines

Chair(s): Jonathan Bird, Ronghai Qu

Design and Rotor Shape Modification of a Multiphase High Speed Permanent Magnet Assisted Synchronous Reluctance Motor for Stress Reduction 5389

Md Tawhid Bin Tarek and Seungdeog Choi

University of Akron, United States

Rotor Losses Reduction in High Speed PM Generators for Organic Rankine Cycle Systems 5396
Grazia Berardi and Nicola Bianchi
University of Padova, Italy

Ripple Compensation of Suspension Force and Torque in a Bearingless SPM Motor with Integrated Winding 5403
Junichi Asama, Kenta Sasaki, Takaaki Oiwa and Akira Chiba
Shizuoka University, Japan; Tokyo Institute of Technology, Japan

Electromagnetic and Thermodynamic Design of a Novel Integrated Flux-Switching Motor-Compressor with Airfoil-Shaped Rotor 5409
Hao Ding, Yingjie Li, Seun Guy Min and Bulent Sarlioglu
University of Wisconsin-Madison, United States

Session 161: Noise, Vibration, Short Circuit of Electric Machines
Chair(s): Konstantinos Gyftakis, Rashmi Prasad

Inter-Turn Short Circuit Ratio Estimation in IPMSMs based on a Fault Index Current Observer 5417
Pablo Castro Palavicino, Dheeraj Bobba and Bulent Sarlioglu
University of Wisconsin-Madison, United States

A Review of Condition Monitoring of Induction Motors based on Stray Flux 5424
Chen Jiang, Sufei Li and Thomas G. Habetler
Georgia Institute of Technology, United States

Investigation of Design based Solutions to Reduce Vibration in Permanent Magnet Synchronous Machines with Low Order Radial Forces 5431
Iftekhhar Hasan, Yilmaz Sozer, Alejandro Piña Ortega, Subhra Paul and Rakib Islam
University of Akron, United States; Nexteer Automotive, United States

Analysis of Vibration of Permanent Magnet Synchronous Motor with Distributed Winding for the PWM Method of Voltage Source Inverters 5438
Takafumi Hara, Toshiyuki Ajima, Yousuke Tanabe, Masanori Watanabe, Katsuhiro Hoshino and Kazuto Oyama
Hitachi, Ltd., Japan; Hitachi Automotive Systems Ltd., Japan

Session 162: Electric Drives for Aerospace and Traction Applications
Chair(s): John Neely, Long Wu

A Current-Fed Quasi Z-Source Inverter with SiC Power Modules for EV/HEV Applications 5445
Faris E. Alfaris and Subhashish Bhattacharya
North Carolina State University, United States

High Performance 12 kW Motor and Drive for Modern Aircrafts 5453
Sayeed Mir, John Neely and Stan Seely
Eaton Aerospace, United States

Temperature Effects Compensation Control Algorithm of IPM Machines Utilizing Current Pulse Injection and Online Multi-Parameter Estimation for Traction Applications 5461
Silong Li, Di Han and Bulent Sarlioglu
University of Wisconsin-Madison, United States

A Versatile Power-Hardware-in-the-Loop based Emulator for Rapid Testing of Electric Drives 5468

Amitkumar K.S., R. Sudharshan Kaarthik and Pragasen Pillay

Concordia University, Canada; Indian Institute of Space Science and Technology, India

Session 163: SiC Switching II

Chair(s): Keiji Wada, Ben Guo

Extraction of Parasitic Inductances of SiC MOSFET Power Modules based on Two-Port S-Parameters Measurement 5475

Tianjiao Liu, Yanjun Feng, Runtao Ning, Wendi Wang, Thomas T.Y. Wong and Z. John Shen

Illinois Institute of Technology, United States

High Speed dV/dt Control Technology for SiC Power Module for EV/HEV Inverters 5483

Taku Shimomura, Takayuki Ikari, Akinori Okubo, Ryusei Yamada and Tetsuya Hayashi

Nissan Motor Co., Ltd., Japan

Switching Performance of a SiC MOSFET Body Diode and SiC Schottky Diodes at Different Temperatures 5487

M.R. Ahmed, R. Todd and A.J. Forsyth

University of Manchester, United Kingdom

Digital Control based Voltage Balancing for Series Connected SiC MOSFETs under Switching Operations 5495

Katsuya Shingu and Keiji Wada

Tokyo Metropolitan University, Japan

Session 164: Wireless Power Transfer IV

Chair(s): Huang-jen Chiu, Luis Herrera

Optimization of Coils and Control Strategy for a Three-Phase Magnetically Coupled Resonant Wireless Power Transfer System Oriented by the Optimal Output Power Characteristics 5501

Xiewei Fu, Fuxin Liu and Xuling Chen

Nanjing University of Aeronautics and Astronautics, China

Radiation Noise Reduction using Spread Spectrum for Inductive Power Transfer Systems considering Misalignment of Coils 5507

Keisuke Kusaka, Kent Inoue and Jun-ichi Itoh

Nagaoka University of Technology, Japan

Maximum Power Point Tracker for Electromagnetic Energy Harvesting System 5515

Kimberley Hiu Kwan Tse and Henry Shu Hung Chung

City University of Hong Kong, Hong Kong

Exciting Voltage Control for Transfer Efficiency Maximization for Multiple Wireless Power Transfer Systems 5523

Masato Sasaki and Masayoshi Yamamoto

Sharp Corporation, Japan; Shimane University, Japan

Session 165: Hybrid Energy Systems

Chair(s): Jiacheng Wang, Jorge Garcia Garcia

Direct Storage Hybrid (DSH) Inverter: A New Concept of Intelligent Hybrid Inverter 5529

Ha Pham

University of Technology Sydney, Australia

New Soft-Switched High Frequency Multi-Input Step-up/down Converters for High Voltage DC-Distributed Hybrid Renewable Systems 5537

Sanjida Moury and John Lam

York University, Canada

Optimal Sizing of Photovoltaic-Wind Hybrid System for Community Living Environment and Smart Grid Interaction 5545

Mohammad B. Shadmand, Mehran Mirjafari and Robert S. Balog

Kansas State University, United States; Dell Inc., United States; Texas A&M University, United States

Modeling and Control of Brushless DC Motor for Compressor Driving 5553

Zhiguang Hua, Dongdong Zhao, Manfeng Dou, Liming Yan and Haitao Zhang

Northwestern Polytechnical University, China

Session 166: Wave Energy System

Chair(s): Martin Ordonez, Mazharul Chowdhury

Electromechanical Design and Experimental Evaluation of a Double-Sided, Dual Airgap Linear Vernier Generator for Wave Energy Conversion 5557

Jennifer Vining, Tim Mundon and Balky Nair

Oscilla Power, United States

Grid-Connected Operation of Direct-Drive Wave Energy Converter by using HVDC Line and Undersea Storage System 5565

Seyyedmahdi Jafarishiadeh, Mehdi Farasat and Shahab Mehraeen

Louisiana State University, United States

Power Conversion and Control of a Pole-Modulated Permanent Magnet Synchronous Generator for Wave Energy Generation 5572

Samir Hazra, Prathamesh Kamat, Subhashish Bhattacharya, Wen Ouyang and Steven Englebretson

North Carolina State University, United States; ABB Corporate Research Center, United States

Competitive Control of Wave Power Plants through Price-Signal Optimum Allocation of Available Resources 5579

Antoni M. Cantarellas, Daniel Remon, Jorge M. Garcia and Pedro Rodriguez

Abengoa, Spain; Technical University of Catalonia, Spain; Loyola Andalucía University, Spain

Session 167: Grid Connected Inverters and LCL Filter Design

Chair(s): Edison da Silva, Mahshid Amirabadi

Analysis and Design of LCL Filter based Synchronverter 5587

Roberto Rosso, Jair Cassoli, Soenke Engelken, Giampaolo Buticchi and Marco Liserre

WRD GmbH, Germany; Christian-Albrechts-University of Kiel, Germany

A Common Magnetic Integration Method for Single-Phase LCL Filters and LLCL Filters	5595
Xiaoqiang Li, Jingyang Fang, Pengfeng Lin and Yi Tang <i>Nanyang Technological University, Singapore</i>	
Investigation of the Sideband Effect for the LCL-type Grid-connected Inverter with High LCL Resonance Frequency	5601
Dongsheng Yang, Xiongfei Wang and Frede Blaabjerg <i>Aalborg University, Denmark</i>	
An Improved Active Damping Method with Grid-Side Current Feedback to Maximize Damping Ratio for LCL-Type Grid-Connected Inverter	5607
Weibiao Wu, Li Peng, Yu Qi, Qian Liu, Zeyi Huang, Fangming Dong, Manlin Chen and Bowen Wang <i>Huazhong University of Science and Technology, China; CRRC Zhuzhou institute Co., Ltd., China; Commercial Aircraft Corporation of China, Ltd., China; Shenzhen Hopewind Electric Co., Ltd., China</i>	
Session 168: Modeling and Monitoring of Batteries II	
Chair(s): Phillip Kollmeyer, Mohammad Anwar	
An Advanced SOF Estimation Algorithm for LiFePO4 SLI Battery of Vehicle with Online Update of Cranking Resistance	5612
Tae-Won Noh, Jung-Hoon Ahn and Byoung Kuk Lee <i>Sungkyunkwan University, Korea</i>	
Online Condition Monitoring of Lithium-Ion Batteries using Impedance Spectroscopy	5617
Sean Moore and Paul Barendse <i>University of Cape Town, South Africa</i>	
A New State of Charge Estimation Method for Lithium-Ion Battery based on Sliding Mode Observer	5625
Chunyu Wang, Naxin Cui, Miao Liu and Chenghui Zhang <i>Shandong University, China</i>	
Accelerated Ageing of Lithium-Ion Batteries based on Electric Vehicle Mission Profile	5631
Daniel-Ioan Stroe, Maciej Swierczynski, Søren Knudsen Kær, Egoitz Martinez Laserna and Elixabet Sarasketa Zabala <i>Aalborg University, Denmark; IK4-Ikerlan, Spain</i>	
Session 169: Single-Phase AC/DC Converters	
Chair(s): Hongliang Wang, Petar Grbovic	
Half-Wave Class DE Low dv/dt Rectifier using Thinned-Out Method with Delta-Sigma Modulation	5638
Akinobu Shigeno and Hirotaka Koizumi <i>Tokyo University of Science, Japan</i>	
A Single-Stage Asymmetrical Half-Bridge AC/DC Converter with Coupled Inductors	5645
Chia-Hao Li, Ying-Ting Huang, Yaow-Ming Chen and Yung-Ping Tong <i>National Taiwan University, Taiwan; Lite-On Technology Corporation, Taiwan</i>	
A 220-V AC, LUT-Controlled 6-Segmented LED Driver with Background Calibration	5651
Hyunseung Lee, Eunseo Kim and Jaeha Kim <i>Seoul National University, Korea</i>	

A Moving Pole-Placement Compensation Design Method to Increase the Bandwidth of RC-Damper-based Dual “Buck-Boost” AC/DC Converter 5657
Weimin Wu, Weibo Qin, Houqing Wang, Min Huang, Frede Blaabjerg and Marco Liserre
Shanghai Maritime University, China; Aalborg University, Denmark; Kiel University, Germany

Session 170: Multilevel Converters II
Chair(s): Alessandro Costabeber, Yi Tang

On-Line Switching Loss Reduction Scheme by General Space Vector PWM for Multilevel NPC Inverter 5665
Toshiji Kato, Kaoru Inoue and Takumi Sono
Doshisha University, Japan

Three-Level Two-Stage Decoupled Active NPC Converter with Si IGBT and SiC MOSFET 5671
Di Zhang, Jiangbiao He and Sachin Madhusoodhanan
GE Global Research Center, United States

A Ladder Transistor-Clamped Multilevel Inverter with High-Voltage Variation 5679
Eshet T. Wodajo, Malik Elbuluk, Seungdeog Choi and Haitham Abu Rub
University of Akron, United States; Texas A&M University at Qatar, Qatar

Predictive Control of Modular Multilevel Series/Parallel Converter for Battery Systems 5685
Zhongxi Li, Ricardo Lizana, Angel V. Peterchev and Stefan M. Goetz
Duke University, United States; Universidad Católica de la Santísima Concepción, Chile

Session 171: Isolated DC/DC Converters
Chair(s): Luca Tarisciotti, Alireza Safaee

High-gain Soft-switching DC-DC Converter with Voltage-doubler Rectifier Modules 5692
Rohit Suryadevara, Tao Li, Kumar Modepalli and Leila Parsa
Rensselaer Polytechnic Institute, United States; Dialog Semiconductor, United States; FINsix Corporation, United States; University of California Santa Cruz, United States

Driving Piezoelectric-Transformer-based DC/DC Converters using Pulse Density Modulation 5698
Juan Diaz, Miguel J. Prieto, Fernando Nuno, Juan A. Martín-Ramos and Juan A. Martínez
University of Oviedo, Spain

Bidirectional DC-DC Converter Utilizing Magnetic and Capacitive Power Transfer – 97.1% Efficiency at 1.2-MHz Switching 5704
Jong-Won Shin, Masanori Ishigaki, Ercan M. Dede and Jae Seung Lee
Toyota Research Institute of North America, United States; Toyota Central RD Labs., Inc., Japan

LLC Resonant Converter with Shared Power Switches and Dual Coupled Resonant Tanks to Achieve Automatic Current Sharing 5712
Hongliang Wang, Yang Chen, Yan-Fei Liu, Zhihua Yang, Jahangir Afsharian and Bing Gong
Queen's University, Canada; Murata Power Solutions, Canada

Session 172: Grid Synchronization Techniques

Chair(s): Zheng Wang, Alireza Bakhshai

A Voltage Sensorless Phase Locked Loop Structure for Single Phase Grid Connected Converter System 5720

Subhajyoti Mukherjee, Vikram Roy Chowdhury, Pourya Shamsi and Mehdi Ferdowsi
Missouri University of Science and Technology, United States

Comparative Analysis about Dynamic Performances of Grid Synchronization Schemes 5726

Hao Yi, Xiongfei Wang, Frede Blaabjerg and Fang Zhuo
Xi'an Jiaotong University, China; Aalborg University, Denmark

A Phase-Locked Loop based on Cascaded Least-Error Squares Filter 5731

Bowen Wang, Li Peng, Manlin Chen, Weibiao Wu and Yuntao Xiao
Huazhong University of Science and Technology, China

New Frequency and Amplitude Estimation Techniques for Grid-Connected DC/AC Inverters 5738

Iman Askarian, Suzan Eren, Majid Pahlevani and Andy Knight
University of Calgary, Canada; Queen's University, Canada

Session 173: Modeling and Control of DC-AC Converters II

Chair(s): Leon M Tolbert, Dong Dong

Anti-Windup Control for Stationary Frame Current Regulators using Digital Conditioning Architectures 5744

B.P. McGrath and D.G. Holmes
RMIT University, Australia

A Current Sharing Technique for Parallel-Operated Unipolar-PWM Inverters 5752

Dong Li, Carl Ngai Man Ho and Ken King Man Siu
University of Manitoba, Canada

Low Frequency Current Ripple Reduction of a Current-Fed Switched Inverter 5760

Anil Gambhir and Santanu Mishra
Indian Institute of Technology Kanpur, India

Accuracy Analysis of the Zero-Order Hold Model for Digital Pulsewidth Modulation 5767

Junpeng Ma, Xiongfei Wang, Frede Blaabjerg, Lennart Harnefors and Wensheng Song
Southwest Jiaotong University, China; Aalborg University, Denmark; ABB Corporate Research Center, Sweden

Session 174: Testing, Measurement, and Validation of Power Converters

Chair(s): Vladimir Blasko, Qin Lei

DC Current Determination in Grid-Connected Transformerless Inverter Systems using a DC Link Sensing Technique 5775

Weichi Zhang, Matthew Armstrong and Mohammed Elgendy
Newcastle University, United Kingdom

Online Measurement of Bus Impedance of Interconnected Power Electronics Systems: Applying Orthogonal Sequences 5783

Tomi Roinila, Hessamaldin Abdollahim, Silvia Arrua and Enrico Santi
University of South Carolina, United States

Switching Frequency Characterization of Hysteresis Control in a Pump Back Test Configuration 5789

Xu She, Tony Frangieh and Rajib Datta
GE Global Research, United States

Capacitance Estimation Algorithm based on DC-Link Voltage Harmonics Using Artificial Neural Network in Three-Phase Motor Drive Systems 5795

Hammam Soliman, Pooya Davari, Huai Wang and Frede Blaabjerg
Aalborg University, Denmark; Arab Academy for Science and Technology, Egypt

Session 175: Motors for Transportation

Chair(s): Ronghai Qu, Khwaja Rahman

Principle of Variable Leakage Flux IPMSM using Arc-Shaped Magnet Considering Variable Motor Parameter Characteristics Depending on Load Current 5803

Takashi Kato, Toru Matsuura, Kensuke Sasaki and Tsutomu Tanimoto
Nissan Motor Co., Ltd., Japan

Performance Analysis of Surface Permanent Magnet Synchronous Machine Topologies with Dual-Wound Stators 5811

Subhra Paul, Alejandro Piña Ortega, Cong Ma, Rakesh Mitra, Prerit Pramod and Rakib Islam
Nexteer Automotive Corp., United States

Breakdown Resistance Analysis of Traction Motor Winding Insulation under Thermal Ageing 5819

K.N. Gyftakis, P.A. Panagiotou, N. Lophitis, D.A. Howey and M.D. McCulloch
Coventry University, United Kingdom; University of Oxford, United Kingdom

High Torque Density PM Motor for Racing Applications 5826

Marco Munaro, Nicola Bianchi and Giovanni Meneghetti
University of Padova, Italy

Session 176: General Topics in Electrical Machines

Chair(s): Jose Antonino-Daviu, Dong Jiang

Design and Experimental Evaluation of a Multilayer AC Winding Configuration for Sinusoidal MMF with Shorter End-turn Length 5834

Md Ashfanor Kabir, Mohamed Zubair M. Jaffar, Zhao Wan and Iqbal Husain
North Carolina State University, United States

Impact of Machine Magnetization State on Permanent Magnet Losses in Permanent Magnet Synchronous Machines 5840

Daniel Fernández Alonso, David Reigosa, Juan Guerrero, Carlos Suarez and Fernando Briz
University of Oviedo, Spain

Operating Limits and Practical Operation of a Brushless Doubly-Fed Reluctance Machine 5846

William K. Song, David G. Dorrell, Andrew M. Knight, Robert E. Betz and David Gay
University of Technology Sydney, Australia; University of KwaZulu-Natal, South Africa; University of Calgary, Canada; University of Newcastle, Australia

A Novel Flux-Reversal Hybrid Magnet Memory Machine 5853

Hui Yang, Heyun Lin, Z.Q. Zhu, Haitao Wang, Shuhua Fang and Yunkai Huang
Southeast University, China; University of Sheffield, United Kingdom

Session 177: PM and IPM Motor Drives III

Chair(s): Bilal Akin, Annette Muetze

- Online Stator Resistance Tracking for Reluctance and Interior Permanent Magnet Synchronous Motors** 5861
R. Antonello, L. Ortombina, F. Tinazzi and M. Zigliotto
University of Padova, Italy
- On-Line Stator Resistance and Permanent Magnet Flux Linkage Identification on Open-end Winding PMSM Drives** 5869
M. Pulvirenti, G. Scarcella, G. Scelba, A. Testa and M.M. Harbaugh
University of Catania, Italy; University of Messina, Italy; Rockwell Automation, United States
- Quick Compensation Method of Motor Phase Current Sensor Offsets without Motor Parameters for PMSM Drive** 5877
Koroku Nishizawa, Jun-ichi Itoh and Yoshinobu Nishizawa
Nagaoka University of Technology, Japan
- Analytical Design and Auto-Tuning of Adaptive Flux-Weakening Voltage Regulation Loop in IPMSM Drives with Accurate Torque Regulation** 5884
Nicola Bedetti, Sandro Calligaro and Roberto Petrella
Gefran S.p.A., Italy; Free University of Bozen, Italy; University of Udine, Italy

Session 178: Device Self Sensing Techniques

Chair(s): Adam Skorek, Jing Xu

- Elimination of Bus Voltage Impact on Temperature Sensitive Electrical Parameter During Turn-on Transition for Junction Temperature Estimation of High-power IGBT Modules** 5892
Haoze Luo, Francesco Iannuzzo, Frede Blaabjerg, Xiang Wang, Wuhua Li and Xiangning He
Aalborg University, Denmark; University of Cassino and Southern Lazio, Italy; Zhejiang University, China
- IGBT Junction Temperature Estimation via Gate Voltage Plateau Sensing** 5899
Christoph H. van der Broeck, Alexander Gospodinov and Rik W. De Doncker
RWTH Aachen University, Germany
- On-Line Temperature Estimation of SiC Power MOSFET Modules through On-State Resistance Mapping** 5907
Fausto Stella, Gianmario Pellegrino, Eric Armando and Davide Daprà
Politecnico di Torino, Italy; Vishay Semiconductor Italiana S.p.A., Italy
- Characterization of SenseGaN Current-Mirroring for PowerGaN with the Virtual Grounding in a Boost Converter** 5915
Mehrddad Biglarbegian and Babak Parkhideh
University of North Carolina at Charlotte, United States

Power Quality Improvement Utilizing Photovoltaic Generation Connected to a Weak Grid

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Abstract—Microgrid research and development in the past decades have been one of the most popular topics. Similarly, the photovoltaic generation has been surging among renewable generation in the past few years, thanks to the availability, affordability, technology maturity of the PV panels and the PV inverter in the general market. Unfortunately, quite often, the PV installations are connected to weak grids and may have been considered as the culprit of poor power quality affecting other loads in particular sensitive loads connected to the same point of common coupling (PCC). This paper is intended to demystify the renewable generation, and turns the negative perception into positive revelation of the superiority of PV generation to the power quality improvement in a microgrid system. The main objective of this work is to develop a control method for the PV inverter so that the power quality at the PCC will be improved under various disturbances. The method is to control the reactive current based on utilizing the grid current to counteract the negative impact of the disturbances. The proposed control method is verified in PSIM platform. Promising results have been obtained.

Keywords—Photovoltaic, PV, solar power, power quality, reactive power, unbalance, symmetrical, weak grid.

I. INTRODUCTION

Nowadays, most of the renewable energy sources such as Photovoltaic (PV) panels are connected to the grid using inverters. They can feed substantial power to the grid. However, high penetration levels of PV panels could bring significant impacts to the power system. A review of some reports and a survey to utility engineers regarding impacts of PV penetration is presented in [1]. Several concerns about high PV penetration include transient condition during cloud passing, voltage rise in steady state and the need to include voltage regulation in PV inverters.

Since the voltage regulation corresponds to reactive power flow in power system, a PV inverter should have an additional capability to control the reactive power flow. Thus, the PV plant would provide voltage support in steady state and transient (fault) condition in order to reduce network losses and improve transmission capacity.

Many studies about reactive power control in a grid-connected PV inverter have been done [2]-[7][9]. Generally, a PV inverter absorbs or injects reactive power or current depending upon its control strategies, such as constant voltage,

constant reactive power, or constant power factor type. The control strategy is commonly supported by a PI controller or a V-Q slope characteristic. It is also possible to employ an intelligent controller [7]. Some controllers work in a dq reference frame to simplify the control process. Reactive power flow can also be determined by active power flow associated to system impedance (R_s/X_s). For unbalanced system, it is common for PV and other distributed generation inverters to apply a symmetrical component method in the control process [6][9]-[11]. In [6], the controller defines control parameters (k^+ and k^-) to balance the positive- and negative-sequence voltages (voltage equalizing strategy). Moreover, the injected reactive current to the grid is mostly based on the required voltage or power. To convert to the current, the process frequently needs extensive calculation. In this paper, a different approach to the control strategy is based on utilizing the available reactive current flowing in the power system, which corresponds to system voltage. Different from the previous approaches, the strategy is simple, comprehensive and robust, because the reactive current produced by the PV generator just emulates to the reactive current circulating in the grid. Since the main objective of this research is to improve the grid power (voltage) quality, this system is also effective for all conditions especially unsymmetrical faults.

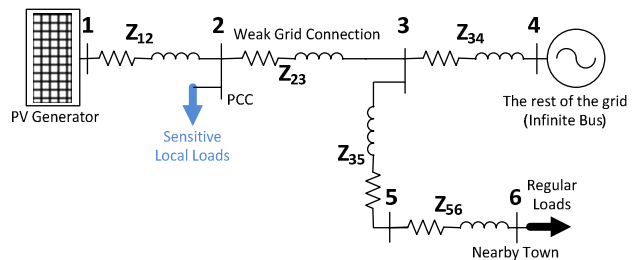


Figure 1. A single line diagram of a typical PV installation.

A typical system of interest is illustrated in the single line diagram in Fig. 1. As shown, a typical PV installation is connected to the main grid via weak lines (weak grid system). On the same site, regular loads and sensitive loads (e.g. medical equipment, computer center, and a radar installation) may be connected to the same bus. The major concern is mostly on the

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power quality of the grid at the installation of the PV inverter, that may affect the performance of the loads connected to the point of common coupling (PCC). This paper intends to reveal the benefit of PV generation and the significance of the proposed control strategy to the power (voltage) quality improvement in a microgrid system.

II. PV INVERTER TO IMPROVE POWER QUALITY

PV panels convert solar energy to electrical energy. They generate active power in a DC quantity. In order to deliver the active power from PV panels to the grid, an inverter along with a MPPT controller is commonly used to interface PV panels to the grid. In addition, the PV inverter will be equipped with a reactive power controller.

A. PV Model

The PV generator consists of PV panels and a PV inverter along with its controller. The DC side of the PV inverter is attached to PV panels, and the AC side of the PV inverter is connected to the grid. PV panels generally operate as a current source. While a grid-connected PV inverter works in a current-controlled mode [6][9][10][12]. The PV inverter and its controller determine the PV output currents sent to the grid, which is usually based on sliding mode control [12]. This paper chooses a three-phase dependent current source as an average model for representing the PV generator. The Norton equivalent circuit of the dependent current source is shown in Fig. 2, where I_{a-pv} , I_{b-pv} and I_{c-pv} are connected to a three-phase reference current of the controller ($I_{ref(a,b,c)}$).

B. PV Controller

The PV output currents comprise of the active and reactive current. To produce the PV output currents, the controller has to drive the PV inverter using the three-phase reference current ($I_{ref(a,b,c)}$). The main block diagram of the PV inverter control strategy is shown in Fig. 3.

The quantity of active power sent to the grid is determined by the intensity of sunlight striking on PV panels as well as the environment surrounding the panels. To get maximum active power, the PV inverter is supported by the maximum power point tracking (MPPT) controller, which regulates the DC-bus voltage [12]. Hence, the active power delivered to the grid is relatively independent on the electric power system condition. On the other hand, the active power from PV panels may influence the performance of the power system.

Different from active power flow, the PV generator will contribute reactive currents flowing to the grid. The reference current for reactive currents as well as unbalanced currents will be constructed by utilizing grid currents. According to Watanabe [13], instantaneously, reactive power is being exchanged between phases of the power system. The reactive as well as unbalanced current is flowing in the power system without transferring energy.

Therefore, the controller has to sense the currents flowing in the grid. A current sensor is placed on each phase of the grid to detect three-phase grid currents ($I_{grid} = I_{43}$). Based on the three-phase grid current, the control strategy focuses on

developing a three-phase active positive-sequence current ($I_{+active(a,b,c)}$).

From the output signals of grid current sensors, the controller separates the grid currents into positive-sequence, negative-sequence and zero-sequence current components. If the system is balanced, then the grid currents only have positive-sequence currents. To obtain the three-phase positive-sequence current ($I_{+(a,b,c)}$), the three-phase grid/line currents ($I_{grid(a,b,c)}$) are processed with symmetrical component extraction according to equation (1) and (2).

$$\begin{bmatrix} I_+ \\ I_- \\ I_0 \end{bmatrix} = \frac{1}{3} \begin{bmatrix} 1 & a & a^2 \\ 1 & a^2 & a \\ 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix} \quad (1)$$

$$\begin{bmatrix} I_{+a} \\ I_{+b} \\ I_{+c} \end{bmatrix} = \begin{bmatrix} 1 \\ a^2 \\ a \end{bmatrix} I_+ \quad (2)$$

Where:

I_a, I_b, I_c = line currents

I_+, I_-, I_0 = positive-, negative-, and zero-sequence currents

$a = e^{j120^\circ}$ and, $a^2 = e^{-j120^\circ}$

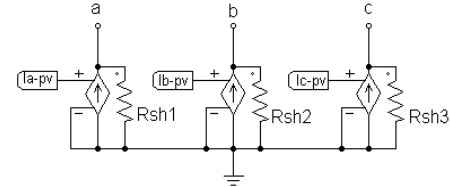


Figure 2. A three-phase PV average model

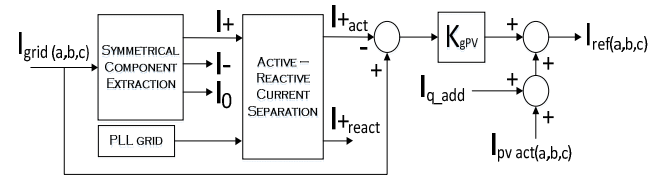


Figure 3. A block diagram of a PV inverter control strategy.

The positive-sequence currents, which are three-phase balanced currents, consist of active and reactive currents. As a consequence, the three-phase positive-sequence currents have to be split into three-phase active and reactive positive-sequence currents. To obtain the active currents, the positive-sequence currents are synchronized to the grid voltages using a phase lock loop (PLL) controller. The active currents are in-phase with the grid voltages, while the reactive currents are perpendicular to the grid voltages. Both the active and reactive positive-sequence currents are three-phase balanced currents.

$$I_{+(a,b,c)} = I_{+active(a,b,c)} + I_{+reactive(a,b,c)} \quad (3)$$

Finally, the three-phase active positive-sequence current is subtracted from the grid currents. As a result, the controller will automatically produce a three-phase reactive unbalanced current ($I_{r(a,b,c)}$), which consists of reactive currents as well as negative- and zero-sequence currents for unbalanced system.

$$I_{r(a,b,c)} = I_{grid(a,b,c)} - I_{+active(a,b,c)} \quad (4)$$

$$I_{r(a,b,c)} = I_{+reactive(a,b,c)} + I_{-(a,b,c)} + I_{0(a,b,c)} \quad (5)$$

However, the PV inverter will not employ the entire reactive unbalanced current ($I_{r(a,b,c)}$) component as for supporting the whole power system. The inverter supplies only a fraction of this current (multiplied by a gain, K_{gPV}) for improving the voltage regulation at the PCC bus. The gain K_{gPV} is a constant between 0 and 1, and is associated with the system impedance.

This current combined with the active current ($I_{PV\ active(a,b,c)}$) from PV panels will become the three-phase reference current.

$$I_{ref(a,b,c)} = I_{PV\ active(a,b,c)} + K_{gPV} I_{r(a,b,c)} \quad (6)$$

If the PV inverter possesses satisfying conversion effect, then the reference current becomes the output currents of the PV inverter (I_{PV})

$$I_{PV(a,b,c)} = I_{PV\ active(a,b,c)} + K_{gPV} (I_{+reactive(a,b,c)} + I_{-(a,b,c)} + I_{0(a,b,c)}) \quad (7)$$

Thus, the generated current by the PV generator contains the current components that will counteract the load- and disturbance-impact on the PCC voltage. As a result, the voltage at the PCC will be corrected to normal per unit value.

The main control system mentioned above is an open loop. As a result, the PCC voltages may not equal to the reference voltage, and a small voltage gap (ΔV_{PCC}) may occur. To create a close loop system, a simple PI controller will be integrated to the main controller. The PI controller adjusts the reactive current generated by the PV inverter. However, the PI controller cannot operate without the main controller since it is not capable to handle unbalance condition. The block diagram of the PI controller with anti-windup is shown in Fig. 4.

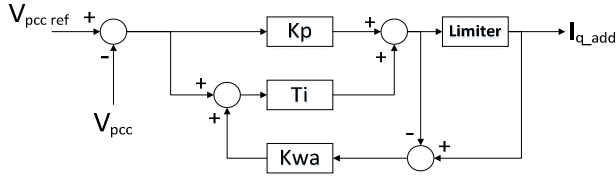


Figure 4. PI controller.

III. MICROGRID SYSTEM INVESTIGATED

A. System under Study

The system under study is depicted in Fig. 1. From the figure, it can be seen that the three-phase dependent current source representing a high power PV plant is connected to the point of common coupling (PCC – bus 2) through a star-star winding connection power transformer (represented by impedance Z_{12}). The PV plant, which is a type of distributed generation (DG), is usually located some distance away from the transmission line. Therefore, the PCC (bus 2) is connected to bus 3 via a weak grid connection, which is normally characterized by high impedance ($Z_{23} = Z_{weak}$). The short circuit ratio (SCR) at this point is smaller than 10 [8]. SCR is the ratio of PCC short circuit power to

maximum apparent power of generator. Bus 3 is the terminal of a three-phase infinite voltage source/grid with small equivalent impedance (Z_{34}).

To prove the concept proposed above, the system in Fig. 1 is simulated under dynamic conditions and transient faults. In case of the fault occurrence, the PV generator is still connected to the grid (fault ride-through) and supports the voltage level at PCC. The system parameters under study are listed in Table I.

TABLE I
SYSTEM PARAMETER UNDER STUDY

MVA base	10MVA
KV base (L-L)	20kV
Z_{12}	7%
$Z_{weak} (Z_{23})$	50% (SCR \approx 2)
Z_{34}	5%
Z_{35}	7%
Load (bus 5)	0.4pu, PF = 0.9 lag
K_{gPV}	0.1
Z_f	1%

B. Dynamic Simulations of a Quasi-Steady-State System

Under normal condition, the voltage and current of the system change dynamically due to predominantly the fluctuation of solar irradiation. In reference to Fig. 1, the voltage equation under normal condition can be presented as follow:

$$V_2 = V_3 + I_{PV} Z_{23} \quad (8)$$

Or in reference to the voltage at bus 4 (V_4), we can also write the equation as follow:

$$V_2 = V_4 - I_{43} Z_{34} + I_{PV} Z_{23} \quad (9)$$

Where

$$I_{43} = I_{35} - I_{PV} \quad (10)$$

1) Night Operation of the PV generation

At night, the PV panels do not generate active power ($P_{PV} = 0$). The PV inverter still works as a reactive power controller and generates small reactive currents. Fig. 5 shows that the load current is supplied mostly by the grid since there is no contribution of active current from PV generator. The system is stable. In this case, the system is open loop. The value of the PCC voltage (phase-neutral) is 0.992p.u.

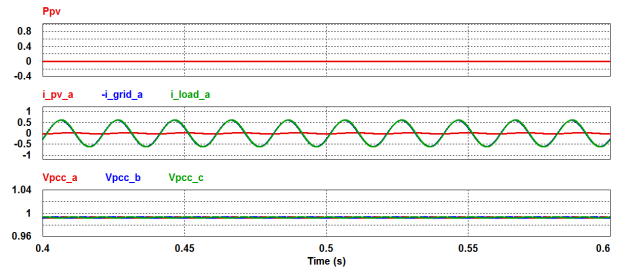


Figure 5. At night ($P_{PV} = 0$), system currents in phase A (middle), PCC voltages (bottom) for an open loop system.

Actually, the PCC voltage gap (ΔV_{PCC}) is small ($< 1\%$). However, if to fill the voltage gap is needed, the PI controller can adjust the reactive power generated by PV inverter. The PI controller output signal (I_{q_add}) will be added to the main controller output as shown in Fig. 3. Fig. 6 (bottom) shows the additional reactive power. The system is close loop and the PCC voltages equal to 1p.u.

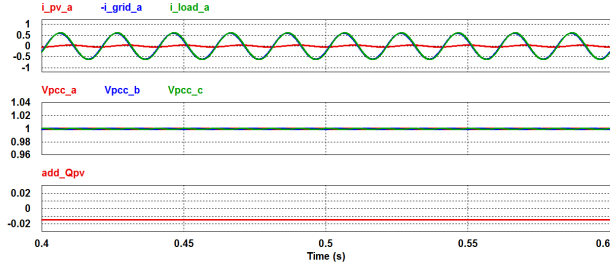


Figure 6. At night ($P_{PV} = 0$), system currents in phase A (top), and PCC voltages (1p.u) (middle), an additional reactive power (bottom) for a close loop system.

2) Power Changes of PV Generation

The fluctuation of solar irradiation due to earth rotation and weather condition as well as temporary cloud passing will vary the active power generated by PV panels. The PV active current will also change following the solar irradiation variation. The PV active current will create a voltage across Z_{23} . As a result, the PCC voltage will fluctuate according to equation (8). However, the reactive power controller will keep the PCC voltage constant at 1p.u by adjusting the reactive current component of I_{PV} .

Figure 7 shows that the active current generated by PV generator is larger than the load current. Part of the PV active current flows to the grid. From Fig. 7, when solar irradiation (PV active power (P_{PV})) fluctuates, the grid current fluctuates following the PV output current because the load current is constant. The fluctuation of solar irradiance has no effect on the system performance and stability. Fig. 8 also shows the same system performance when cloud passing occurs in a short time so that P_{PV} slightly decreases. Active power reduction depends on the cloud condition that obstructs the PV panels from sunlight.

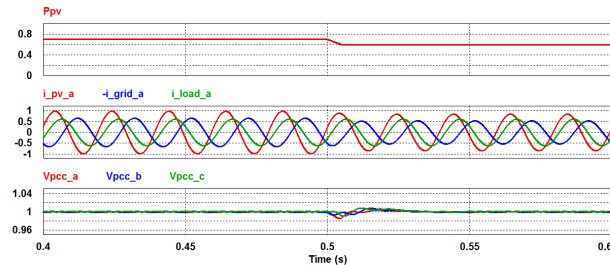


Figure 7. Solar power drops (top), system currents in phase A (middle) and PCC voltages (bottom) when solar irradiation changes

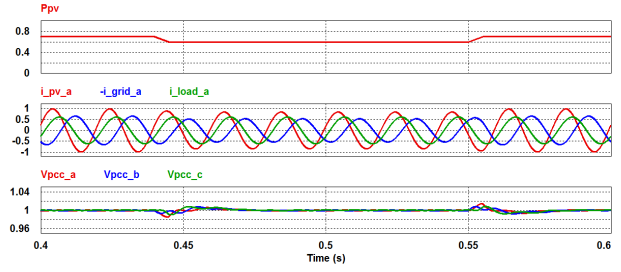


Figure 8. Solar power fluctuation (top), system currents in phase A (middle) and PCC voltages (bottom) when cloud passing

C. Dynamic Simulations under Transient Faults

The system under study experiencing different kinds of fault is depicted in Fig. 9. From this figure, only the main circuit is affected by large fault current. The branch connected to the PV plant is not drawn, because the current source nature of the PV inverter does not contribute to the fault current. The dependent current source basically generates currents according to the reference currents which consists of the active current ($I_{PV\ active}$) from PV panels and the reactive unbalanced current derived from the grid currents. Moreover, as a current source, currents from the grid are prevented flowing into the PV generator.

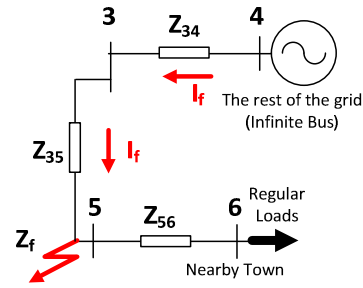


Figure 9. System under fault condition.

During the fault, $I_{35} = I_f$, and, as the amount of the fault current $I_f \gg I_{PV}$, the current contributed from the PV plant will not affect significantly the voltage at bus 3.

$$I_{43} = I_f - I_{PV} \approx I_f \quad (11)$$

The voltage at the bus 3 can be expressed as

$$V_3 = \frac{Z_f + Z_{35}}{Z_f + Z_{35} + Z_{34}} V_4 \quad (12)$$

And the voltage at the bus 5 can be expressed as

$$V_5 = \frac{Z_f}{Z_f + Z_{35} + Z_{34}} V_4 \quad (13)$$

Thus, for a solid ground fault, the voltage at bus 5 is theoretically zero. Meanwhile at bus 3 as well as bus 2, there are significant voltage drops depending on the ratio Z_{35} to Z_{34} .

However, I_{PV} can be controlled such that the currents from the PV plant have the ability to improve the voltage at the PCC

(bus 2). Thus, it will protect the sensitive local loads connected to bus 2 from experiencing a severe voltage dip.

$$V_2 = V_4 - I_f Z_{34} + I_{PV} Z_{23} \quad (14)$$

Assuming that X/R of the system impedance is high, and the reactive unbalanced currents generated by PV inverter controller significantly support the voltage regulation. If K_{gPV} can be chosen such that

$$K_{gPV} = \frac{Z_{34}}{Z_{23}} \quad (15)$$

Then

$$I_f Z_{34} \approx I_{PV} Z_{23} \quad (16)$$

As a result, the value of bus 2 voltage is close to bus 4 voltage ($V_2 \approx V_4$). Thus, the disturbance effect of the fault is neutralized by the additional reactive power generated by the PV plant and the ratio of the line impedance. The value of K_{gPV} can also be applied to the normal condition.

1) Fault and breaker logic

The following figures illustrate the process of the proposed control strategy drawn in Fig. 3. When $t < 0.6s$, the system is normal and balanced. During $0.6s < t < 0.9s$, a disturbance happens. And when $t > 0.9s$, protection system detects the fault so that breaker is active. So the disturbance is cut off, and the system returns to normal and balance. The system breaker is closed at $t = 1.05s$ assuming that fault has been removed at this point. The system is stable. Detailed fault and breaker logic are presented in Fig. 10.

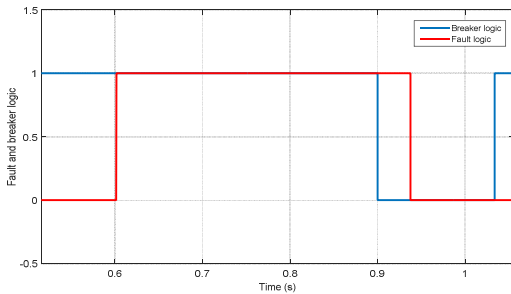


Figure 10. Fault and breaker logic under transient faults

To explain the main-control process, a double-line to ground fault is selected as the demonstration case. When the fault happens at bus 5 (phase A and B), the voltage sag also takes place at the PCC. The large grid currents flow into the faulty bus (Fig. 11 top). The current sensors detect the fault currents. From the current sensor output, the symmetrical component extractor creates a three-phase positive-sequence current as shown in Fig. 11 (bottom). Then, the three-phase positive-sequence current is decomposed into three-phase active and reactive positive-sequence currents. Only the active positive-sequence current (Fig. 12 top) that is in-phase with the grid voltage is needed in the next process. Fig. 12 (bottom) shows the distinction between the positive-sequence current

and the active positive-sequence current. Then, the three-phase active positive-sequence current is subtracted from the three-phase grid current in order to generate three-phase reactive unbalanced current ($I_{r(a,b,c)}$) (Fig. 13 top). This current is multiplied by a gain (K_{gPV}) because the inverter supplies only a small quantity (Fig. 13 bottom) to enhance the PCC voltage.

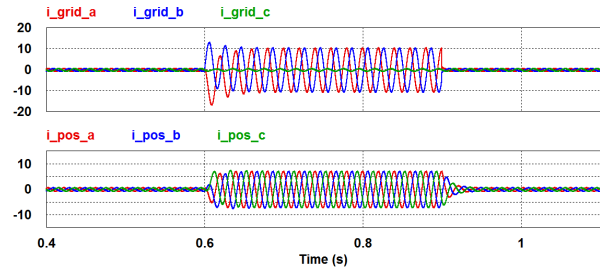


Figure 11. Grid (fault) currents (top), and positive-sequence currents (bottom).

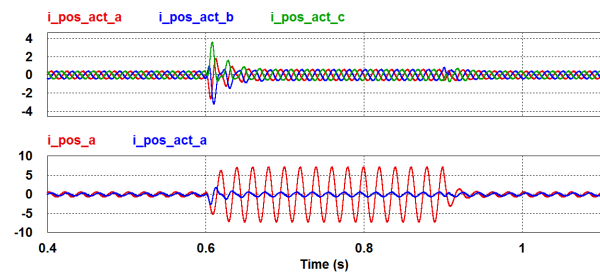


Figure 12. Three-phase active positive-sequence currents (top), and distinction between positive-sequence current and active positive-sequence current – phase A (bottom)

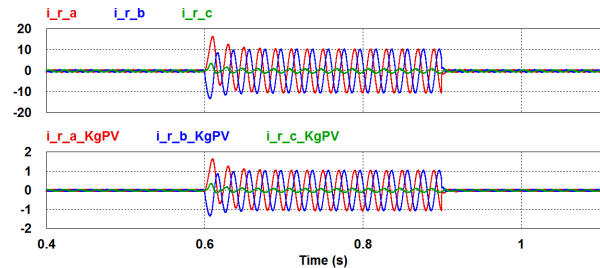


Figure 13. Reactive unbalanced currents: from the grid (top), and after multiplied by K_{gPV} (bottom)

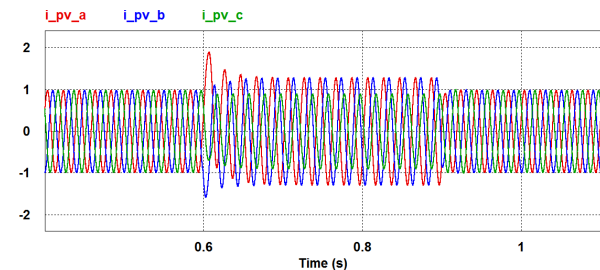


Figure 14. Three-phase reference currents (= PV inverter output currents)

Finally, the large active current ($I_{PV \text{ active}} = 0.7p.u$) from PV panels is added to create the three-phase reference current as

(Fig. 14). The amount of active power generated from PV panels is not affected by the disturbances. For dependent current source's gain equals one, the PV output currents equal to the reference currents.

2) Symmetrical faults

Symmetrical faults happen when there is a three-phase short circuit. In this case, a three-phase to ground fault through Z_f occurs at bus 5. During the fault, the grid fault-current (I_f) rises considerably (Fig. 15 bottom). The fault disturbs the voltage of the adjacent buses including PCC voltage. The three-phase voltage at PCC declines significantly (Fig. 15 top).

The PV inverter senses the three-phase grid fault-current (I_f) and the controller responds quickly by generating reactive currents to counteract the voltage dip at the PCC. For a symmetrical-fault case, there is no unbalanced current. Fig. 16 (top) describes that the PV output current is a summation of the active current (from solar power, $P_{PV} = 0.7p.u.$) and the reactive current proportional to the grid fault-current. It can be seen that the system is stable and the PCC voltage is corrected very well to 1p.u, as shown in Fig. 16 (bottom), according to equation (16) and due to the PI controller. The PCC voltage is balanced as well. Hence, the voltage quality is enhanced.

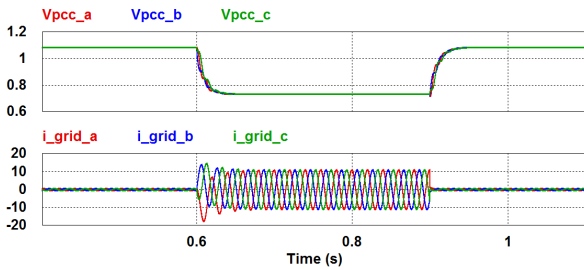


Figure 15. Voltages at PCC (top), and grid currents (bottom) without reactive power control for a three-phase to ground fault (symmetrical fault)

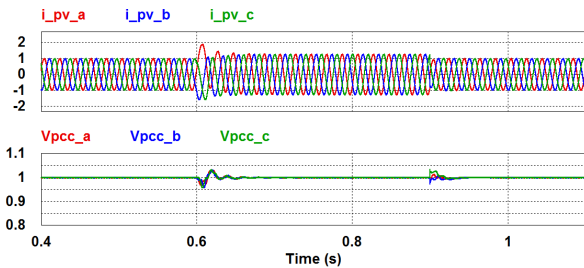


Figure 16. PV output currents (top) and voltages at PCC (bottom) with reactive power control for a three-phase to ground fault (symmetrical fault)

3) Unsymmetrical faults

The unsymmetrical faults introduced in this paper includes a single-line to ground fault, a line-to-line fault and a double-line to ground fault. The faults through Z_f create unbalanced voltage and current. Thus, the PV inverter has to produce reactive unbalanced currents to compensate unbalanced disturbances.

a) Single-Line to Ground Fault

Fig. 17 illustrates the voltage at the PCC when bus 5 experiences a single-line to ground fault at phase A. The phase-A voltage decreases about 30%, while the other phases stay a slightly higher than the normal voltage. Obviously, the phase-A grid current will rise very high and flow to the faulty bus. The phase-A grid current peak is about 10p.u (Fig. 17 bottom). The grid currents are unbalanced due to the unsymmetrical fault.

Consequently, during the fault the output current of the PV inverter will also be unbalanced, which is similar to the grid currents with a proportional gain K_{gPV} . Since K_{gPV} is selected to be 0.1, the PV reactive unbalanced current peak (phase A) is about 1p.u. From Fig. 18, it can be seen that the PV generator produces reactive unbalanced currents during the fault in addition to the active currents ($P_{PV} = 0.7p.u.$) as shown in Fig. 18 (top). The unbalanced voltage drop is compensated very well so that voltage at PCC is three-phase balanced voltage waveform and its magnitude is 1p.u (rms) (Fig. 18 bottom). The system is stable and the voltage quality is enhanced.

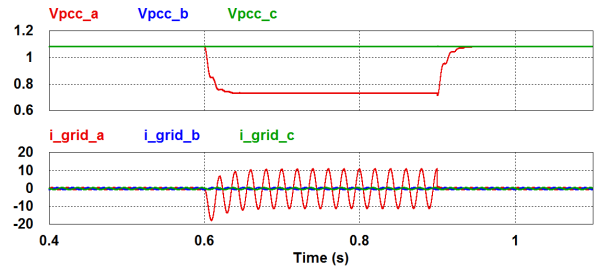


Figure 17. Voltages at PCC (top), and grid currents (bottom) without reactive power control for a single-phase to ground fault (unsymmetrical fault)

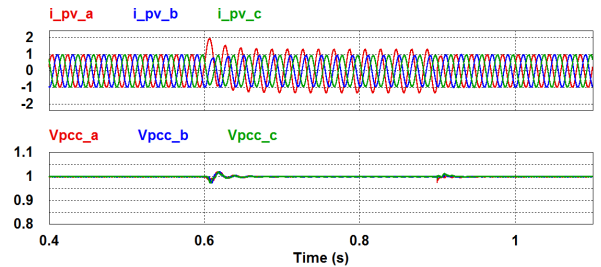


Figure 18. PV output currents (top) and voltages at PCC (bottom) with reactive power control for a single-phase to ground fault

b) Line-to-Line (double-line) to Ground Fault

Fig. 19 describes the voltage at the PCC when bus 5 experiences a line-to-line to ground fault at phase A and B. The phase-A and phase-B voltages drop about 30%, while the phase C voltage is still around the normal value. The three-phase unbalanced grid currents flow to the fault. Due to the control strategy proposed in this paper, the PV inverter will generate the active current and the reactive unbalanced current that is similar to the grid currents but with proportional gain K_{gPV} . Fig. 20 shows the PV output currents (top picture), and the PCC balanced voltages which are corrected to 1p.u (rms) during disturbance (bottom picture). The voltage quality is enhanced.

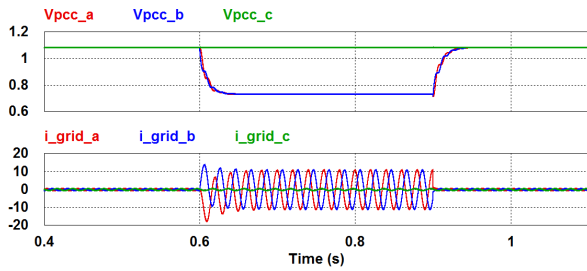


Figure 19. Voltages at PCC (top), and grid currents (bottom) without reactive power control for a line-to-line to ground fault

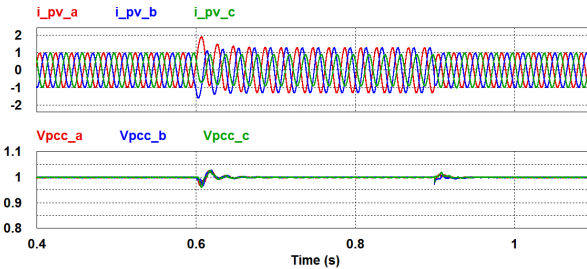


Figure 20. PV output currents (top) and voltages at PCC (bottom) with reactive power control for a line-to-line to ground fault

c) Line-to-Line Fault

Fig. 21 illustrates voltages at the PCC when bus 5 experiences a line-to-line fault between phase A and B. The short circuit between phase-A and phase-B causes voltage drops about 25% at the phase A and about 15% at phase B, while the phase C remains at a normal value. The fault also makes the phase angle of the three-phase PCC voltage unbalanced (Fig. 22). Obviously, phase-A and phase-B grid currents will rise very high and flow to the fault bus.

Similar to the previous unsymmetrical faults, based on the control strategy proposed, the PV inverter output currents will be a summation of the active current ($P_{PV} = 0.7\text{p.u.}$), the reactive unbalanced current that is similar to the grid current with a proportional gain, and an additional reactive current from the PI controller as demonstrated in Fig. 23 (top picture). The figure also shows that the system is stable, and the voltage drop is recovered significantly. Fig. 24 shows the magnitude and the phase angle of the PCC balanced voltages during disturbance. The voltage quality is enhanced.

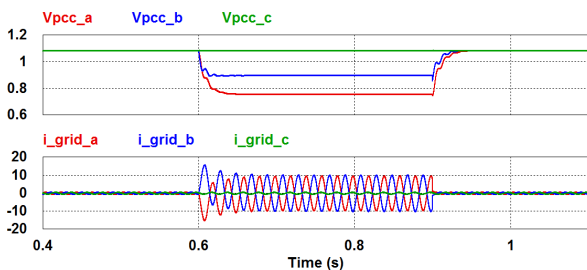


Figure 21. Voltages at PCC magnitude (top), and grid currents (bottom) without reactive power control for a line-to-line fault

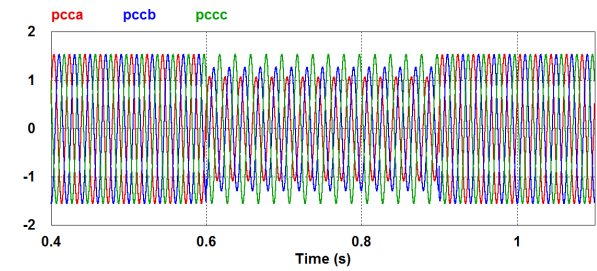


Figure 22. Unbalanced magnitude and phase angle of the PCC voltages without reactive power control for a line-to-line fault

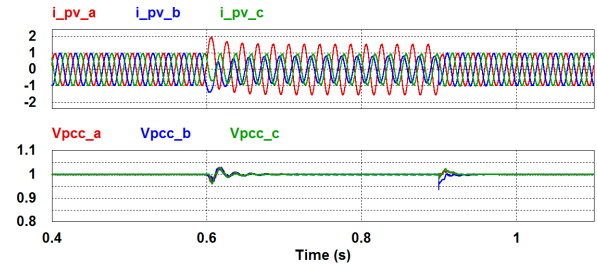


Figure 23. PV output currents (top) and voltages at PCC (bottom) with reactive power control for a line-to-line fault

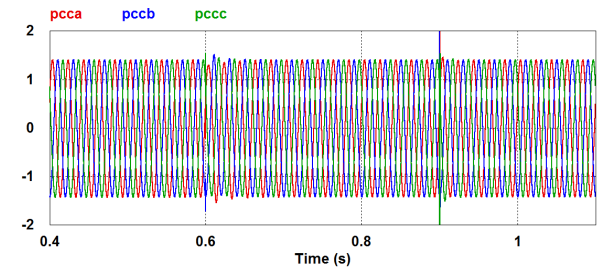


Figure 24. The balanced magnitude and phase angle of the PCC voltages with reactive power control for a line-to-line fault

D. The Effect of K_{gPV} Variation

The effect of K_{gPV} variation on the PCC voltage is described in Figure 25 and Figure 26. K_{gPV} is the impedance ratio that controls the voltage drop across Z_{23} . Without the assistance of K_{gPV} , equation (16) will not be justified. K_{gPV} can be varied corresponding to the variation of grid impedance (Z_{34}).

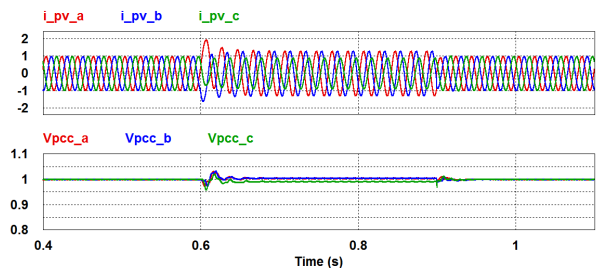


Figure 25. PV output current and PCC voltage when $K_{gPV} = 0.104$

Figure 25 shows the voltage of PCC during a fault (selected case: a double line to ground fault, phase A and B) when K_{gPV} is 0.104. Clearly, the PCC voltage is unbalanced and not equal to 1p.u. The phase-C voltage ($< 1p.u$) is lower than other two phases ($> 1p.u$). On the other hand, when K_{gPV} is 0.096 (Fig. 26), the phase-C voltage ($> 1p.u$) is higher than other two phases ($< 1p.u$).

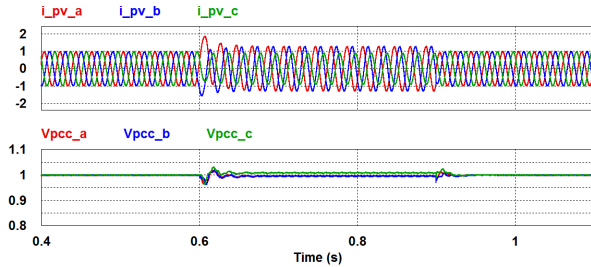


Figure 26. PV output current and PCC voltage when $K_{gPV} = 0.096$

IV. CONCLUSION

This paper presents the performance of the grid-connected PV source to support voltage regulation of microgrid system especially under transient faults. The high-power PV source is connected to the grid through a weak line with high impedance. Since PV panels only generate active power, the PV inverter is equipped with a reactive power controller to improve the power (voltage) quality.

The control strategy is based on utilizing the grid currents so that the PV generator creates a three-phase reactive unbalanced current. However, the inverter supplies only a small amount (multiplied by a gain, K_{gPV}) for improving the voltage at the PCC. The gain K_{gPV} is associated with the system impedance. This open loop strategy succeeds to maintain the PCC voltage close to 1p.u. If it is necessary to make the PCC voltage equals to 1p.u value, a simple PI controller is integrated to the main controller. The PI controller adjusts the reactive current generated by the PV inverter. The advantages of this control strategy are simple because of less computation, comprehensive and robust due to emulating the reactive current circulating in the grid

The control method proposed in this paper is simulated in PSIM. Simulation results demonstrate that satisfactory results are obtained and the proposed control strategy is feasible to manage the voltage regulation. Power quality in terms of voltage level is improved under both normal conditions and transient disturbances. The system is stable and voltage dips at the PCC due to both symmetrical and unsymmetrical faults are corrected significantly.

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